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LOS ALAMOS SCIENTIFIC LABORATORY of the University of California

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Theory of a Radio-Frequency "Spin Filter" for a Metastable Hydrogen, Deuterium, or Tritium Atomic Beam

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by

Gerald G. Ohlsen Joseph L. McKibben

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THEORY OF A RADIO-FREQUENCY "SPIN FILTER" FOR A

METASTABLE HYDROGEN, DEUTERIUM, OR TRITIUM ATOMIC BEAM

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Gerald G. Ohlsen and Joseph L. McKibben

ABSTRACT

Techniques for selection of metastable hydrogen, deuterium, or tritium atoms with a particular nuclear spin polarization are discussed. The emphasis is on the "three-level interaction" technique, which promises to be the most versatile and satisfactory of those available.

1. INTRODUCTION

In connection with the development of the Los Alamos Scientific Laboratory "metastable hydrogen" polarized ion source, calculations about possible nuclear spin selection techniques have been made. The discussion of these calculations, which have been partially reported,^{1,2} comprises the main part of this report. However, for orientation purposes, the basic operating scheme for the LASL polarized ion source is reviewed. The discussion in this section is in terms of protons, although the scheme works as well for deuterons or for tritons.

A beem of protons is extracted from a duoplasmatron and then decelerated to a velocity (~ 3×10^7 cm/ sec) corresponding to 500 eV. Additional electrons are injected to space-charge neutralize the beam, which is then passed through a curtain of cesium vapor. Collisions in the cesium convert a large number of protons into H^{2S} atoms,³ together with ground-state atoms, and positive and negative ions. The beam then enters a longitudinal magnetic field of about 500 to 600 G. A transverse "clearing" electric field separates the charged particles from the neutral atoms (H^{2S} and H^{1S}). The neutral atoms then pass through a radio-frequency transition region where the H^{2S} atoms possessing any but the desired nuclear spin magnetic quantum number are quenched to the ground state while a large fraction of the atoms with the selected m_I remain in the H^{2S} state. This mixture of ~100% polarized H^{2S} and essentially unpolarized* H^{1S} atoms is then passed through an argon exchange cell, where, at this particular velocity, the reaction $H^{2S} + A + H^- + A^+$ occurs with a probability very much larger than does the corresponding ground-state reaction.⁴

One interesting point is that the LASL nuclear spin selection method selects rather than rejects a particular nuclear spin state. Thus, a deuteron beam corresponding to a pure $m_I = 1$, 0, or -1 state may be obtained with a single radio-frequency selection device. The selection device, which employs perpendicular radio-frequency and static electric fields, behaves as a filter which allows only those metastable atoms with a specific nuclear spin quantum number (m_I) to pass through without being quenched to the ground state. This device is hereinafter referred to as a "spin filter."

The theoretical upper limit for transmission of the desired nuclear spin state through the spin filter is 1/2. Thus, for deuterons, at least 5/6 of the

*The portion of the H^{1S} produced background current which arises from decay of H^{2S} atoms in the rf region is in fact partially polarized in the opposite sense. incident metastable beam will be quenched, while for protons or tritons at least 3/4 of the incident metastable beam will be quenched. In addition, the incident atomic beam will have a large (perhaps 80 or 90%) ground-state component.

The degree of selection achieved in the argon exchange reaction depends on the ratio of the H^{2S} + $A \rightarrow H^- + A^+$ reaction cross section (denoted by σ^{2S}) to the $H^{1S} + A \rightarrow H^- + A^+$ reaction cross section (denoted by σ^{1S}). This ratio is not accurately known at present. The quantity which can be readily measured is the quenching ration Q; that is, the ratio of the negative ion yield obtained through a cesium exchange reaction followed by an argon exchange reaction without and with the application of intervening fields sufficient to quench the entire metastable component of the beam. This ratio can be expressed in terms of the fraction of the atomic beam in the metastable state, f, as follows:

$$Q = (1 - f) + f(\sigma^{2S}/\sigma^{1S}).$$

The quenching ratio is related to the resulting nuclear spin state purity (p) by

 $p = 1 - \frac{4}{Qn}$

for protons and tritons, and by

 $p = 1 - 6/Q_{\eta}$

for deuterons, where n is the efficiency of the spin filter. That is, n = 1 if the theoretical upper limit of 1/2 for transmission is reached. The relationship between p and the beam polarization parameters is given below.

	1	Spin 1/2 Particles	
	<u> </u>	P	
	1/2	р	
	-1/2	- p	
		Spin 1 Particles	
<u>m</u> I		P <u>z</u>	Pzz
1		р	р
0		0	-2p
-1		-p	р
abov	re P = 1	N(1/2) - N(-1/2), P	= N(1)

In the above P = N(1/2) - N(-1/2), $P_z = N(1) - N(-1)$, and $P_{zz} = N(1) + N(-1) - 2N(0)$, where $N(m_I)$ is the fraction of the beam particles with quantum

number m_T.

A measured value of Q = 90 was reported in Reference 4. This corresponds, for n = 0.8 (about the value expected), to a spin state purity corresponding to 91.7% for deuterons and 94.5% for protons and tritons. However, preliminary data obtained at LASL suggest that this value may be high by a factor of ~ 2 . For intense beams, the achievable Q seems to be further reduced to about 30. If these preliminary indications are correct, a spin state purity of about 83% for protons and tritons, and 75% for deuterons, would be expected.

2. ENERGY LEVELS OF THE HYDROGEN ATOM

We begin by reviewing briefly some facts about the n = 2 energy levels of the hydrogen atom. Figure 1 shows the n = 2 energy levels in a weak external magnetic field. At zero magnetic field, the energy difference between the n = 2 and n = 1 states is $13.6(\frac{1}{1^2} - \frac{1}{2^2})eV = 10.15 eV$. The $2S_{1/2} - 2P_{1/2}$

level spacing (the Lamb shift) corresponds to about 1059 MHz while the $2P_{3/2} - 2P_{1/2}$ level separation corresponds to about 10,968 MHz. In a weak magnetic field, the $2P_{3/2}$ states are split into four magnetic substates and the $2P_{1/2}$ and $2S_{1/2}$ levels each split into two magnetic substates. The $2P_{3/2}$ substates are usually referred to as a (for $m_T = 3/2$), b (for



Fig. 1. The n = 2 levels of the hydrogen atom in a weak magnetic field; nuclear hyperfine structure is neglected.



Fig. 2. The $2S_{1/2}$ and $2P_{1/2}$ levels of the hydrogen atom vs magnetic field with nuclear hyperfine structure included. The diagram for tritium atoms is nearly identical.

 $m_{J} = 1/2$, c (for $m_{J} = -1/2$), and d (for $m_{J} = -3/2$). Similarly, the 2P_{1/2} states are referred to as e (for $m_J = 1/2$) and f (for $m_J = -1/2$); the $2S_{1/2}$ states are referred to as α (for m_{τ} = 1/2) and β $(for m_{\tau} = -1/2).$

As shown in Figs. 2 and 3 for the $2S_{1/2}$ and $2P_{1/2}$ levels. which are the ones of primary interest here, the nuclear hyperfine interaction further modifies the energies. In sufficiently large magnetic fields, each magnetic substate, for hydrogen or tritium atoms, is split into two nuclear magnetic substates.



Fig. 3. The $2S_{1/2}$ and $2P_{1/2}$ levels of the deuterium atom vs magnetic field with nuclear hyperfine structure included. The order of the e and f levels is the same as the order of the α and β levels, respectively.

That is, there is a substate corresponding to each of the allowed nuclear magnetic quantum numbers $m_T = 1/2$ or $m_T = -1/2$. For deuterium atoms, where m_T can have the value 1, 0, or -1, each substate is split into three nuclear magnetic substates. Note that the order of the m_{T} substate energies is inverted when the electron spin m_{T} value is negative. The hyperfine energy level diagram for the $2S_{1/2}$ states is described by the Breit-Rabi formula:

$$W = -\frac{\Delta W}{2(2I+1)} \pm \frac{\Delta W}{2} (1 + \frac{2m_F}{1+\frac{1}{2}} X + X^2)^{1/2} + \epsilon \Delta W X m_F$$

where

ε

g

μ

В

Δ

g

$$X = B/B_{1},$$

$$B_{1} = \Delta W(1 + \epsilon)/(g_{J}\mu_{o}),$$

$$\epsilon = 1/(\frac{1836.lg_{J}}{g_{I}} - 1),$$

$$g_{J} = Lande g factor,$$

$$\mu_{o} = Bohr magneton,$$

$$B = magnetic field,$$

$$\Delta W = zero field hyperfine splitting,$$

$$g_{I} = \mu_{I}/I = nuclear g factor, and$$

$$m_{F} = m_{J} + m_{I}.$$

The last term arises from the interaction of the nuclear magnetic moment with the applied magnetic field and is, for ordinary magnetic fields, very small.

The Breit-Rabi formula is only approximate for the 2P1/2 levels since, for the field strengths of interest here, J is only an approximately good quantum number. An exact calculation requires the diagonalization of the Hamiltonian including both fine structure and hyperfine structure terms; in the numerical results presented below we have only applied a first order correction to the Breit-Rabi formula by shifting the e and f lines downward by an amount calculated from the solution to the fine structure Zeeman splitting problem. Referred to the mean value of the multiplet, the correction >is $\Delta W = -\frac{4}{9}W(\frac{B}{5214 \text{ G}})$. The values for the constants associated with the cases of interest are tabulated in Table I.

Table I Parameters Characterizing the Hyperfine Structure of the n = 2 States of Hydrogen, Deuterium, and Tritium Atoms

Nucleus	State	${f g}_{f J}$	gl	$\Delta W(MHz)$	ε	B _l (in G)
Proton	²⁵ 1/2	2.00229	5.585486	177.551	1.522×10^{-3}	63.448
Proton	2P1/2	0.66589	5.585486	59.190	4.589 x 10 ⁻³	63.796
Deuteron	²⁵ 1/2	2.00229	0.857407	40.924	0.233 x 10 ⁻³	14.605
Deuteron	^{2P} 1/2	0.66589	0.857407	13.640	0.702 x 10 ⁻³	14.644
Triton	²⁵ 1/2	2.00229	5.957680	189.588	1.623 x 10 ⁻³	67.755
Triton	^{2P} 1/2	0.66589	5.957680	63.200	4.897 x 10 ⁻³	68.138

In the numerical tabulations of the energy levels (Tables II-VII), all energies are expressed in equivalent frequency units (MHz) and are referred to the centroid of the $2S_{1/2}$ zero field multiplet. The latest published values of the Lamb shift^{6,7} have been used in this calculation (1058.05 MHz for H atoms and 1059.34 MHz for D atoms). A value of 1058.05 MHz has been used for T atoms.

The states are labeled by their strong field quantum numbers. Note that, for sufficiently high fields, the frequency separation for states whose m_I values differ by 1 unit is $\Delta W/2$ for spin 1/2 particles and $\Delta W/3$ for spin 1 particles. Note also that the magnitude of the field B_1 , which is customarily thought of as the field value which defines the weak and strong field regions, is much smaller here than is the case for ground-state atoms.

3. SELECTION RULES

The angular momenta involved in the complete description of a one-electron atomic state are the orbital angular momentum \vec{t} ; the spin angular momentum \vec{s} ; and the nuclear spin angular momentum \vec{t} . In a very strong magnetic field (i.e. in the Paschen-Back region, which is $\sim 10^5$ G or greater for n = 2 hydrogen atoms) the quantities \vec{t} , \vec{s} , and \vec{t} are completely decoupled. Thus, transitions may be induced which involve only one of the pairs of quantum numbers t, m_{e} ; s, m_{s} ; or I, m_{T} . In weaker fields where $\bar{\chi}$ and \bar{s} couple to form \bar{J} (usually known as the strong field region, which is in the range $\sim 10^2 - 10^4$ G for n = 2 hydrogen atoms), transitions can be induced which involve either J,m_J or I,m_I . Finally, for very weak fields, \bar{J} and \bar{T} couple to form \bar{F} , and transitions will involve changes in F,m_F. For a one-electron atom, s is a constant; I is always constant in atomic physics.

We are concerned here only with the lowest order transitions; i.e., with electric and magnetic dipole transitions.

a. Electric Dipole Selection Rules

The electric dipole operator is $e(\vec{E} \cdot \vec{r})$, where e is the electronic charge, \vec{E} is an applied (possibly oscillating) electric field, and \vec{r} is the electronnucleus radius vector. Since this operator is odd, it can have nonzero matrix elements only between states of opposite parity; i.e., Δt must be odd. Further, if one expands the operator into spherical components, it can be shown (Section 6) that $\Delta t =$ *1 is required.

For very strong fields, then, the selection rule is $\Delta \ell = \pm 1$; $\Delta m_{\ell} = 0$, ± 1 and $\Delta m_{I} = \Delta m_{g} = 0$, since this operator does not affect the spin functions. For strong fields we have $\Delta J = 0$, ± 1 ; $\Delta m_{J} = 0$, ± 1 and $\Delta m_{I} = 0$. For weak fields, we have $\Delta F = 0$, ± 1 ; Δm_{F} = 0, ± 1 . If $\Delta m = 0$, where m represents whichever quantity is appropriate among m_{I} , m_{g} , m_{g} , m_{J} , or

TAULE II

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HYDROGEN ATOM 25 STATES

ALPHA STAT	ES
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BETA STATES

GAUSS	X	MI≡n.5	MI==0.5	MT=-0.5	MI=n.5
0.0	0.00	44.39	44.39	44.39	-133.16
20.0	• 315	72.46	48.69	16+32	-137.47
40.0	•630	100.53	60.56	-11.75	-149.33
60.0	•946	128,60	77 . 8n	-39.82	-166.57
80.0	1•261	156.66	98.48	-67.R9	-187.25
100.0	1.576	184.73	121.32	-95.96	-210.n9
120.0	1.891	212.80	145.54	-124+03	+234 . 32
140.0	2.207	24n . 87	170.68	-152+10	-259.45
160.0	2.522	268.94	196.44	- 18n•17	-285.22
180.0	2.837	297.01	222.66	-208.24	-311.43
200.0	3.152	325.08	249.20	-236.30	-337.97
550.0	3.467	353.15	275.98	-264 • 37	-364.76
240.0	3.783	381.22	302.96	-292.44	-391.73
260.0	4.098	409.29	330.0A	-320+51	-418.86
280.0	4.413	437.36	357.32	-348.58	-446.10
300.0	4.728	465.43	384.66	-376.65	-473.43
320.0	5.044	493.49	412.07	-404.72	-500.85
340.0	5.359	521.56	439.55	-432.79	-528.33
360.0	5.674	549.63	467.09	-460.86	-555 86
380.0	5.989	577.70	494.67	-488.93	-583.44
400.0	6.304	605 77	522 29	-517.00	-611.07
420.0	6.620	633.84	549 94	-545.07	-638.72
440.0	6.935	661,91	577.63	-573.13	-666 40
460.0	7.250	689 98	605.34	-601.20	-694.11
480.0	7.565	718.05	633,07	-629.27	-721.95
500.0	7.881	745,12	660.82	-657.34	-749 60
520.0	8,196	774.19	688,59	-685.41	-777 - 77
540.0	8.511	802,26	716,38	-713.48	-805,15
560.0	8,826	830,33	744,18	-741. 55	_832,95
580.0	9.141	858,39	771,99	-769.62	860 77
600.0	9.457	886,46	799.81	-797.69	<u>_888</u> _59
620.0	9.772	914.53	827.65	-825.76	-916,42
640.0	10.087	942,60	855 49	_A51,A3	_944,27
660.0	10.402	970.67	883,34	_ 881 . 90	-972,12
680.0	10.718	998,74	911,20	-909.97	_ 999 _ 98
700.0	11.033	1026.81	939.07	-938.03	-1027.84
720.0	11.348	1054 88	966,94	-966,10	-1055,72
740.0	1).663	1082,95	994.82	-994.17	-1083.60
760.0	11.978	1111.02	1022.70	-1022.24	-1111.48
780.0	12.294	1139.09	1050.59	-1050.31	-1139.37
800.0	12.609	1167.16	1078,49	=1078+3B	-1167,26
820.0	12.924	1195,22	1106.39	-1106.45	-1195,16
840.0	13.239	1223.29	1134.29	-1134.52	-1223.07
860.0	13.555	1251.36	1162.20	-1162+59	-1250.97
HH0+0	13+870	1214.43	1140.11	-1170+66	-1278-88
900.0	14.185	1307.50	1218.02	-1218.73	-1300.79
920+0	14.500	1333,5/	1245.94	-1240+80	=1334.71
940.0	14+815	1303.64	1273.85	-12/4.86	-1362.63
960.0	15+131	1391.71	1301.79	-1302-93	-1390.55
AH0+0	13+440	1419.78	1329.70	-1351+90	=1418.48
1000+0	15•761	1447.85	1357.63	-1359+07	-}440.40

TABLE III

HYDROGEN ATOM 2P STATES

ALPHA	STATES	BETA	STATES
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GAUSS	Х	MI=0.5	MI=-1.5	MT=-0.5	MI=0.5
0.0	0.00	-1043.25	-1043.25	-1043.25	-1102.44
20.0	• 314	-1033.93	-1041.86	-1052.63	-1103.94
40.0	.627	-1024.64	-1037.98	-1061.99	-1107.95
60.0	.941	-1015.38	-1032.35	-1071-41	-1113.76
80.0	1.254	-1006.16	-1025.60	-1080.86	-1120.74
100.0	1.548	-996.96	-1018.16	-1090.34	-1128 47
120.0	1,991	-987.80	-1010.29	-1099.96	-1136.49
140 0	2 105	_970 67	-1002 15	1109 40	-1145 05
160 0	2.508	-969 57	-1007 83	-1119 09	-1164 05
180 0	2 0 0 0	-960 50	-005 30	1120 50	-1147 47
100.0	2 1 7 6	951 47	076 87	1127877	-1103+03
220 0	3 4 4 0	642 46	-969 30	-1137.73	-11/2.15
220.0	3 743		-760 JU	1157 21	-1101.30
240.0	30102	-034 EE	-051 09	=1157+N1	-1190./1
200.0	4.070	-724.55	-971.00	-117/+57	-1200-12
280.0	4.349	-915.05	-942.45	-11//+12	-1209.60
300+0	4+/03	-906.//	-933+02	-1186.42	-1219-15
320+0	5.010	-89/.93	-722+50	-1196.75	-1228.75
340.0	5+330	-889.12	-916.59	-1205+62	-1238.41
350.0	5+643	-880.34	-901.99	-1216+51	-1248+12
350.0	5+95/	-8/1.59	=899.40	-1220+44	-1257.87
400.0	6.270	-802.87	-890.04	-1235+40	-126/ 6/
420+0	0.584	-034.14	-882.30	-1240-39	-12//•51
440.0	5.847	-845.54	=8/3./7	-1256+42	-1287-39
460.0	7.211	-836.92	-365.27	-1205.48	-1297.32
480.0	7.574	-828,33	-856.80	-12/6.56	-1307.28
500.0	7.838	-819.77	-848.35	-1286.48	~1317 _• 28
520.0	8+151	-811.25	-839.92	-1296.84	-1327.32
540.0	0.403	=002,70	-71.02	-1307.02	=1357.40
500.0	8.778	-/94.30	-823,15	-1317.74	-1.347.51
580.0	9.092	-103.01	-814.01	-132/ .43	-1357.65
630 0	7 4 1 3	760 11	-010	-133/ ./0	-130/ -44
640 0	9./19	-760 70	-795.20	-1347.08	-13/8,06
640.0	10.032	-752 40	-701 71	-1105+42	-1300.11
600.0	10+340	744 01	7771+11	-1307+80	-1340+00
700 0	10.077	-735 07	-765 36	=1379.20	-1418.97
720 0	11.394	-727 77	-757 10	-1400.13	-1420 44
740.0	11.600	-710 59	-740 00	-1410.62	-1427+55
760 0	11.013	-711 45	-741 00	-1421 16	-1450 54
780.0	12.227	-702.34	-733.94	-1421+17	-1450.74
800 0	12.240		-734 03	-1431472	
830.0	12 940	487 33	-716 92	-1446+36	-14/1.55
840.0	17.147	-679.21	-709 96	-1457.47	-1492.11
860.0	13-101	-67, 23	=700.00	-1403002	-14-2070
880.0	13.704	-663.39		-14/4431	-1503+32
900.0	14.108	-655.36	-685.24	-1407+04	-1513.94
930.0	14+4-110	-647.47		-1477470	-1727+00
940.0	14-921	-639.63	-011041	-170797	-1733.38
960.0	15.049	-631.84	=661.89	-1711+41	-1740.14
980.0	15.262	=624.01	-661.02	-1-2-1-20	-1750.72
1000.0	15.475	-614.35		-1-57-15	1901474
100000	124012	-010052	-0+0+33	-1-20+07	-1210+24

TABLE IV

DEUTERIUM ATOM 25 STATES

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ALPHA STATES BETA STATES

GAUSS	X	MT=1	M1=0	MT=+1	MI=-1	MI=O	MI=1
0.0	0.000	13.64	13.64	13.64	13.64	-27.28	-27.28
50.0	1+369	41.68	33.01	21.94	-14.40	-35.49	-46.64
40.0	2.739	69.72	58.95	46.03	-42.44	-59.70	-72.56
60.0	4.108	97.76	86.10	72.77	-70.49	-86.45	-09.71
80.0	5.477	125.80	113.66	100.17	-98.52	-113.96	-127.25
100.0	6.847	153 84	141 30	100.17	-176 56	-141.50	-154 97
100.0	9.316	191 99	141.39	127072	-156 60	-141.52	-107 70
120.0	0 506	101.00	107.1-	100.77	-13++00	-107-31	-196+10
140.0	4.546	209.92	197.10	143+43	-192.64	-197+17	-210.65
100.0	10.422	231.90	223.02	211+32	-210.68	-225+07	-234.55
180.0	12.374	266.00	252.96	239.24	-238.72	-253+00	-246.48
200+0	13.694	294.04	S80+71	267 . 17	-266.76	-280+95	-294.42
550.0	15+063	322.08	308.88	295.12	-294.R0	-308+91	-322.38
240.0	16+432	350,12	336.86	323.09	-322.83	-336.88	-350.35
260.0	17.902	378.16	364.85	351.06	-350.97	-364•87	-378.32
280.0	19.171	406.20	392.84	379.03	-378,91	-392+86	-406.30
300.0	20.541	434.24	420.83	407.01	-406.95	-420.85	-434.28
320.0	21.910	462.28	448.83	435.00	-434.99	-448.85	-462.27
340.0	23.279	490.32	476.84	462.99	-463.03	-476.85	-490.26
360.0	24.649	518.36	504.84	490.98	-491.07	-504.85	-518.25
380.0	26+018	546.40	512.85	518.97	-519.11	-532.86	-546.24
400.0	27.387	574.44	560.86	546.97	-547.15	-560.87	-574.24
430.0	28.757	602.47	508.87	674.96	-575 10	-589.99	-514124
440.0	30.126	630.51	616 88	603.96	-603.33	-504144	-630.34
460.0	31.496	658 55	644 90	670.06	-631 07	-646.00	-669 34
480.0	31.445	686 59	670.91	459.04	-659 31	-673.93	-696 76
500 0	32 0003	714 47	700 97	484 07	-077.41 407 aF	-700 07	714 24
500.0	344634	74.03	700.73			700.43	-14.24
520.0	17+004	142.01	720.95	/14.9/	-/15.39	-120.95	-142.25
540.0	30.973	//0./1	756.95	142.91	-143,43	-756.97	-170.25
560.0	34.342	/94./5	784.98	770.98	-771.47	-784.98	-798.26
580.0	39.712	826,79	813.00	798.98	-799.51	-813.00	-826,26
600.0	41.081	854,83	841.02	826.99	-827.55	-841.02	-854,27
620.0	42.451	882,87	869.04	854.99	-855,59	-869.04	-882.27
640.0	43.820	910,91	897.06	883.00	-883.63	-897.06	-910.28
660.0	45.189	938,95	925.04	911.01	-911.67	-925.08	-938.29
680.0	46.559	966,99	953,10	939.02	-939.71	-953.10	-966,30
700.0	47 . 928	995.03	981.12	967.02	-967.75	-981.12	-994.30
720.0	49.297	1023.07	1000.14	995.03	-995.79	-1009.14	-1022.31
740.0	50.667	1051.11	1037.16	1023+n4	-1023.83	-1037-17	-1050.32
760.0	52+036	1079.15	1065.19	1051.05	-1051.87	-1065+19	-1078.33
780.0	53.405	1107.19	1093.21	1079.06	-1079.91	-1093-21	-1106.34
800.0	54.775	1135.23	1121.23	1107.07	-1107.95	-1121-23	-1134.35
820.0	56.144	1163.27	1149.25	1135+08	-1135.99	-1149.25	-1162.36
840.0	57.514	1191.31	1177.28	1163.09	-1164.03	-1177.28	-1190.37
860.0	58.883	1219.35	1205.30	1191.10	-1192.07	-1205-30	-1218.38
880.0	60.252	1247.39	1233.32	1219.11	-1220.11	-1233-32	-1246.30
900-0	61.622	1275.47	1261.34	1247.13	=1248.14	=1261.25	-1274-40
9:0.00	62.991	1303.47	1289.37	1075.10	-1276.19	-1289.37	-1203.41
940.0	64.360	1331.61	1217.20	1203-14	=1304.00	-1217-30	-1305+41
960.0	45.730	1331031	1365.69	1 70 3 4 4	-1304+22	-131/157	-1340+42
980.0	67.400	1387 69	1347442	1,53[0]3	-1332.70	-1347+42	-1397.43
0.00		1307+37	1373+44	1324010		-1401-14	-1375+44
1000+0	00+404	1412+03	1401+46	130/0]/	-1388.34	-1401+46	-1414+45

TABLE V

DEUTFRIUM ATOM 2P STATES

ALPHA STATES BETA STATES

GAUSS	X	MI=1	MI=0	M[=-1	MI=-1	MI=0	MI=1
0.0	0.000	-1054.79	-1054.79	-1054.79	-1054.79	-1068+43	-1068.43
20+0	1.366	-1045.48	-1048.37	-1052.10	-1064.14	-1071+18	-1074.89
40.0	2.731	-1036.20	-1039.80	-1044.10	-1073.51	-1079-27	-1043.55
60+0	4.097	-1026.96	-1030.85	-1035-29	-1082.92	-1088-24	-1092.66
80+0	5.463	-1017.74	-1021.79	-1026.30	-1092.35	-1097+47	-1101.93
100.0	6.829	-1008.56	-1012.72	-1017.25	-1101.82	-1106+81	-1111.29
120+0	8.194	-999.41	-1003.64	-1008+18	-1111.32	-1116+23	-1120.71
140.0	9.560	-990.29	-994.57	-999.13	-1120,86	-1125.70	-1130.18
160.0	10.926	-981,20	-985.53	-990.10	-1)30,42	-1135-21	-1139.70
180.0	12.292	-972,15	-976.50	#981 .08	-1140.02	-1144.77	-1149.26
200.0	13.657	-963,12	-967.51	-972.09	-1149,65	-1154.37	-1158.85
220.0	15.023	-954.13	-958.54	-963.13	-1159,31	-1164.00	-1168,48
240.0	16.389	-945,17	-949.60	-954.20	-1169.00	-1173.67	-1178.14
260.0	17.755	-936,24	<u>-940</u> 69	-945.30	-1178,72	-1183.37	_ 1187 . 84
280.0	19.120	-927.35	-931.81	-936.42	=1188,48	-1193.11	-1107.57
300.0	20.486	-918,48	-922.96	- 927 . 58	-1198,27	-1202.88	-1207.34
320.0	21.852	-909,65	-914.14	-918.76	-1208,09	-1212.69	-1217.14
340.0	23.217	-900,85	-905,35	-909.98	-1217.94	-1222.52	-1226.97
360.0	24,583	-892,08	-896 60	-901.23	-1227,82	-1232.39	-1236-83
380.0	25.949	-883,34	-887.87	-892.51	-1237,73	-1242.29	-1246.73
400.0	27.315	-8/4,64	_H79_17	-883.81	-1247,68	-1252.23	-1256,66
420.0	28.680	-865,96	-870,51	-875,16	-1257,66	-1262.20	-1266.62
440.0	30.046	-857,32	-861,88	-866.53	-1267,67	-1272.20	-1276.61
450.0	31.412	-848.71	-853,27	-857.93	-1277,71	-1282.23	-1286.64
480.0	32.778	-840,13	-844.70	-849.36	-1287,79	-1292+29	-1296.69
500.0	34 143	+831,58	-H36,17	-840.83	-1297,89	-1302.39	-1306.78
520.0	35.509	-823.07	-H27.66	-832.33	-1308.03	-1312.51	-1316.91
540.0	30.013	=014,57	-819,18	-423.85	-1318,20	-1322.67	-1327.06
500.0	30 606	707 73		907	-1320,40	-1332.47	-1337-24
600.0	40.972	_789 33	-703 95	-798 47	-1348 00	-1343+09	-134/.40
620 0	40 338	-780 97	-705 60	-790.00	-1340.40	-1353+34	-137/+/1
640.0	43.703	-772.65	-777 28	-781 97	-1369 53	-1373.05	-136/.99
660.0	45.069	-764.36	-768 99	-773.49	-1370 00	-1284.20	1200 65
680.0	46.435	-756.10	-760.74	-765.44	=1390.38	-1294.69	-1300.03
700.0	47.801	-747.87	-752.52	-757.32	=1400.70	-1405.10	=14.9.43
720.0	49.166	-739.67	-744.33	-749.03	=1411.16	-1415.55	-1419.88
740.0	50.532	-731.51	-736.17	-740.88	=1421.65	=1426+03	=1430.35
760.0	51.898	-723.38	-728.04	-732.76	=1632.17	-1436.54	-1440.85
780.0	53.264	-715.28	-719.94	-724.66	-1442.72	-1447.08	-1451.39
800.0	54,629	-707.21	-711.88	-716.60	-1453.30	-1457.66	-1461.96
820.0	55 995	-699.17	-703.85	-708.57	-1463.92	-1468.26	-1472.55
840.0	57.361	-691.16	-695.85	-700.58	-1474.56	-1478.90	-1483.19
860.0	58+727	-683.19	-687.88	-692+61	-1485.24	-1489+57	-1493.85
880.0	60.092	-675.25	-679.94	-684 .68	-1495.95	-1500+28	-1504.54
9n0•0	61+458	-667.34	-672.03	-676 . 78	-1506.69	-1511.01	-1515+27
920 • 0	62.824	-659,46	-664.16	-669.90	-1517.47	-1521.77	-1526.03
940.0	64.189	-651.61	-656.32	-661.07	-1528.27	-1532.57	-1536-82
960.0	65•555	-643.80	-648.51	-653.26	-1539.11	-1543+40	-1547.64
980.0	66.921	-636.02	-64 0,73	-645.4B	-1549 98	-1554.26	-1558.50
1000.0	68,287	-628,27	-632,98	-637.74	-1560 88	-1565.16	-1569.38

TABLE VI

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TRITIUM ATOM 25 STATES

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			ALPHA S	TATES	BETA S	TATES
$ \begin{array}{c} GAUSS & X & MI = n.5 & MI = n.5 & MI = n.5 & MI = n.5 \\ n.0 & n.00 & 47.40 & 47.4n & 47.4n & -142.19 \\ 20.0 & .295 & 75.47 & 51.44 & 19.32 & -146.23 \\ 40.0 & .590 & 103.54 & 62.68 & -8.75 & -157.48 \\ 6n.0 & .886 & 131.61 & 79.22 & -36.82 & -174.02 \\ 80.0 & 1.181 & 159.69 & 99.28 & -64.89 & -194.n7 \\ 100.0 & 1.476 & 187.76 & 121.6n & -92.96 & -216.39 \\ 120.n & 1.771 & 215.83 & 145.4n & -121.n4 & -240.2n \\ 140.0 & 2.066 & 243.90 & 170.2n & -149.11 & -265.n0 \\ 160.n & 2.066 & 243.90 & 170.2n & -149.11 & -265.n0 \\ 160.n & 2.066 & 243.90 & 170.2n & -149.11 & -265.00 \\ 160.n & 2.066 & 243.90 & 170.2n & -149.11 & -265.00 \\ 160.n & 2.066 & 243.90 & 170.2n & -149.11 & -265.00 \\ 160.n & 2.066 & 243.90 & 170.2n & -149.11 & -265.00 \\ 160.n & 2.061 & 271.97 & 195.7n & -177.18 & -290.49 \\ 180.0 & 2.457 & 300.05 & 221.68 & -205.25 & -316.48 \\ 200.0 & 2.457 & 306.19 & 274.66 & -261.40 & -369.46 \\ 240.0 & 3.542 & 384.26 & 311.50 & -289.47 & -396.30 \\ 260.0 & 3.837 & 412.33 & 328.51 & -317.54 & -423.30 \\ 260.0 & 3.837 & 412.33 & 328.51 & -317.54 & -423.30 \\ 260.0 & 3.837 & 412.33 & 328.51 & -317.54 & -450.44 \\ 300.0 & 4.428 & 468.48 & 382.89 & -373.48 & -477.69 \\ 320.n & 4.723 & 496.55 & 410.23 & -401.76 & -505.02 \\ 340.n & 5.n18 & 524.62 & 437.64 & -229.83 & -532.43 \\ 360.n & 5.n18 & 524.62 & 437.64 & -429.83 & -532.43 \\ 360.n & 5.813 & 552.69 & 465.11 & -457.91 & -587.92 \\ 340.n & 5.08 & 580.77 & 492.63 & -485.97 & -587.42 \\ 400.n & 6.494 & 664.98 & 575.45 & -570.19 & -670.24 \\ 460.n & 6.789 & 693.05 & 603.11 & -598.26 & -697.91 \\ 480.n & 7.970 & 805.34 & 714.02 & -710.55 & -808.81 \\ 560.n & 8.265 & 833.41 & 741.79 & -738.62 & -836.58 \\ 580.0 & 8.560 & 861.49 & 769.58 & -664.24 & -781.66 \\ 540.0 & 9.446 & 945.70 & 853.01 & -850.91 & -947.80 \\ 660.0 & 9.741 & 973.77 & 880.84 & -878.98 & -975.63 \\ 680.0 & 10.185 & 809.56 & 797.37 & -794.76 & -892.17 \\ 70.0 & 10.931 & 1029.92 & 936.52 & -935.12 & -1031.37 \\ 720.0 & 10.626 & 1057.99 & 964.38 & -963.20 & -1059.17 \\ 70.0 & 10.921 & 1086.06 & 992.24 & -991.27 & -1087.03 \\ 70.$			-		_	-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	GAUSS	¥	Miso.5	MT=0.5	MTE-0.5	MT=0 4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0,0000	0.000	47 40	47 40	47.40	-142 10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20.0	1000	75 47	47.440	4/440	-146 -19
0.00 0.390 10.395 0.790 10.395 0.790	40.0	.590	103 54	47.68	17032	
0.00 $1.4.00$ $1.51.01$ $7.2.2$ $-3.5.2.2$ $-1.7.1.02$ 0.00 $1.4.76$ 187.76 121.60 -92.96 -216.39 120.01 1.771 215.83 145.40 -121.04 -240.20 140.00 2.066 243.90 170.20 -149.11 -265.00 160.01 2.361 271.97 195.70 -177.18 -290.49 $1A0.00$ 2.657 300.05 221.68 -205.25 -316.48 200.01 2.952 $32A.12$ 248.04 -233.32 -342.83 220.03 3.247 356.19 274.66 -261.40 -369.46 240.03 3.542 384.26 301.50 -289.47 -396.30 260.03 3.637 412.33 328.51 -317.54 -423.30 280.04 4.133 440.41 355.65 -346.47 -396.30 260.00 4.428 468.48 382.89 -373.48 -477.69 320.01 4.428 468.48 382.89 -373.48 -477.69 320.01 4.723 496.55 410.23 -401.76 -505.02 340.01 5.018 524.62 437.64 -429.83 -532.43 360.01 5.904 608.84 520.20 -587.42 -587.42 400.05 5.904 608.84 520.20 -514.04 -614.99 420.01 6.199 636.91 547.81 -562.433 -725.60 500.01 <td>€0.0</td> <td>.996</td> <td>103.34</td> <td>79 33</td> <td>-76.07</td> <td>-174 07</td>	€0.0	.996	103.34	79 33	-76.07	-174 07
$100 \cdot 0$ $1 \cdot 476$ $187 \cdot 76$ $121 \cdot 60$ $-92 \cdot 96$ $-216 \cdot 39$ $120 \cdot 0$ $1 \cdot 771$ $215 \cdot 83$ $145 \cdot 40$ $-121 \cdot 04$ $-240 \cdot 20$ $140 \cdot 0$ $2 \cdot 066$ $243 \cdot 90$ $170 \cdot 20$ $-149 \cdot 11$ $-265 \cdot 00$ $160 \cdot 0$ $2 \cdot 361$ $271 \cdot 97$ $195 \cdot 70$ $-177 \cdot 18$ $-290 \cdot 49$ $180 \cdot 0$ $2 \cdot 657$ $300 \cdot 05$ $221 \cdot 68$ $-205 \cdot 25$ $-316 \cdot 48$ $200 \cdot 0$ $2 \cdot 952$ $328 \cdot 12$ $248 \cdot 04$ $-233 \cdot 32$ $-342 \cdot 83$ $220 \cdot 0$ $3 \cdot 542$ $384 \cdot 26$ $301 \cdot 50$ $-289 \cdot 47$ $-396 \cdot 30$ $260 \cdot 0$ $3 \cdot 837$ $412 \cdot 33$ $328 \cdot 51$ $-317 \cdot 54$ $-423 \cdot 30$ $260 \cdot 0$ $3 \cdot 837$ $412 \cdot 33$ $328 \cdot 51$ $-317 \cdot 54$ $-423 \cdot 30$ $260 \cdot 0$ $3 \cdot 837$ $412 \cdot 33$ $328 \cdot 51$ $-317 \cdot 54$ $-423 \cdot 30$ $260 \cdot 0$ $3 \cdot 837$ $412 \cdot 33$ $328 \cdot 51$ $-317 \cdot 54$ $-423 \cdot 30$ $260 \cdot 0$ $3 \cdot 837$ $412 \cdot 33$ $328 \cdot 51$ $-317 \cdot 54$ $-423 \cdot 30$ $260 \cdot 0$ $4 \cdot 133$ $440 \cdot 41$ $355 \cdot 65$ $-345 \cdot 61$ $-450 \cdot 44$ $300 \cdot 0$ $4 \cdot 428$ $468 \cdot 48$ $382 \cdot 89$ $-373 \cdot 68$ $-477 \cdot 69$ $320 \cdot 0$ $4 \cdot 723$ $496 \cdot 55$ $410 \cdot 23$ $-401 \cdot 76$ $-505 \cdot n2$ $340 \cdot 0$ $5 \cdot 618$ $580 \cdot 77$ $492 \cdot 63$ $-485 \cdot 97$ $-587 \cdot 42$ $360 \cdot 0$ $5 \cdot 618$ $580 \cdot 77$ $492 \cdot $	90.0	1.101	151.01	09 29	-64.00	-194 -7
100.01.476107.10121.00-72.40-210.14120.01.771215.83145.40-121.04-240.20140.02.066243.90170.20-149.11-265.00160.02.361271.97195.70-177.18-290.491A0.02.657300.05221.68-205.25-316.48200.02.952328.12248.04-733.32-342.83220.03.947356.19274.66-261.40-369.46240.03.542384.26301.50-289.47-396.30260.03.837412.33328.51-317.54-423.30280.04.133440.41355.65-345.61-450.44300.04.428468.48382.89-373.68-477.69320.04.723496.55410.23-401.76-505.02340.05.018524.62437.64-429.83-532.43360.05.018524.62437.64-445.97-559.90380.05.608580.77492.63-485.97-587.42400.05.408580.77492.63-485.97-587.42400.05.408580.77492.63-485.97-587.42400.05.408580.77492.63-642.40-753.32520.06.199636.91547.81-542.12-642.60540.07.470805.34714.02-710.55-808.81560.08.265833.41741.79<	100.0	1.476	187 76	101 60	-041-77 D-06	-016 -00
140.002.0.06243.90170.20 -149.11 -265.00 160.02.361271.97195.70 -177.18 -290.49 180.02.457300.05221.68 -205.25 -316.48 200.02.952328.12248.04 -233.32 -342.83 220.03.247356.19274.66 -261.40 -369.46 240.03.542384.26301.50 -289.47 -396.30 260.03.837412.33328.51 -317.54 -423.30 280.04.428468.48382.89 -373.68 -477.69 320.04.723496.55 410.23 -401.76 -505.02 340.05.618524.62 437.64 -429.83 -532.43 360.05.618580.77492.63 -485.97 -587.42 400.05.904608.84521.20 -514.04 -614.99 420.06.199636.91547.81 -542.12 -642.60 440.06.494664.98575.45 -570.19 -670.24 460.07.970805.34714.02 -710.55 -808.81 50.07.675777.27 686.26 -682.48 -781.06 540.07.970805.34714.02 -710.55 -808.81 560.08.765833.41741.79 -739.62 -846.37 60.09.151917.63 422.84 -919.98 640.09.446945.70 853.01 -850.91 -94	120.0	1.771	215.83	145.40	=121.04	-240.20
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	140.0	2.066	243.90	170.20	=149.11	-245 00
180.002.457300.05221.68-205.25-316.48200.002.952328.12244.04-233.32-342.83220.003.947356.19274.66-261.40-369.46240.003.542384.26301.50-289.47-396.30260.003.837412.33328.51-317.54-423.30260.003.837412.33328.51-317.54-423.30260.004.133440.41355.65-345.61-450.44300.004.428468.48382.89-373.68-477.69320.014.723496.55410.23-401.76-505.02340.015.018524.62437.64-429.83-532.43360.015.618580.77492.63-485.97-587.42400.015.608580.77492.63-485.97-587.42400.015.904608.84520.20-514.04-614.99420.016.199636.91547.81-542.12-642.60440.016.494664.98575.45-570.19-670.24460.016.789693.05603.11-598.26-697.91480.017.970805.34714.02-710.55-808.81560.017.675777.27686.26-682.48-781.06540.017.970805.34714.02-710.55-808.81560.018.265833.41741.79-738.62-866.58580.018.560	160.0	2.361	271.97	195.70	-177.18	-290.49
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	180.0	2.457	300.05	221.69	-205.25	-316.49
220.0 3.747 356.19 274.666 $7.561.40$ -369.46 240.0 3.542 384.26 $3n1.50$ -289.47 -396.30 260.0 3.837 412.33 328.51 -317.54 -423.30 280.0 4.133 440.41 355.65 -345.61 -450.44 300.0 4.428 468.48 382.89 -373.68 -477.69 320.0 4.723 496.55 410.23 -401.76 -505.02 340.0 5.018 524.62 437.64 -429.83 -532.43 360.0 5.618 $58n.77$ 492.63 -485.97 -587.42 400.0 5.904 608.84 520.20 -514.04 -614.99 420.0 6.199 636.91 547.81 -542.12 -642.60 440.0 6.494 664.98 575.45 -570.19 -670.74 460.0 6.199 636.91 547.81 -582.12 -642.60 440.0 6.494 664.98 575.45 -570.19 -670.74 460.0 6.199 636.91 547.81 -582.12 -642.60 440.0 6.494 664.98 575.45 -570.19 -670.74 460.0 6.789 693.05 603.11 -598.26 -697.91 480.0 7.675 777.27 686.26 -682.48 -781.06 50.0 7.675 777.27 686.26 -682.48 -781.06 540.0 7.970 805.3	200.0	2.952	328,12	248.04	-233.32	-342.83
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	220.0	3.247	356.19	274.66	=261.40	-369.46
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	240.0	3.542	384.26	301.50	-289.47	-396.30
$\begin{array}{c} 280.0 & 4.133 & 440.41 & 355.65 & -345.61 & -450.44 \\ 300.0 & 4.428 & 468.48 & 382.89 & -373.68 & -477.69 \\ 320.0 & 4.723 & 496.55 & 410.23 & -401.76 & -505.02 \\ 340.0 & 5.018 & 524.62 & 437.64 & -429.83 & -532.43 \\ 360.0 & 5.313 & 552.69 & 465.11 & -457.90 & -559.90 \\ 380.0 & 5.608 & 580.77 & 492.63 & -485.97 & -587.42 \\ 400.0 & 5.904 & 608.84 & 520.20 & -514.04 & -614.99 \\ 420.0 & 6.199 & 636.91 & 547.81 & -542.12 & -642.60 \\ 440.0 & 6.494 & 664.98 & 575.45 & -570.19 & -670.74 \\ 460.0 & 6.494 & 664.98 & 575.45 & -570.19 & -670.74 \\ 460.0 & 6.789 & 693.05 & 603.11 & -598.26 & -697.91 \\ 480.0 & 7.084 & 721.13 & 630.81 & -626.33 & -725.60 \\ 500.0 & 7.379 & 749.20 & 658.53 & -654.40 & -753.32 \\ 520.0 & 7.675 & 777.27 & 686.26 & -682.48 & -781.06 \\ 540.0 & 8.265 & 833.41 & 741.79 & -738.62 & -806.58 \\ 580.0 & 8.560 & 861.49 & 769.58 & -766.69 & -864.37 \\ 600.0 & 9.446 & 945.70 & 853.01 & -850.91 & -947.80 \\ 640.0 & 9.446 & 945.70 & 853.01 & -850.91 & -947.80 \\ 660.0 & 9.741 & 973.77 & 880.84 & -878.98 & -975.63 \\ 680.0 & 10.036 & 1001.85 & 908.67 & -907.05 & -1003.47 \\ 700.0 & 10.922 & 1086.06 & 922.24 & -991.27 & -1087.03 \\ 720.0 & 10.626 & 1057.99 & 964.58 & -963.20 & -1059.17 \\ 740.0 & 10.922 & 1086.06 & 922.24 & -991.27 & -1087.03 \\ 760.0 & 11.217 & 1114.13 & 1020.11 & -1019.34 & -1114.90 \\ \end{array}$	260.0	3.837	412.33	328.51	-317.54	-623.30
300.0 4.428 468.48 382.89 -373.48 -477.69 320.0 4.723 496.55 410.23 -401.76 -505.02 340.0 5.018 524.62 437.64 -429.83 -532.43 360.0 5.018 527.69 465.11 -457.90 -559.90 $3R0.0$ 5.608 580.77 492.63 -485.97 -587.42 400.0 5.904 608.84 520.20 -514.04 -614.99 420.0 6.199 636.91 547.81 -542.12 -642.60 440.0 6.494 664.98 575.45 -570.19 -670.24 460.0 6.494 693.05 603.11 -598.26 -697.91 $4R0.0$ $7.0R4$ 721.13 630.81 -626.33 -725.60 500.0 7.675 777.27 686.26 -682.48 -781.06 540.0 7.970 805.34 714.02 -710.55 -808.81 560.0 8.265 833.41 741.79 -739.62 -864.37 600.0 9.446 945.70 853.01 -850.91 -947.80 640.0 9.446 945.70 853.01 -878.98 -975.63 680.0 9.741 973.77 880.84 -878.98 -975.63 680.0 9.744 973.77 880.84 -878.98 -975.63 680.0 9.744 973.77 880.84 -878.98 -975.63 680.0 9.446 <td< td=""><td>280.0</td><td>4.133</td><td>440.41</td><td>355.65</td><td>-345.61</td><td>-450.44</td></td<>	280.0	4.133	440.41	355.65	-345.61	-450.44
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	300.0	4.428	468.48	382.89	-373.68	-477.69
340.0 5.018 524.62 437.64 -429.83 -532.43 360.0 5.313 552.69 465.11 -457.90 -559.90 380.0 5.608 580.77 492.63 -485.97 -587.42 400.0 5.904 608.84 520.20 -514.04 -614.99 420.0 6.199 636.91 547.81 -542.12 -642.60 440.0 6.494 664.98 575.45 -570.19 -670.24 460.0 6.494 693.05 603.11 -598.26 -697.91 480.0 7.084 721.13 630.81 -626.33 -725.60 500.0 7.675 777.27 686.26 -682.48 -781.06 540.0 7.970 805.34 714.02 -710.55 -808.81 560.0 8.265 833.41 741.79 -738.62 -864.37 600.0 8.560 861.49 769.58 -766.69 -864.37 600.0 9.151 917.63 825.18 -822.84 -919.98 640.0 9.446 945.70 853.01 -850.91 -947.80 660.0 9.741 973.77 880.84 -878.98 -975.63 680.0 10.185 908.67 -907.05 -103.47 70.0 10.331 1029.92 936.52 -935.12 -1031.32 720.0 10.626 1057.99 964.38 -963.20 -1059.17 740.0 10.922 1086.06	320.0	4.723	496.55	410.23	-401.76	-505.02
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	340.0	5.018	524.62	437.64	-429.83	-532.43
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	360.0	5.313	552.69	465.11	-457.90	-559.90
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	380.0	5.608	58n .77	492.63	-485.97	-587.42
$420 \cdot 0$ $6 \cdot 199$ $636 \cdot 91$ $547 \cdot 81$ $-542 \cdot 12$ $-642 \cdot 60$ $440 \cdot 0$ $6 \cdot 494$ $664 \cdot 98$ $575 \cdot 45$ $-570 \cdot 19$ $-670 \cdot 24$ $460 \cdot 0$ $6 \cdot 789$ $693 \cdot 05$ $603 \cdot 11$ $-598 \cdot 26$ $-697 \cdot 91$ $480 \cdot 0$ $7 \cdot 084$ $721 \cdot 13$ $631 \cdot 81$ $-626 \cdot 33$ $-725 \cdot 60$ $500 \cdot 0$ $7 \cdot 079$ $749 \cdot 20$ $658 \cdot 53$ $-654 \cdot 40$ $-753 \cdot 32$ $520 \cdot 0$ $7 \cdot 675$ $777 \cdot 27$ $686 \cdot 26$ $-682 \cdot 48$ $-781 \cdot 66$ $540 \cdot 0$ $7 \cdot 970$ $805 \cdot 34$ $714 \cdot 02$ $-710 \cdot 55$ $-808 \cdot 81$ $560 \cdot 0$ $8 \cdot 265$ $833 \cdot 41$ $741 \cdot 79$ $-733 \cdot 62$ $-836 \cdot 58$ $580 \cdot 0$ $8 \cdot 560$ $861 \cdot 49$ $769 \cdot 58$ $-766 \cdot 69$ $-864 \cdot 37$ $601 \cdot 0$ $8 \cdot 855$ $889 \cdot 56$ $797 \cdot 37$ $-794 \cdot 76$ $-892 \cdot 17$ $620 \cdot 0$ $9 \cdot 151$ $917 \cdot 63$ $825 \cdot 18$ $-822 \cdot 84$ $-919 \cdot 98$ $640 \cdot 0$ $9 \cdot 446$ $945 \cdot 70$ $853 \cdot 01$ $-870 \cdot 91$ $-947 \cdot 80$ $660 \cdot 0$ $9 \cdot 741$ $973 \cdot 77$ $880 \cdot 84$ $-878 \cdot 98$ $-975 \cdot 63$ $680 \cdot 0$ $10 \cdot 331$ $1029 \cdot 92$ $936 \cdot 52$ $-935 \cdot 12$ $-1031 \cdot 32$ $720 \cdot 0$ $10 \cdot 626$ $1057 \cdot 99$ $964 \cdot 38$ $-963 \cdot 20$ $-1059 \cdot 17$ $740 \cdot 0$ $10 \cdot 922$ $1086 \cdot n6$ $992 \cdot 24$ $-991 \cdot 27$ $-1087 \cdot n3$ $760 \cdot 0$ $11 \cdot 217$ $1114 \cdot 13$ <td>400.0</td> <td>5.904</td> <td>608.84</td> <td>520.20</td> <td>-514.04</td> <td>-614.99</td>	400.0	5.904	608.84	520.20	-514.04	-614.99
$440 \cdot n$ $6.4.94$ 664.98 575.45 $-57n.19$ -670.24 $46n \cdot n$ 6.789 693.05 $6n3.11$ -598.26 -697.91 $48n \cdot n$ 7.084 721.13 $63n.81$ -626.33 -725.60 $5n0 \cdot n$ 7.379 749.20 658.53 -654.40 -753.32 $520 \cdot n$ 7.675 777.27 686.26 -682.48 -781.66 $540 \cdot n$ 7.970 805.34 714.02 -710.55 -808.81 $560 \cdot n$ 8.265 833.41 741.79 -739.62 -864.37 $6n0 \cdot n$ 8.560 861.49 769.58 -766.69 -864.37 $6n0 \cdot n$ 8.560 861.49 769.58 -766.69 -864.37 $6n0 \cdot n$ 8.550 899.56 797.37 -794.76 -892.17 $62n \cdot n$ 9.151 917.63 $A25.18$ -822.84 -919.98 $640 \cdot n$ 9.446 945.70 853.01 -850.91 -947.80 $660 \cdot n$ 9.741 973.77 $88n.84$ -878.98 -975.63 $680 \cdot n$ 10.626 1057.99 964.38 -963.20 -1059.17 $740 \cdot n$ 10.626 1057.99 964.38 -963.20 -1087.03 $760 \cdot n$ 11.217 1114.13 $102n.11$ -1019.34 -1114.90	420.0	6+199	636.91	547.81	-542.12	-642.60
460.0 6.789 693.05 603.11 -598.26 -697.91 480.0 7.084 721.13 630.81 -526.33 -725.60 500.0 7.379 749.20 658.53 -654.40 -753.32 520.0 7.675 777.27 686.26 -682.48 -781.06 540.0 7.970 805.34 714.02 -710.55 -808.81 560.0 8.265 833.41 741.79 -739.62 -864.37 500.0 8.560 861.49 769.58 -766.69 -864.37 600.0 8.550 889.56 797.37 -794.76 -892.17 620.0 9.151 917.63 825.18 -822.84 -919.98 640.0 9.446 945.70 853.01 -850.91 -947.80 660.0 9.741 973.77 880.84 -878.98 -975.63 680.0 10.185 908.67 -907.05 -1003.47 700.0 10.626 1057.99 964.38 -963.20 -1059.17 740.0 10.922 1086.06 992.24 -991.27 -1087.03 760.0 11.217 1114.13 1020.11 -1019.34 -1114.90	440.0	6.494	664.98	575.45	-570 • 19	-670.24
$4^{H}0 \cdot 0$ $7 \cdot 0^{H}4$ $721 \cdot 13$ $631 \cdot 81$ $-626 \cdot 33$ $-725 \cdot 60$ $5n0 \cdot 0$ $7 \cdot 379$ $749 \cdot 20$ $658 \cdot 53$ $-654 \cdot 40$ $-753 \cdot 32$ $520 \cdot 0$ $7 \cdot 675$ $777 \cdot 27$ $686 \cdot 26$ $-682 \cdot 48$ $-781 \cdot n6$ $540 \cdot 0$ $7 \cdot 970$ $805 \cdot 34$ $714 \cdot 02$ $-710 \cdot 55$ $-808 \cdot 81$ $560 \cdot 0$ $8 \cdot 265$ $833 \cdot 41$ $741 \cdot 79$ $-738 \cdot 62$ $-836 \cdot 58$ $580 \cdot 0$ $8 \cdot 560$ $861 \cdot 49$ $769 \cdot 58$ $-766 \cdot 69$ $-864 \cdot 37$ $6n0 \cdot 0$ $8 \cdot 855$ $889 \cdot 56$ $797 \cdot 37$ $-794 \cdot 76$ $-892 \cdot 17$ $620 \cdot 0$ $9 \cdot 151$ $917 \cdot 63$ $825 \cdot 18$ $-822 \cdot 84$ $-919 \cdot 98$ $640 \cdot 0$ $9 \cdot 446$ $945 \cdot 70$ $853 \cdot 01$ $-850 \cdot 91$ $-947 \cdot 80$ $660 \cdot 0$ $9 \cdot 741$ $973 \cdot 77$ $880 \cdot 84$ $-878 \cdot 98$ $-975 \cdot 63$ $680 \cdot 0$ $10 \cdot 331$ $1029 \cdot 92$ $936 \cdot 52$ $-935 \cdot 12$ $-1031 \cdot 32$ $720 \cdot 0$ $10 \cdot 626$ $1057 \cdot 99$ $964 \cdot 38$ $-963 \cdot 20 - 1059 \cdot 17$ $740 \cdot 0$ $10 \cdot 922$ $1086 \cdot n6$ $992 \cdot 24$ $-991 \cdot 27 - 1087 \cdot n3$ $760 \cdot 0$ $11 \cdot 217$ $1114 \cdot 13$ $1020 \cdot 11$ $-1019 \cdot 34$ $-1114 \cdot 90$	460.0	6.789	693.05	603.11	-598.26	-697.91
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	480+0	7.084	721.13	630.81	-626+33	-725.60
520.0 7.675 777.27 686.26 -562.48 -781.08 540.0 7.970 805.34 714.02 -710.55 -808.81 560.0 8.265 83.41 741.79 -739.62 -836.58 580.0 8.560 861.49 769.58 -766.69 -864.37 600.0 9.856 89.56 797.37 -794.76 -892.17 620.0 9.151 917.63 825.18 -822.84 -919.98 640.0 9.446 945.70 853.01 -850.91 -947.80 660.0 9.741 973.77 880.84 -878.98 -975.63 680.0 10.185 908.67 -935.12 -103.47 700.0 10.331 1029.92 936.52 -935.12 -1031.32 720.0 10.626 1057.99 964.38 -963.20 -1059.17 740.0 10.922 1086.06 992.24 -991.27 -1087.03 760.0 11.217 1114.13 1020.11 -1019.34 -114.90	500.0	7.379	749.20	658.53	-654.40	-/53.32
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	520.0	7.070	111.21	714 07	-102.4H	=/81.05
580.0 8.743 633.41 741.17 -734.76 -864.37 580.0 8.560 861.49 769.58 -766.69 -864.37 600.0 8.455 889.56 797.37 -794.76 -892.17 620.0 9.151 917.63 825.18 -822.84 -919.98 640.0 9.446 945.70 853.01 -850.91 -947.80 660.0 9.741 973.77 880.84 -878.98 -975.63 680.0 10.1.85 908.67 -907.05 -103.47 700.0 10.331 1029.92 936.52 -935.12 -1031.32 720.0 10.626 1057.99 964.38 -963.20 -1059.17 740.0 10.922 1086.06 992.24 -991.27 -1087.03 760.0 11.217 1114.13 1020.11 -1019.34 -1114.90	540.0	8 345	877 41	741 70	-739 40	=700 H1
600.0 8.855 889.56 797.37 -794.76 -892.17 600.0 9.151 917.63 825.18 -822.84 -919.98 640.0 9.446 945.70 853.01 -850.91 -947.80 660.0 9.741 973.77 880.84 -878.98 -975.63 680.0 10.136 1001.85 908.67 -907.05 -1003.47 700.0 10.331 1029.92 936.52 -935.12 -1031.32 720.0 10.626 1057.99 964.38 -963.20 -1059.17 740.0 10.922 1086.06 992.24 -991.27 -1087.03 760.0 11.217 1114.13 1020.11 -1019.34 -1114.90	590 0	0.703	861 40	740 50	-766 60	444 77
620.0 9.151 917.63 825.18 -822.84 -919.98 640.0 9.446 945.70 853.01 -850.91 -947.80 660.0 9.741 973.77 880.84 -878.98 -975.63 680.0 10.136 1001.85 908.67 -907.05 -1003.47 700.0 10.331 1029.92 936.52 -935.12 -1031.32 720.0 10.626 1057.99 964.38 -963.20 -1059.17 740.0 10.922 1086.06 992.24 -991.27 -1087.03 760.0 11.217 1114.13 1020.11 -1019.34 -1114.90	600 0	9.955	889 56	797 37	-794.76	-892 17
640.0 9.446 945.70 853.01 -850.91 -947.80 640.0 9.446 945.70 853.01 -850.91 -947.80 660.0 9.741 973.77 880.84 -878.98 -975.63 680.0 10.136 1001.85 908.67 -907.05 -1003.47 700.0 10.331 1029.92 936.52 -935.12 -1031.32 720.0 10.626 1057.99 964.38 -963.20 -1059.17 740.0 10.922 1086.06 992.24 -991.27 -1087.03 760.0 11.217 1114.13 1020.11 -1019.34 -1114.90	620 0	9,151	917 63	825 19	-822 84	_919 98
660.0 9.741 973.77 880.84 -878.98 -975.63 680.0 10.0.36 1001.85 908.67 -907.05 -1003.47 700.0 10.331 1029.92 936.52 -935.12 -1031.32 720.0 10.626 1057.99 964.38 -963.20 -1059.17 740.0 10.922 1086.06 992.24 -991.27 -1087.03 760.0 11.217 1114.13 1020.11 -1019.34 -1114.90	640.0	9.446	945.70	853 01	-850.91	-947.80
680.0 10.036 1001.85 908.67 -907.05 +1003.47 700.0 10.331 1029.92 936.52 -935.12 -1031.32 720.0 10.626 1057.99 964.38 -963.20 -1059.17 740.0 10.922 1086.06 992.24 -991.27 -1087.03 760.0 11.217 1114.13 1020.11 -1019.34 -1114.90	660.0	9.741	973.77	880.84	-878.98	-975.63
7nn+0 10+331 1029+92 936+52 -935+12 -1n31+32 720+0 10+626 1057+99 964+38 -963+20 -1059+17 740+0 10+922 1086+06 992+24 -991+27 -1087+03 760+0 11+217 1114+13 1020+11 -1019+34 -1114+90	680.0	10+036	1001.85	9n8.67	-907.05	+1003.47
720+0 10+626 1057+99 964+38 -963+20 -1059+17 740+0 10+922 1086+06 992+24 -991+27 -1087+03 760+0 11+217 1114+13 1020+11 -1019+34 -1114+90	700.0	10+331	1029.92	936.52	-935+12	-1031.32
740.0 10.922 1086.06 992.24 -991.27 -1087.03 760.0 11.217 1114.13 1020.11 -1019.34 -1114.90	720.0	10•626	1057.99	964.38	-963.20	-1059.17
760+0 11+217 1114+13 1020+11 -1019+34 -1114+90	740•0	10.925	1086.06	992.24	-991.27	-1087+03
	760•0	11+512	1114.13	1020+11	-1019.34	-1114.90
780+0 11+512 1142+21 1047+98 -1047+41 -1142+77	780.0	11•512	1142.21	1047.98	-1047.41	-1142.77
800+0 11+807 1170+28 1075+86 -1075+48 -1170+65	800.0	11+807	1170.28	1075-86	-1075+48	-1170.65
820.0 12.102 1198.35 1103.74 -1103.56 -1198.54	820.0	12.102	1198.35	1103.74	-1103+56	-1198.54
840.0 12.348 1226.42 1131.03 -1131.63 -1226.42	840.0	12+348	1226.42	1131.63	-1131+63	-1220.42
860.0 12.443 1254.47 1154.52 -1154.70 -1254.32	860.0	12+643	1254.49	1154.52	-1159+70	-1254+32
000.0 12.002 1310 64 1015 30 1016 04 1310 11	0.040	12.093	1202.5/	114/442	-1016.04	-1310 -1
	0000	13.579	1310.04	1212.35	-1717444	-1210011
940.0 13.873 1366.78 1271.13 -1271.09 -1365.02	940-0	13.973	1366.78	1271.13	-1271.09	-1365.92
960.0 14.169 1394.85 1299.04 -1300.06 -1393.84	960-0	14.169	1394.85	1299.04	-1300.06	-1393.84
940.0 14.464 1422.93 1326.95 -1328.13 -1421.75	940.0	14.464	1422.93	1326.95	-1329-13	-1421.75
	1000.0	14.759	1451.00	1354.87	-1356.20	-1449.66

TABLE VII

TRITIUM ATOM 2P STATES

ALPHA	STATES	BETA	STATES

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GAUSS	X	MI#0.5	MI=-0.5	Mĭ==0.5	MI=0.5
0.0	0.000	-1042.25	-1042.25	-1042.25	-1105.45
20.0	.294	-1032.93	-1040.95	-1051.63	-1106.87
40.0	+587	-1023.64	-1037.28	-1060.99	-1110.67
60.0	.881	-1014.38	-1031.88	-1070+41	-1116.25
80.0	1 • 174	-1005.15	-1025.34	-1079.86	-1123.03
100.0	1.468	-995.95	-1018.07	-1089.35	-1130.58
120.0	1.761	-986.79	-1010.34	-1098.86	-1138.66
140.0	2.055	-977.66	-1002.31	-1109+41	-1147.11
160.0	2.348	-968,56	- 994.08	-1117.99	-1155.82
180.0	2.642	-959.49	-985.72	-1127.60	-1164.72
200.0	2.935	-950.45	-977.26	-1137.24	-1173.78
220.0	3.229	-941.45	-968.75	-1146.91	-1182.96
240.0	3.522	-932,48	-960.19	-1156.62	-1192.24
260.0	3.816	-923.54	-951.61	-1166+36	-1201.62
280.0	4 • I N 9	-914.63	-943.02	-1176+13	-1211.06
300.0	4+403	-905.75	-934.42	-1185.93	-1220.58
320•0	4.696	-896.91	-925.82	-1195.77	-1230+15
340.0	4.990	-888.10	-917.24	-1205+63	-1239.79
360.0	5.283	-879.32	-908.66	-1215.53	-1249.47
380.0	5+577	-8/0.5/	-900.09	-1225+46	-1259+20
400+0	5+871	-801.85	-891+55	=1235+42	-1268.99
420.0	0+164	-853.11	-883.02	-1245.42	-12/8.н1
440.0	0.470	-076 00	-0/4.51	-1255+44	-1200.60
40()•()	7.045	-837 30	-967 54	=1205+50	-1540+24
500.0	7.338	-818 75	-849.13	-1285.71	-1300+74
520.0	7.632	-810.22	=840.71	-1295.97	-1328.55
540.0	7.925	-801.73	-832.32	=1306.05	-1338.62
560.0	8.219	-793.27	-823.96	-1316-27	-1348.72
580.0	8.512	-784.84	-815.62	-1326.52	-1358.86
600.0	8.806	-776.44	-807.31	-1336.80	-1369.03
620.0	9.099	-768.08	-799.03	-1347+11	-1379.24
640.0	9.393	-759.74	- 791.78	-1357.46	-1389.49
660•0	9.686	-751.44	-782.56	-1367.84	-1399.77
680.0	9.980	-743.17	-774.36	-1378+25	-1410+08
700+0	10.273	-734.93	-766.20	-1388.69	-1420.43
720.0	10.567	-726.73	-758.06	-1399+16	-1430.R1
740.0	10.860	-718.55	-749.95	-1409+66	-1441+23
760.0	11+154	-710.41	-741.87	-1420-20	-1451.68
780.0	11.448	-702.30	-733.82	-1430.77	-1462.16
800.0	11.741	-694 23	-/25.80	-1441.37	-1472.68
820.0	12.035	-686,18	-717.82	-1452.00	-1483.23
040.0	12.325	-0/0,1/	-/04.00	-1402.07	-1493.81
880.0	12+622	-0/0.18	≠101.73	-14/3.37	=1504.43
	12.713	*002.23	-674.03	-1404.04 1404.04	-1212.08
930 0	13.207	-034.32	-478 30	-1474.47 1805 KE	-1525./6
940 0	13.702	-638 57	-670 52	-1614 47	-1530,44
960.0	14.080	-630 75	-663 74	-1537 33	-1558 -1
980.0	14, 383	_622 96	-655 00	-1538.22	-1568 85
1000.0	14.676	-615.20	=647.29	-1549.14	-1579 47
*****	148010	-010420	~~~~	~1 14 2014	~ * * * * * 0 0 1

 $m_{\rm F}$, the field required to induce the transition is parallel to the quantization axis, while if $\Delta m = \pm 1$, it is perpendicular to the quantization axis.

b. Magnetic Dipole Selection Rules

The magnetic dipole operator is of the form $-\vec{\mu} \cdot \vec{B}'$ where \vec{B}' is usually an oscillating or rotating magnetic field, and where $\vec{\mu}$ may be an electronic or nuclear magnetic moment. This operator can have nonzero matrix elements only between states of the same parity. This means, at least for the present case, $\Delta \ell = 0$.

For very strong fields we have $\Delta m_I = 0$, *1 and $\Delta \ell = \Delta m_{\ell} = \Delta m_{\rm s} = 0$; or $\Delta m_{\rm s} = 0$, *1 and $\Delta \ell = \Delta m_{\ell} = \Delta m_{\rm I} = 0$. For intermediate fields we have $\Delta J = 0$, *1; $\Delta m_{\rm J} = 0$, *1 and $\Delta m_{\rm I} = 0$; or $\Delta m_{\rm I} = 0$, *1 and $\Delta J = \Delta m_{\rm J} = 0$. For weak fields we have $\Delta F = 0$, *1, $\Delta m_{\rm F} = 0$, *1. Again the magnitude of Δm determines, in the same way as above, the parallel or perpendicular nature of the field required to induce the transition.

Finally, we note that $F = 0 \Rightarrow F = 0$ is absolutely forbidden for one-quantum transitions.

4. DISCUSSION OF THE GENERAL SPIN STATE SELECTION PROBLEM

A wide assortment of methods exists which might be used to polarize a metastable hydrogen atomic beam. This is in contrast to the problem of spin state selection in an ordinary (ground state) hydrogen atomic beam where only magnetic dipole transitions between the various hyperfine components, or adiabatic reduction of the magnetic field, may be considered.

It is believed that a "three-level interaction," in which the applied fields may simultaneously cause transitions among three levels, offers the best solution to the selection problem. This technique, which was first demonstrated and explained by Lamb and Retherford, 5 and Lamb, 8 is the method used in the LASL ion source. However, we first consider some of the various other possibilities by which a polarized metastable atomic beam may be produced.

In a magnetic field of about 575 G the β and e states become degenerate. If a small (a few V/cm) transverse electric field is applied, the β -states are coupled to the short-lived e-states (the half-life of the e-states is ~1.6 nsec) and decay rapidly. Thus one can obtain a beam of a metastables. Such a beam is analagous to the beam obtained in conventional polarized ion sources after separation in a quadrupole or sextupole field. That is, there is 100% electronic polarization but no nuclear polarization. Such a beam could then be converted to a partially polarized negative ion beam by adiabatically reducing the magnetic field to near zero before the $H^{2S} + A \rightarrow H^{-} + A^{+}$ reaction is allowed to occur. However, these particles have a relatively high velocity ($\sim 3 \times 10^7$ cm/sec) and thus a long and carefully designed decreasing B field region is probably needed. Drake and Krotkov,⁹ who first used this method, attributed the fact that they obtained only $\sim 2/3$ of the theoretical polarization to an inadequate length in their B field transition region.

To obtain increased polarization, one must turn to a selective transition scheme of some sort. We first consider the use of a magnetic dipole transition between a particular α state and a particular β state in exactly the fashion often used in conventional polarized ion sources. One finds, however (see Section 6), that the electric dipole matrix elements are of the order of $1/\alpha$ (\approx 137) times larger than the magnetic dipole matrix elements. Even though a line through an rf cavity can be found where 8 is maximum and E is zero, for practical beam sizes the <u>average</u> E field will be sufficiently large to make the electric dipole transition rate far exceed the magnetic dipole transition rate.

We ask if these electric dipole transitions might be directly employed for our purposes. For hydrogen or tritium atoms the α -f frequency separation for the two m_I values is approximately 120 MHz; this is to be compared with the natural width of 100 MHz for the f (and e) levels. Thus one could possibly obtain a reasonable polarization with such a transverse electric field transition. However, both the beam intensity and polarization depend critically on the rf power level. For deuterium atoms the corresponding frequency separation is only about 18 MHz, so for this case the method is infeasible. The corresponding α -e (longitudinal electric field) transitions are separated by onehalf the corresponding α -f separation; thus these



Fig. 4. Schematic diagram of the α -d crossing; the numbers correspond to the $\Delta m_{\rm F}$ required for a transition between the two crossing states.

transitions would be even less favorable.

It has been demonstrated¹⁰ that at the α -d crossing (~2360 G) a static electric field may be used to preferentially quench a single nuclear spin state. For protons or tritons, only $\alpha(m_T = -1/2)$ and $d(m_{\tau} = 1/2)$ can be coupled by electric dipole radiation. Since this transition violates the strong field selection rules $\Delta m_{I} = 0$, $\Delta m_{J} = 0$, ± 1 , it is "first-order forbidden." However, the remaining transitions involve $\Delta m_{F} > 1$ and, because they are incompatible with dipole radiation, are more highly forbidden. Figure 4 illustrates this situation for both spin 1/2 and spin 1 nuclei. It is seen that, in the deuteron case, two transitions are compatible with $\Delta m_{\rm F} \neq 1$ (transverse electric field) and one with $\Delta m_{\rm F} = 0$ (longitudinal electric field). Thus one could selectively quench one magnetic substate for spin 1/2 systems and either one or two magnetic substates for spin 1 systams. Since the transitions here are first-order forbidden, relatively large electric fields are needed and serious loss will occur through the α -f or α -e transitions. It has been estimated¹⁰ that, for protons, one might obtain 50% polarization with 25% a state survival.

Another proposal¹¹ involves the use of a radio-

frequency transition at zero magnetic field. The $2S_{1/2}(F = 1)$ level may be coupled to the $2P_{1/2}$ (F = 0) level by longitudinal or transverse radiation of the appropriate frequency. A small magnetic field is permissible if both transverse and longitudinal radiations are present. The $28_{1/2}$ (F = 0) state is not appreciably quenched by coupling to the $2P_{1/2}$ (F = 1) state because the frequency difference is ~236 MHz; the $2S_{1/2}$ (F = 0) to $2P_{1/2}$ (F = 0) transition is strictly forbidden. Thus, one might obtain a pure $2S_{1/2}$ (F = 0) metastable beam. If the field were then adiabatically increased to a high value, the metastable beam would have 100% nuclear and 100% electronic longitudinal polarization. This scheme, however, is applicable only to protons or tritons.

5. QUANTUM MECHANICAL FORMULATION OF THE FOUR-LEVEL PROBLEM

We consider only the four-level system α , β , e, and f since the $2P_{3/2}$ levels are sufficiently distant to have no significant effect on our problem. In addition, since we are working in a strong magnetic field, the nuclear magnetic quantum number m_I is conserved and we may therefore consider separately each group of four atomic levels associated with a particular nuclear spin orientation.

For the amplitudes of the α , β , e, and f states, we use the notation a, b, c, and d. We use ω (with or without subscripts) to denote an angular frequency.

The Schroedinger equation may be written:

$$(H_{o} + H')\psi = i\hbar \frac{\partial \psi}{\partial t}$$
,

where H_0 is a time-independent Hamiltonian whose eigenfunctions satisfy the equation $H_0 u_n = E_n u_n$. If the exact wave function is written in the form

$$\psi = \Sigma a_n(t) u_n^{-iE_nt/h},$$

it is easy to show that the coefficients $a_n(t)$ must satisfy the differential equations

$$i\hbar\dot{a}_{k} = \Sigma H' a_{kn} t$$

where

$$\omega_{\rm kn} = (E_{\rm k} - E_{\rm n})/\hbar \, ,$$

$$H_{kn}' = \int u_k^* H' u_n d\tau \cdot$$

For the four-level case, these equations may be written out explicitly as:



where the damping terms $-i\gamma c/2$ and $-i\gamma d/2$ have been added to account for the decay of the e and f states. Except for the damping terms, the above matrix is Hermitian. The α - β and e-f transitions may be induced only by a transverse magnetic field; the α -f and β -e transitions may be induced only by a transverse electric field; and the α -e and β -f transitions may be induced only by a longitudinal electric field.

We assume a longitudinal oscillating electric field (angular frequency ω), with an associated transverse oscillating magnetic field, and a transverse static electric field. The matrix elements may then be written in the form

> H' Ba = hMcoswt = ħM'cosωt H' fe

ъ

H'	=	ħRcosωt
H'rs	=	ħR'coswt
H	=	ħV
H' fa	=	ň۷',

where M and M' represent magnetic dipole matrix elements, R and R' represent longitudinal electric dipole matrix elements, and V and V' represent transverse electric dipole matrix elements. (The notation R and V is selected since R and R' will be associated with a radio-frequency electric field, and V and V' will be associated with a static electric field.) These matrix elements are discussed in Section 6; for the present we merely observe that the magnitude of dipole matrix elements is directly proportional to the relevant applied field. Note that the unprimed matrix elements relate to the e level, and the primed matrix elements relate to the f level.

In this notation our equations become:

$$\begin{bmatrix} i\dot{a} \\ i\dot{b} \\ i\dot{c} \\ i\dot{d} \end{bmatrix} = \begin{bmatrix} 0 & M^* e^{i\omega_{\alpha}\beta^t} \cos \omega t & R^* e^{i\omega_{\alpha}e^t} \cos \omega t & V^{**} e^{i\omega_{\alpha}f^t} \\ M & e^{-i\omega_{\alpha}\beta^t} \cos \omega t & 0 & V^* e^{i\omega_{\beta}e^t} & R^{**} e^{i\omega_{\beta}f^t} \cos \omega t \\ R & e^{-i\omega_{\alpha}e^t} \cos \omega t & V & e^{-i\omega_{\beta}e^t} & -i\gamma/2 & M^{**} e^{i\omega_{e}f^t} \cos \omega t \\ V^* & e^{-i\omega_{\alpha}f^t} & R^* e^{-i\omega_{\beta}f^t} \cos \omega t & M^* e^{-i\omega_{e}f^t} \cos \omega t & -i\gamma/2 \end{bmatrix} \begin{bmatrix} a \\ b \\ c \\ d \end{bmatrix}$$

The equations are used in this form for the numerical integration studies discussed in Sections 8 and 9. However, the effect of the f state on the system is not large--it merely causes a slow overall decay of the metastable beam. For our first discussion of the system, we neglect the f level effects.

Also, except in the numerical integration studies, we follow the standard practice¹² and drop the term in cos $\omega t = \frac{1}{2} (e^{i\omega t} + e^{-i\omega t})$ which is incapable of resonance. (We note that this approximation cannot be made for both frequencies if one uses an oscillating transverse electric field as well as an oscillating longitudinal electric field, since then at least two frequency terms can always resonate. In fact, one then obtains interference between the two contributions.) With these approximations the equations become:

$$\begin{bmatrix} i \tilde{a} \\ 0 \\ M e \end{bmatrix} = \begin{bmatrix} 0 \\ M e^{-i(\omega_{\alpha\beta} - \omega)t} \\ M e^{-i(\omega_{\alpha\beta} - \omega)t} \\ 0 \\ -i(\omega_{\alpha e} - \omega)t \\ R e \end{bmatrix} \begin{bmatrix} -i(\omega_{\alpha e} - \omega)t \\ 0 \\ 0 \end{bmatrix}$$

These are the equations given by Lamb.⁸ In Section 7 we follow the method indicated by Lamb to obtain an analytic solution to these equations for the special case of constant field magnitudes during the interaction time.

6. MATRIX ELEMENTS

Neglecting the nuclear hyperfine interaction, the wave functions which describe the n = 2 states of the hydrogen atom may be written in the form given in Table VIII.* The coefficients $\varepsilon_1 - \varepsilon_4$ can be expressed as follows. Define the dimensionless parameter $\xi = \mu_0 B/\Delta E$, where ΔE is the fine structure splitting (10,968 MHz). (ξ becomes unity at a field of about 7800 G; thus, as far as fine structure is concerned, we are interested primarily in the weak field region. Accordingly, Table VIII is subdivided into the weak field groups (where J and m_J are good quantum numbers) although the wave functions are exact for all fields.) We may write

$$\varepsilon_{1} = \sqrt{\frac{3}{4}(1 + \delta_{+})}$$

$$\varepsilon_{2} = \sqrt{\frac{3}{2}(1 - \delta_{+})}$$

$$\varepsilon_{3} = \sqrt{\frac{3}{2}(1 + \delta_{-})}$$

$$\varepsilon_{h} = \sqrt{\frac{3}{4}(1 - \delta_{-})}$$

where

$$\delta_{+} = (\xi + 1/3)/\sqrt{1 + 2\xi/3 + \xi^2}$$

and

$$\delta_{-} = (\xi - 1/3)/\sqrt{1 - 2\xi/3 + \xi^2}$$

The quantities ξ , δ_{+} , δ_{-} , and $\epsilon_{1} - \epsilon_{1}$ are tabulated,

$\begin{bmatrix} i(\omega & -\omega)t \\ R^* & e \end{bmatrix}$	a
v* e ^{iω} βe ^t	ъ
-iy/2	c]

for various magnetic fields, in Table IX. We note that, for zero field, $\xi_{+} + 1/3$, $\xi_{-} + -1/3$ and $\varepsilon_{1} - \varepsilon_{1}$ become unity. In that case, the coefficients in Table IX become the usual Clebsch-Gordan coefficients which couple angular momenta 1 and 1/2. For large fields, $\xi_{+} + 1$ and $\xi_{-} + 1$; thus ε_{2} and ε_{1} become zero while $\varepsilon_{1} + \sqrt{\frac{3}{2}}$ and $\varepsilon_{3} + \sqrt{3}$. In this case, we obtain the wave functions for which t, m_{t} . s, and m_{s} are the appropriate quantum numbers. We now consider the effect of the nuclear hyperfine

* The values of $\epsilon_1 - \epsilon_4$ were obtained from Bethe and Salpeter,¹³ Section 46. The Clebsch-Gordan coefficients and angular functions used throughout this section are, however, those of Condon and Shortley.¹⁴ The tables of matrix elements given in Ref. 13 may be used if account is taken of the $(-1)^m$ difference in phase conventions for the spherical harmonics.

Multiplet	State		Function
	a	3/2	R ₂₁ ψ ₁₁ (+)
2P2/2	Ъ	1/2	$\int_{3}^{\underline{p}} \varepsilon_{1} R_{21} \psi_{10} (+) + \int_{3}^{\underline{1}} \varepsilon_{2} R_{21} \psi_{11} (+)$
3/2	с	-1/2	$\int_{3}^{\underline{h}} \varepsilon_{3} R_{21} \psi_{1-1} (+) + \int_{3}^{\underline{2}} \varepsilon_{4} R_{21} \psi_{10} (+)$
	đ	-3/2	$R_{21}\psi_{1-1}$ (+)
2P1/2	e	1/2	$-\int_{3}^{\underline{1}} \epsilon_{2} R_{21} \psi_{10} (+) \int_{3}^{\underline{2}} \epsilon_{1} R_{21} \psi_{11} (+)$
_, _	f	-1/2	$-\sqrt{\frac{2}{3}}\varepsilon_{4}R_{21}\psi_{1-1}(+) + \sqrt{\frac{1}{3}}\varepsilon_{3}R_{21}\psi_{10}(+)$
28 _{1/2}	α	1/2	$R_{20}\psi_{00}$ (+)
-, C	β	-1/2	$R_{20}\psi_{00}$ (+)

TABLE VIII

n = 2 Hydrogen Atom Wave Functions in a Magnetic Field

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NOTATION

(+) and (+) are electron spinors

$$R_{20} = \frac{1}{\sqrt{2}} e^{-\frac{3}{2}gr} (1 - \frac{1}{2}gr)$$
$$R_{21} = \frac{1}{2\sqrt{6}} r e^{-\frac{3}{2}gr}$$

 $\psi_{11} = -\sqrt{\frac{3}{8\pi}} \sin\theta e^{i\phi}$ $\psi_{10} = \sqrt{\frac{3}{4\pi}} \cos\theta$ $\psi_{1-1} = \sqrt{\frac{3}{8\pi}} \sin\theta e^{-i\phi}$

$$\psi_{OO} = \int_{\frac{1}{4\pi}}^{\frac{1}{2}}$$

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TABLE IX

Field (G)	ξ	⁶ +	٥_	ε _l	٤2	ε ₃	٤ ₄
0	0	× • 3333	3333	1	1	1	1
390	.05	.3833	2833	1.016	.983	1.034	.967
780	.1	.4333	2333	1.031	.965	1.068	•935
3,900	•5	.8333	1666	1.117	.872	1.113	.712
7,800	1,0	1.3333	+.6666	1.167	.563	1.538	• 525
39,000	5.0	5.3333	4.6666	1.220	.122	1.724	.152
78,000	10.0	10.3333	9.6666	1.224	.084	1.730	.111

Factors Required for the Computation of the Hydrogen Atom Wave Functions in an Arbitrary Magnetic Field

interaction. The magnetic fields of interest are in the region of 500-600 G. The parameter which defines the strong and weak field regions (with respect to the hyperfine interaction) is $X \cong \mu_B / \Delta W$, where ΔW corresponds to the zero field hyperfine splitting. The magnetic field at which X is unity varies from ~15 to ~65 G for the cases of present interest (see Table I) and we are thus interested in the strong field region as far as the hyperfine interaction is concerned. This means that the appropriate wave functions which include the nuclear spin are of the form given in Table VIII multiplied by a nuclear spin wave function which corresponds to a particular m_{τ} . (These are only approximately correct wave functions; in fact, a small amount of nuclear spin component of other than the predominant m_{τ} value will be present. The situation is analagous to the situation discussed above for the fine structure wave functions, if \vec{F} , \vec{J} , and \vec{I} replace \vec{J} , \vec{L} , and \vec{S} . The α -d crossing technique¹⁰ discussed in Section 4 makes use of this fact.)

Turning to the evaluation of the matrix elements which connect the various states, we assume that m_I is a good quantum number; i.e., that we may use electron wave functions of the form given in Table VIII multiplied by a nuclear spinor. The selection rule $\Delta m_I = 0$ holds for the transitions of interest so the nuclear spin wave function is omitted in the following discussion. Further, we assume that the direction of the static magnetic field defines the +z axis of the system.

We first consider the magnetic dipole matrix elements

which connect the β to the α and the f to the e states. The perturbing interaction is

$$H' = -\vec{\mu} \cdot \vec{B}' = -g_{\ell} \mu_{o} \vec{\ell} \cdot \vec{B}' - g_{g} \mu_{o} \vec{s} \cdot \vec{B}'$$

where, neglecting radiative corrections, $g_{g} = 1$ and $g_{g} = 2$, and where μ_{o} is the Bohr magneton. We may write:

$$\vec{t} \cdot \vec{B}' = \frac{1}{2} (B_X' + iB_Y') (\hat{t}_X - i\hat{t}_Y) + \frac{1}{2} (B_X' - iB_Y')$$

$$(\hat{t}_X + i\hat{t}_Y) + \frac{1}{2} \hat{t}_Z = \frac{1}{2} \hat{t}_Z + \frac$$

Using this expression together with the similar expression for $\vec{s} \cdot B'$, the $\beta \cdot \alpha$ matrix element may be written:

$$H'_{\alpha\beta} = -\mu_{o} \int R_{20} \psi_{00}^{*}(+) [\frac{1}{2}B_{+}^{*}(g_{\ell}\ell_{-} + g_{g}B_{-}) + \frac{1}{2}B_{-}^{*}(g_{\ell}\ell_{+} + g_{g}B_{+}) + B_{z}(g_{\ell}\ell_{z} + g_{g}B_{-})$$

$$R_{20}\psi_{00}(+)d\tau \quad .$$

The operators l_{+} , l_{-} , and l_{π} obey the equations¹³

$$\begin{split} & \ell_{+}\psi_{\ell m_{\ell}} = \sqrt{(\ell - m_{\ell})(\ell + m_{\ell} + 1)} \psi_{\ell m_{\ell}} + 1 , \\ & \ell_{-}\psi_{\ell m_{\ell}} = \sqrt{(\ell + m_{\ell})(\ell - m_{\ell} + 1)} \psi_{\ell m_{\ell}} - 1 , \text{ and} \\ & \ell_{z}\psi_{\ell m_{\ell}} = m_{\ell}\psi_{\ell m_{\ell}} . \end{split}$$

The operators s_{+} , s_{-} , and s_{z} obey identical equa-

TABLE .

n = 2 Electric Dipole Matrix Elements

Transition	Δm	Matrix_Element of eE · r	xE _x	Matrix Element of yE _y	zEz
α <i>→</i> a	+1	-3E_/√2	-3E _x /√2	3iE _v /√2	0
β → d	-1	3E ₊ /√2 .	3E _x /√2	3iE _y /√2	0
α → b	о	√6ε ₁ Ε _z	o	o	νσε ₁ Ε _z
β → c	0	νσε _μ ε _z	0	0	√6ε ₄ E _z
a→c	-1	√ <u>3/2</u> ε ₃ E ₊	√3/2ε ₃ ε _x	√3/2ε ₃ iE _y	0
β → b	+1	-√3/2€2E_	$-\sqrt{3/2}\epsilon_2^E x$	√3/2ε ₂ iE _y	0
α→d	-2	o	0	0	0
β → a	+2	o	0	о	0
α → e	o	−√3ε ₂ E _z	о	о	$-\sqrt{3}\epsilon_2 E_z$
β→f	o	+√3ε ₃ ε _z	о	0	+√3ε ₃ E _z
a → f	-1	-√3ε ₄ E ₊	-√3ε ₄ E _x	$-\sqrt{3}\epsilon_{4}iE_{y}$	0
β → e	+1	-√3ε ₁ Ε_	-√3ε _l E _x	√3ε _l iE _y	0
	1	1			ł

ea.

tions (where s = 1/2, $m_s = \pm 1/2$). In spinor notation, only the following operations yield non-zero results:

$$s_{+}(+) = (+)$$

$$s_{-}(+) = (+)$$

$$s_{-}(+) = \frac{1}{2}(+)$$

$$s_{-}(+) = -\frac{1}{2}(+)$$

For the present example, the l_{+} , l_{-} , and l_{z} operators yield zero and the only contribution to the integral is from the $\frac{1}{2}g_{s}B_{-}^{I}S_{+}$ term. We thus obtain $H_{\alpha\beta}^{I} = -\frac{1}{2}g_{s}\mu_{O}B_{-}^{I} = -\mu_{O}B_{-}^{I}$. In the notation of Section 5 this corresponds to $M = -\mu_{O}B_{x}^{I}/\hbar$ or $M = -i\mu_{O}B_{y}^{I}/\hbar$ for oscillating fields in the x and y directions, respectively.

The matrix element connecting f to e can be similarly evaluated; the result is:

$$H_{ef}' = [-g_{\ell}(\epsilon_2 \epsilon_4 + \epsilon_1 \epsilon_3)/3 + g_{e_1} \epsilon_2 \epsilon_3/6] \mu_0 B_1'$$

For the magnetic fields of interest here, ε_1 , ε_2 , ε_3 , and ε_4 are very near unity. If it is assumed that they are exactly unity, we have

$$H_{ef}' = -\mu_0 B_{-}'/3$$

(This limiting result could have been readily obtained by considering the effective interaction to be $-g_{2P_{1}}\mu_{0}\vec{J}\cdot\vec{B}$ ' together with the Jm_{J} representation of the state.) In the notation of Section 5, this result corresponds to M' = $-\epsilon\mu_{0}B_{X}/3\hbar$ or M' = $-i\epsilon B_{y}/3\hbar$ for oscillating fields in the x and y directions, respectively, where ϵ is given by:

$$\varepsilon = g_{\ell}(\varepsilon_2 \varepsilon_4 + \varepsilon_1 \varepsilon_3) - g_{\mu} \varepsilon_2 \varepsilon_3/2$$
.

We note that $\varepsilon \approx 1$ for field strengths of present interest. Numerically the quantity μ_0/\hbar is 2π times (1.401) MHz/G. Note that M and M' have units of angular frequency.

We now turn to the electric dipole matrix elements. In this case the perturbing part of the Hamiltonian is of the form $H' = e\vec{E} \cdot \vec{r}$ where e is the electronic charge, \vec{E} an electric field strength, and \vec{r} is the electron position vector.

For example, the matrix element which causes the

transition $\alpha \rightarrow e$ may be written

$$H'_{e\alpha} = \int [\epsilon_2 R_{21} \psi_{10}^{*}(+) + \epsilon_1 R_{21} \psi_{11}^{*}(+)] [e\vec{E} \cdot \vec{r}]$$

$$R_{20} \psi_{00}(+) d\tau \quad .$$

Noting the orthonormality of the electron spinors and expanding $e\vec{E} \cdot \vec{r}$, this becomes

$$H_{e\alpha}^{i} = \epsilon_{2} e \int R_{21} \psi_{10}^{*} [\frac{1}{2}E_{+}x_{-} + \frac{1}{2}E_{-}x_{+} + E_{z}z] R_{10} \psi_{00} d\tau$$

If we use the following facts

$$z = r\cos\theta$$
$$x_{+} = r\sin\theta e^{i\phi}$$
$$x_{-} = r\sin\theta e^{-i\phi}$$
$$d\tau = r^{2}\sin\theta d\theta d\phi$$

we obtain

$$\begin{split} H'_{\alpha e} &= \varepsilon_2 e \int_0^{\infty} R_{21}(r) R_{20}(r) r^3 dr \int_0^{2\pi} \int_0^{\pi} \psi_{10}^* \\ & (E_z \cos\theta + \frac{1}{2} E_{+} \sin\theta e^{-i\phi} + \frac{1}{2} E_{-} \sin\theta e^{i\phi}) \psi_{00} \sin\theta d\theta d\phi. \end{split}$$

The radial integral¹³ has the value $3\sqrt{3}a_{0}$, where a_{0} is the Bohr radius. The angular integrals can be evaluated either directly or by reference to tables.¹³ In this case, only $E_{z}\cos\theta$ survives the ϕ integration, and we obtain

$$H'_{\alpha e} = -\sqrt{3}\epsilon_2 e a_0 E_z$$
.

In Table X the matrix elements are given with the assumption of the Condon-Shortley¹⁴ conventions for the vector coupling coefficients and wave functions. Any modification of sign in which ε_1 and ε_3 , or ε_2 and ε_4 are changed simultaneously, or in which the overall phase of a wave function is changed, preserves the orthogonality and eigenvalues of the functions and is therefore acceptable. Thus, for the $2S_{1/2} - 2P_{1/2}$ transitions, many possible consistent sets of signs for the matrix elements are possible.

In the notation of Section 5, the electric dipole matrix elements may be written

$$R = -\sqrt{3}\varepsilon_2 e_0 E_z$$

$$R' = \sqrt{3}\varepsilon_3 e_0 E_z$$

and

$$V = -\sqrt{3}\varepsilon_1 e a_0 E_x \text{ or } -\sqrt{3}\varepsilon_1 e a_0 i E_y$$
$$V' = -\sqrt{3}\varepsilon_1 e a_0 E_x \text{ or } \sqrt{3}\varepsilon_1 e a_0 i E_y$$

depending on whether the transverse field is along the x or y axis. For the magnetic fields of interest, $\varepsilon_1 - \varepsilon_4$ differ from unity by only a few percent. Neglecting these small differences, we may write

$$R^{1} = -R^{*}$$
 and $V^{1} = V^{*}$

This form is used in some of the later discussion. In fact, any relative signs between the matrix elements such that $\arg(R/V) = -\arg(R'*/V'*)$ will result in identical answers for any calculation which involves only these matrix elements.

Numerically, the quantity $\sqrt{3}$ ea_o/ħ is given by $\sqrt{3} \times (1.60206 \times 10^{-19} \text{ C}) \times (5.29172 \times 10^{-9} \text{ cm}) \times 10^{7}/(1.05443 \times 10^{-27} \text{ erg-sec}) = 13.9257 \text{ (cm/V)} \text{ MHz}.$ Note that the quantity $\sqrt{3}$ ea_oE/ħ, where E is an electric field strength (V/cm), has the units of angular frequency.

7. ANALYTIC SOLUTION OF THE THREE-LEVEL PROBLEM For the case of interest, where the magnetic field is such that the β and e levels are nearly degenerate, the f level has little effect on the system. Thus, to good approximation, we may neglect its presence. (The quality of this approximation will be examined in Section 8.)

The equations which characterize the three-level system are then

$$i \overset{i}{a} = \frac{1}{2}M^{*} b e^{i \delta t} + \frac{1}{2}R^{*} c e^{i(\delta + \omega_{\beta e})t}$$
$$i \overset{i}{b} = \frac{1}{2}M a e^{-i \delta t} + V^{*} c e^{i \omega_{\beta e}t}$$
$$i \overset{i}{c} = \frac{1}{2}R a e^{-i(\delta + \omega_{\beta e})t} + V b e^{-i\omega_{\beta e}t} - \frac{1}{2}(i\gamma c) ,$$

where we have defined the angular frequency difference $\delta = \omega_{\alpha\beta} - \omega$.

Let us first consider the easily-solved special case which corresponds to $\delta = 0$ and $\omega_{\beta e} = 0$. In other words, we assume a magnetic field strength such that the β and e levels are degenerate (crossing) and an rf frequency such that $\omega/2\pi = \omega_{\alpha\beta}/2\pi$ (resonance). Note that we are speaking of a particular nuclear spin magnetic quantum number, since

simultaneous resonance and crossing occur at a different magnetic field (and corresponding frequency) for the various m_I values. We also neglect M (for the reasons given in Section 6).

With these assumptions the equations become

If one differentiates the third of these equations and substitutes the first two equations into the third, the result is

$$\ddot{c} + \frac{1}{2}\gamma \dot{c} + P^2 \dot{c} = 0$$

where $P^2 = \frac{1}{2}R^*R + V^*V$. The general solution of this equation is

$$c = C_1 e^{-\mu_1 t} + C_2 e^{-\mu_2 t}$$

where μ_1 and μ_2 are the two roots of $\mu^2 - \frac{1}{2}\gamma\mu + p^2 = 0$:

$$\mu_{1,2} = \gamma/4 \pm \sqrt{(\gamma/4)^2 - P^2}$$
.

To evaluate the constants, we assume some initial conditions. For a particle initially in its α -state, a = 1 and b = c = 0 at t = 0; this implies that $\dot{c} = \frac{1}{2}$ iR at t = 0. Applying these conditions, we obtain:

$$c = \frac{iR}{4\eta} \begin{pmatrix} e^{-\mu_{l}t} & e^{-\mu_{2}t} \\ e^{-\mu_{l}t} & e^{-\mu_{2}t} \end{pmatrix},$$

where $\eta = \sqrt{(\gamma/2)^2 - p^2}$. This solution is valid for all values of P^2 except the critically damped case $p^2 = (\gamma/2)^2$; for this case $c = \frac{-iR}{2} te^{-(\gamma/4)t}$. The solutions for c may be put back into the equations for a and b to obtain

$$a = A_3 + -\frac{3}{2}iR*\int cdt$$

$$b = B_3 + -iV*\int cdt$$

where A_3 and B_3 are integration constants. We obtain:

$$a = 1 - \frac{R^*R}{4p^2} + \frac{R^*R}{8n} \left(\frac{e^{-\mu_2 t}}{\mu_2} - \frac{e^{-\mu_1 t}}{\mu_1} \right)$$

$$\mathbf{b} = -\frac{\mathbf{V}^{\mathbf{H}_{\mathrm{R}}}}{2\mathbf{P}^{2}} + \frac{\mathbf{V}^{\mathbf{H}_{\mathrm{R}}}}{\mathbf{\mu}_{\mathrm{R}}} \begin{pmatrix} -\mu_{2}\mathbf{t} & -\mu_{1}\mathbf{t} \\ \frac{\mathbf{e}}{\mu_{2}} & -\frac{\mathbf{e}}{\mu_{1}} \end{pmatrix}$$

After a sufficiently long time the exponential terms decay to zero, since the real parts of μ_1 and μ_2 are positive for all values of P^2 . Thus, our asymptotic solutions are

 $a \rightarrow \frac{V^*V}{1 p + p} + \frac{V^*V}{1 + p + p}$

$$b \Rightarrow \frac{-\frac{1}{2}V^{*}R}{\frac{1}{2}R^{*}R + V^{*}V}$$

That is, an equilibrium population of the α and β states is established. Since we are dealing with amplitudes, a definite phase relation exists between a and b; i.e., we have a coherent mixture of the α and β states, while the amplitude for the e state has decayed to zero.

We note that our asymptotic solutions satisfy the condition $\frac{1}{3}Ra + Vb = 0$. From inspection of the equations, it is clear that we have a solution if $c = \dot{c} = 0$. The physical nature of the phenomenon is one of interference; the relative phase of the transition matrix elements is such that contributions from a and b to the c state population destructively interfere; i.e., $\frac{1}{3}Ra + Vb = 0$.

We now turn to the solution of the general threelevel equations following the method indicated by Lamb.⁸ First, let us generalize the equations slightly to allow for an arbitrary phase for the rf field at t = 0. That is, we assume

$$H' = H' = hR \cos(\omega t + \delta_0),$$

where δ_0 is the phase at t = 0. This may be written as

$$\frac{1}{2} [\hbar(\mathrm{Re}^{i\delta_{O}})e^{i\omega t} + \hbar(\mathrm{Re}^{-i\delta_{O}})e^{-i\omega t}].$$

We may perform a similar decomposition of M. Dropping the negative frequency term, as before, and de $i\delta_0 = R_0$ and Me = M₀, the equations remain the same except R \Rightarrow R₀ and M \Rightarrow M₀:

23,

$$i\dot{a} = R_{O}^{*} c e^{i(\delta + \omega_{\beta}e^{i})t} + \frac{1}{2}M_{O}^{*} b e^{i\delta t}$$

$$i\dot{b} = V^{*} c e^{i\omega_{\beta}e^{t}} + \frac{1}{2}M_{O} a e^{-i\delta t}$$

$$i\dot{c} = R_{O} a e^{-i(\delta + \omega_{\beta}e^{i})t} + V b e^{-i\omega_{\beta}e^{t}}$$

$$-\frac{1}{2}(i\gamma c) .$$

Following Lamb,⁸ we assume a solution of the form $-\mu_{1}t$ $-\mu_{2}t$ $-\mu_{2}t$

$$a = A_{1}e^{-\mu} + A_{2}e^{-\mu} + A_{3}e^{-3}$$

$$b = (B_{1}e^{-\mu_{1}t} + B_{2}e^{-\mu_{2}t} + B_{3}e^{-\mu_{3}t})e^{-i\delta t}$$

$$c = (C_{1}e^{-\mu_{1}t} + C_{2}e^{-\mu_{2}t} + C_{3}e^{-\mu_{3}t})e^{-i\delta t - i\omega_{\beta}e^{t}}.$$

Substituting this form into the equations and equating coefficients of $e^{-\mu_{\perp}t}$, for example, we obtain

$$\begin{bmatrix} i\mu_{1} & M_{O}^{*} & R_{O}^{*} \\ M_{O} & i\mu_{1}-\delta & V^{*} \\ R_{O} & V & i\mu_{1}-\delta-\omega_{\beta}e^{-i_{2}i\gamma} \end{bmatrix} \begin{bmatrix} A_{1} \\ B_{1} \\ C_{1} \end{bmatrix} = 0,$$

with identical equations holding for μ_2 and μ_3 . We use the general subscript k from here on since the following discussion applies to μ_1 , μ_2 , and μ_3 . For any but the trivial solution $A_k = B_k = C_k = 0$, the determinant of the coefficients must vanish; thus, the three values of μ are the roots of the complex cubic equation:

$$\begin{split} & i\mu_{k}(i\mu_{k} - \delta)(i\mu_{k} - \delta - \omega_{\beta e} - \frac{1}{2}i\gamma) \\ & + (M_{O}^{*}V^{*}R_{O} + M_{O}VR_{O}^{*}) - R_{O}R_{O}^{*}(i\mu_{k} - \delta) \\ & - VV^{*}(i\mu_{k}) - M_{O}M_{O}^{*}(i\mu_{k} - \delta - \omega_{\beta e} - \frac{1}{2}i\gamma) = 0 \; . \end{split}$$

This may be written in the form

$$\mu_{k}^{3} + P\mu_{k}^{2} + Q\mu_{k} + R = 0$$
,

where

$$P = -1(\Delta_{\alpha\beta} + \Delta_{\alphae})$$

$$Q = V*V + \frac{1}{4}(R^*_{O}R_{O} + M^*_{O}M_{O}) - \Delta_{\alpha\beta}\Delta_{\alphae}$$

$$R = 1(M^*_{O}V*R_{O} + M_{O}VR^*_{O} - \frac{1}{4}(R^*_{O}R_{O}\Delta_{\alpha\beta} + M^*_{O}M_{O}\Delta_{\alphae}),$$

and where $\Delta_{\alpha\beta} = -\delta$ and $\Delta_{\alpha e} = -\delta - \omega_{\beta e} - \frac{1}{2}i\gamma$. Such a complex cubic equation may be solved algebraically as follows. Define $\mu_{k} = z + P/3$. The equation for z is then $z^3 + az + b$ where $a = Q - P^2/3$ and b = $2P^3/27 - PQ/3 + R$. Then a solution for z is of the form $z = u - \frac{a/3u}{a}$, where u satisfies the equation $u^3 = -b/2 \pm \sqrt{(b/2)^2 + (a/3)^2}$. All the operations defined are valid for complex numbers; however, we find six values for u of which three lead to redundant solutions. To improve computation precision, we select the + or - sign in the equation for u³ according to which gives the larger absolute value. It was found necessary to use doubleprecision arithmetic to achieve satisfactory accuracy for the values of the coefficients of interest to the present problem. The FORTRAN IV code for this procedure is included in Appendix A.

Returning to the matrix equation, once we know that the determinant of the coefficients is zero, we may use any two equations to relate the quantities B_k and C_k to A_k , which we will assume to be arbitrary. (That is, A_1 , A_2 , and A_3 will be taken to be the three independent constants characteristic of the solution of a system of three first-order differential equations.) One finds

$$\begin{split} B_{k} &= -\frac{1}{2} A_{k} [M_{o}(i\mu_{k} - \delta - \omega_{\beta e} - \frac{1}{2}i\gamma) - R_{o}V^{*}]/D_{k} \\ C_{k} &= -\frac{1}{2} A_{k} [R_{o}(i\mu_{k} - \delta) - M_{o}V]/D_{k} , \end{split}$$

where

$$D_{\mathbf{k}} = (i\mu_{\mathbf{k}} - \delta - \omega_{\beta \mathbf{e}} - \lambda_{\mathbf{i}} \mathbf{i}\gamma)(i\mu_{\mathbf{k}} - \delta) - \mathbf{V} \mathbf{*} \mathbf{V} .$$

Thus, defining $B_k = \epsilon_k A_k$ and $C_k = \delta_k A_k$, our general solution of the equations is of the form

$$\begin{bmatrix} a \\ b \\ c \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ \epsilon_1 & \epsilon_2 & \epsilon_3 \\ \delta_1 & \delta_2 & \delta_3 \end{bmatrix} \begin{bmatrix} -\mu_1 t \\ A_1 e \\ -\mu_2 t \\ A_2 e \\ -\mu_3 t \\ A_3 e \end{bmatrix}$$

To evaluate the coefficients A_1 , A_2 , and A_3 , it is necessary to assume some initial conditions. If there is no e-state component in the initial beam, we may achieve sufficient generality by assuming each of the initial conditions a = 1, b = 0, c = 0and a = 0, b = 1, c = 0. The solution to the problem corresponding to a beam which contains an incoherent mixture of α -state atoms and β -state atoms can then be written by combining these solutions appropriately (i.e., by an average over initial states). We could use some other set of spinors as a basis system; a natural basis system for this problem will be discussed later. For a = 1, b = 0, and c = 0 at t = 0, the solution of the linear equations yields

$$\begin{aligned} \mathbf{A}_{1} &= \left(\epsilon_{2} \delta_{3} - \epsilon_{3} \delta_{2} \right) / \mathbf{D} \\ \mathbf{A}_{2} &= \left(\epsilon_{3} \delta_{1} - \epsilon_{1} \delta_{3} \right) / \mathbf{D} \\ \mathbf{A}_{3} &= \left(\epsilon_{1} \delta_{2} - \epsilon_{2} \delta_{1} \right) / \mathbf{D} \end{aligned}$$

where

$$D = (\epsilon_2 \delta_3 - \epsilon_3 \delta_2) + (\epsilon_3 \delta_1 - \epsilon_1 \delta_3) + (\epsilon_1 \delta_2 - \epsilon_2 \delta_1).$$

For a = 0, b = 1, and c = 0 at t = 0 we obtain

$$A_{1} = (\delta_{2} - \delta_{3})/D$$
$$A_{2} = (\delta_{3} - \delta_{1})/D$$
$$A_{3} = (\delta_{1} - \delta_{2})/D$$

The present solutions have been evaluated numerically by computer methods (Appendix A). In summary, the assumptions made in obtaining these solutions are:

- a) the three-level approximation equations are adequate,
- b) R_o, V, and M_o are constant during the interaction time,
- c) the effect of the $e^{-i\omega t}$ term (the Bloch-Siegert term) is small.

These restrictions will be relaxed in the numerical integration results to be described later.

We note that the initial phase of the rf field plays no role in the solutions. Accordingly, we will refer to R and M, not R and M, in most of the following discussion. The coefficients A_k , B_k , and C_k are slowly varying functions of the angular frequency difference $\delta = \omega_{\alpha\beta} - \omega$. The character of the variation of A_3 and B_3 , the coefficients of the most slowly decaying term, depends on the sign and magnitude of $\omega_{\beta e}$ at the magnetic field for which δ = 0; i.e., to the difference between the resonance and crossing frequencies. Figure 5 shows the modulus and argument of A_3 for $m_1 = 0$ deuterium atoms, as a function of B - B₀ (where B₀ = B(δ = 0)), or $\delta/2\pi$, for the following 3 cases:

Case	ω/2π (MHz)	B _o (G)	ω _{βe} /2π	R _o (MHz)	V (MHz)
l	1471.90	525	89.95	250	250
2	1611.99	575	-1.57	250	250
3	1752.09	625	-92.53	250	250

The numerical values of the matrix elements $(|R_o| = 250 \text{ MHz} \text{ and } |V| = 250 \text{ MHz}$) correspond to a longitudinal rf field of 250/(13.93 x .975) = 18.41 V/cm and to a transverse static field of 250/(13.93 x 1.021) = 17.58 V/cm. The particular frequencies chosen correspond to a resonance ~50 G below crossing, approximately at crossing, and ~50 G above crossing. (The exact field for which $\omega_{\beta e} =$ 0 for $m_{I} = 0$ deuterium atoms is 574.14 G, for which $\omega_{\alpha\beta}/2\pi = 1609.57 \text{ MHz.}$) Since the line shape depends only on $\omega_{\beta e}/2\pi$, the curves in Figures 5-8 apply to any of the hydrogen, deuterium, or tritium



Fig. 5. The variation of $|A_3|$ (solid curves) and arg A_3 (dashed curves) for cases 1, 2, and 3. One of the $|A_3|$ curves is terminated at -8 G where Re (μ_2) becomes smaller than Re (μ_3) .



Fig. 6. The variation of $|B_3|$ (solid curves) and arg B_3 (dashed curves) for cases 1, 2, and 3. One of the $|B_3|$ curves is terminated at 8.5 G, and a second curve at -8 G, where Re (μ_2) becomes smaller than Re (μ_3).



Fig. 7. The variation of the real part (solid curves) and imaginary part (dashed curves) of μ_3 (in MHz angular frequency) for cases 1, 2, and 3.

substates. However, the values of $\omega/2\pi$ and B_o given above are specifically for m_I = 0 deuterium atoms. Since, for a given fixed frequency, $\omega_{\beta e}$ will be different for the different substates of the species being polarized, the line shape corresponding to each will be slightly different. The cases 1 and 3 chosen for illustration are probably a little too far from crossing for reasonable separation of deuterium magnetic substates; a range of ±35 G from the crossing field would appear to be



Fig. 8. The "transmission" $|a|^2$ (upper three curves) and $|b|^2$ (lower three curves) evaluated at t = 0.4 µsec, for cases 1, 2, and 3.

acceptable. For hydrogen or tritium atoms, where the line shape is of little consequence, a much larger difference is acceptable.

Figure 6 shows the modulus and argument of B_3 as a function of $B - B_0$ or $\delta/2\pi$, for the same three cases. Note that the slopes of the $|A_3|$ and $|B_3|$ curves are opposite in sign for a given ω_{Re} .

Figure 7 shows the real and imaginary parts of the small decay constant μ_3 , as a function of B - B_o or $\delta/2\pi$, for the same cases. Figure 8 shows the transmission $|a|^2$ and $|b|^2$ after a time t = 0.4 µsec (12 cm). At a time as large as this, only the μ_3 terms survive, so

$$|\mathbf{a}|^2 = |\mathbf{A}_3^{e^{-\mu}3^t}|^2$$

and

$$|b|^2 = |B_3^{e^{-\mu_3^t}}|^2$$
.

The opposite shift in the apparent resonant field for $|\mathbf{a}|^2$ and $|\mathbf{b}|^2$ transmission is because of the opposite slopes of the $|\mathbf{A}_3|$ and $|\mathbf{B}_3|$ curves noted above.

It is relevant to inquire about the transmission of

TABLE XI

1. Transmission of Unselected Substates

R / V	$\frac{1}{2} \mathbf{R} ^{2} + \mathbf{V} ^{2}$]a ₃]	Re (µ3)
	Units: (125 MHz) ² Angular Frequency	-	(µsec ⁻¹)
0.5	2	1.03	5.3
1.0	2	1.15	20.1
1.5	2	1.39	43.2
0.5	5	.98	5.5
1.0	5	.90	17.4
1.5	5	•75	26.5
0.5	10	•95	3.3
1.0	10	.81	9.3
1.5	10	.68	13.2

2. Transmission of the Selected Substate

R / V	A ₃
0.5 1.0 1.5	0.9412 0.8000 0.6400

atoms with other than the desired m_T quantum number. For hydrogen or tritium atoms, this may easily be made zero. For deuterium atoms, some care must be taken in the choice of parameters. If the optimum driving frequency of 1609.57 MHz is chosen, the transmission curves for $m_{T} = 1$, 0, and -1 are highly symmetric and therefore almost identical. The relevant quantity is the transmission of a given state when the magnetic field is tuned to an adjacent state. For example, for $\omega/2\pi = 1609.57$ MHz, the resonant fields for $m_T = 1, 0$, and -1 deuterium atons are 564.48, 574.14, and 583.96 G. In the case of $m_T = 0$ deuterium atom selection, we are interested in the transmission of $m_T = 1$ and $m_T = 3$ atoms at 574.14 G; i.e., at 9.56 G above and at 9.82 G below their respective resonant fields. The relative contributions from either of these may be determined from Table XI. Thus, for |R| = |V| = 250MHz, the fractional contamination of $m_{T} = 0$ states with $m_{\tau} = 1$ states would be $|0.90e^{-17.4t}/.80|^2$ which, for $t = 0.4 \mu sec$, is about 10⁻⁶. For other driving frequencies the selection is less favorable; however, as mentioned above, the selection would appear to be reasonably satisfactory for a frequency range of ~±100 MHz (corresponding to ~±35 G). The quality of the selection in these cases can be estimated

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from Figures 5-7.

We now write simpler expressions for the special case of resonance ($\delta = 0$). As noted above, the coefficients do not vary rapidly, so some statements about the general nature of the solutions at resonance will apply approximately to the offresonance solutions. We neglect the small matrix element M. For this case, the cubic equation becomes

$$\mu^{3} - (\gamma/2 - i\omega_{\beta e})\mu^{2} + P^{2}\mu = 0$$
,

where $P^2 = \frac{1}{4}RR^* + VV^*$ as before. The roots are $\mu_{1,2} = (\gamma/4 - i\omega_{\beta e}/2) \pm \sqrt{(\gamma/4 - i\omega_{\beta e}/2)^2 - P^2}$

which are seen to be consistent with the solutions obtained above for ω_{Be} = 0.

Inserting these values for the $\boldsymbol{\mu}_k$ in the general relations, we obtain

$$\varepsilon_{k} = +\lambda_{2}RV^{*}/D_{k}$$

nd
$$\delta_{k} = -\lambda_{2}iR\mu_{k}/D_{k}$$

where

 $\mu_3 = 0$,

$$D_{k} = i\mu_{k}(i\mu_{k} - \omega_{\beta e} - i\gamma/2) - v*v$$
$$= -\mu_{k}^{2} + 2\mu_{k}(\gamma/4 - i\omega_{\beta e}/2) - v*v$$

If we define $\xi = (\gamma/4 - i\omega_{\beta e}/2)$ and $\eta = \sqrt{(\gamma/4 - i\omega_{\beta e}/2)^2 - P^2}$ we can tabulate the D_k , ε_k , and δ_k as follows:

k 	<u> </u>	D	ε <u>k</u>	⁶ k
l	ξ + η	R#R/4	2V*/R	-2i(ξ + η)/R
2	ξ — η	R*R/4	2 V*/ R	-2i(ξ - η)/R
3	0	-V*V	-R/2V	0

The determinant D may be written

$$D = -\frac{8iV^*\eta}{R^*R^*} (1 + \frac{R^*R}{4V^*V}) ,$$

For the initial condition a = 1, b = 0, c = 0, we obtain the coefficients

$$\frac{k}{1} \quad \frac{A_k}{\frac{R^*R}{8P^2} \left(1 - \frac{\xi}{\eta}\right)} \quad \frac{B_k}{\frac{RV^*}{4P^2} \left(1 - \frac{\xi}{\eta}\right)} \quad \frac{\frac{1R}{\frac{1R}{4\eta}}}{\frac{1R}{4\eta}}$$

$$2 \quad \frac{R^*R}{8P^2} \left(1 + \frac{\xi}{\eta}\right) \quad \frac{RV^*}{4P^2} \left(1 + \frac{\xi}{\eta}\right) \quad -\frac{1R}{4\eta}$$

$$3 \quad \frac{V^*V}{P^2} \quad -\frac{RV^*}{2P^2} \quad 0$$

For large times, the solutions are therefore

$$a \rightarrow \frac{V^*V}{P^2}$$
 $b \rightarrow \frac{-RV^*}{2P^2}$

Note that a and b have asymptotic values identical to those obtained if $\omega_{\beta e} = 0$; thus, only the transient terms are affected by $\omega_{\beta e} \neq 0$ for $\delta = 0$.

For frequencies slightly off resonance, neglecting the slight variation of the coefficients, we have

$$a \approx \frac{V^*V}{p^2} e^{-\mu_3 t}$$
 $b \approx \frac{-RV^*}{2p^2} e^{-(\mu_3 + i\delta)t}$,

where μ_3 is a rapidly varying function of δ (see Figure 7).

For the initial conditions a = 0, b = 1, c = 0, we obtain the solutions

$$\frac{k}{1} \quad \frac{A_k}{\frac{R^*V}{4p^2} (1 - \frac{\xi}{\eta})} \quad \frac{B_k}{\frac{V^*V}{4p^2} (1 - \frac{\xi}{\eta})} \quad \frac{C_k}{\frac{1V}{2\eta}}$$

$$\frac{R^*V}{4p^2} (1 + \frac{\xi}{\eta}) \quad \frac{V^*V}{2p^2} (1 + \frac{\xi}{\eta}) \quad -\frac{1V}{2\eta}$$

$$3 \quad -\frac{R^*V}{2p^2} \quad \frac{R^*R}{4p^2}$$

From the symmetry of the equations, one can see that the relation between the sets of coefficients for the two assumed initial conditions must involve only the simultaneous interchange of R/2 with V and the definition of $A_{\rm w}$ with that of $B_{\rm w}$.

In general, the roots of the cubic equation are complex. The imaginary components correspond to (time dependent) energy shifts from the unperturbed eigenenergies characterizing the wave functions given in Table VIII. Consider, for illustrative purposes, the situation at crossing and resonance

.

where

$$\mu_{1,2} = \gamma/4 \pm \sqrt{(\gamma/4)^2 - P^2} , \mu_3 = 0.$$

It is clear that if $P^2 < (\gamma/4)^2$, all the roots are real and the unperturbed energies remain correct. If, however, $P^2 > (\gamma/4)^2$, μ_1 and μ_2 will have an imaginary component and the level energies will be shifted. This is related to the phenomena of level repulsion in which, under certain circumstance, the energies of two states as a function of magnetic field do not cross, but rather repel, and thus interchange roles.⁸ This effect does not result in a shift of the position of the three-level resonance. however, since this is determined solely by the frequency at which $Re(\mu_3) = 0$, and this frequency will correspond* to $\delta = 0$ for any value of ω_{Re} or p^2 . For $\delta \neq 0$, μ_3 has an imaginary component (see Figure 7) and the slowly decaying states α and β may be regarded as slightly energy-shifted. The energy shift of the rapidly decaying components has no significance at large times.

Figures 9-11 illustrate the time dependence of $|\mathbf{a}|^2$ and $|\mathbf{b}|^2$ for the cases 1, 2, and 3 defined above (initial conditions $\mathbf{a} = 1$, $\mathbf{b} = 0$, and $\mathbf{c} = 0$). Figure 9 corresponds to resonance ($\delta = 0$), Figure 10 corresponds to 1 G off resonance ($\delta/2\pi = 2.8$ MHz), and Figure 11 corresponds to 9.6 G off resonance ($\delta/2\pi = 26.9$ MHz). The last value is chosen for presentation since 9.6 G is approximately the difference in magnetic field values at which the various deuterium magnetic substates resonate.

Figure 12 illustrates the time dependence of $|a|^2$ and $|b|^2$ at resonance ($\delta = 0$) for the cases 1, 2, and 3 but for the initial conditions a = 0, b = 1, and c = 0.

Figures 13-15 show the transmission of hydrogen metastable atoms versus magnetic field for an rf field of fixed frequency and strength (here taken to be 1610 MHz and 18.41 V/cm, respectively) and for several values of the transverse field (8.79,

*As has been noted above, the apparent resonant frequency sometimes differs slightly from $\delta = 0$. This is due only to the slow variation of the coefficients $|A_3|$ and $|B_3|$ with frequency, and is unrelated to the energy shifts presently under discussion.





Fig. 9. The variation of $|a|^2$ and $|b|^2$ vs time for $B = B_0 (\delta = 0)$ with initial conditions a(0) = 1, b(0) = c(0) = 0 for cases 1, 2, and 3.

Fig. 11. The variation of $|a|^2$ and $|b|^2$ vs time for B - B₀ = -9.6 G ($\delta/2\pi \approx 26.9$ MHz) with initial conditions a(0) = 1, b(0) = c(0) = 0 for cases 1, 2, and 3.



Fig. 10. The variation of $|a|^2$ and $|b|^2$ vs time for B - B₀ = -1 G ($\delta/2\pi \approx 2.8$ MHz) with initial conditions a(0) = 1, b(0) = c(0) = 0 for cases 1, 2, and 3.



Fig. 12. The variation of $|a|^2$ and $|b|^2$ vs time for B = B₀ (δ = 0) with initial conditions b(0) = 1, a(0) = c(0) = 0 for cases 1, 2, and 3.



Fig. 13. The transmission of hydrogen metastable atoms $(|a|^2 + |b|^2 \text{ and } |a|^2)$ vs magnetic field for 1610 MHz; |R| = 250 MHz, and |V| = 125 MHz. The solid curves correspond to initial condition a(0)= 1 and the dashed curves correspond to b(0) = 1.



Fig. 14. The transmission of hydrogen metastable atoms $(|a|^2 + |b|^2 \text{ and } |a|^2)$ vs magnetic field for 1610 MHz; |R| = 250 MHz, and |V| = 250 MHz. The solid curves correspond to initial condition a(0)= 1 and the dashed curves correspond to b(0) = 1.

17.58, and 26.37 V/cm). The peaks at different magnetic field strengths correspond, of course, to different nuclear spin substates. An interaction time of 0.4 µsec (corresponding to a cavity length 12 cm) is assumed. The solid curves correspond to an ini-



Fig. 15. The transmission of hydrogen metastable atoms $(|a|^2 + |b|^2 \text{ and } |a|^2)$ vs magnetic field for 1610 MHz; |R| = 250 MHz, and |V| = 375 MHz. The solid curves correspond to initial condition a(0) = 1 and the dashed curves correspond to b(0) = 1.

tial pure alpha-state beam (a(0) = 1) and the dashed curves correspond to a pure beta-state beam (b(0) = 1). For the highly symmetric case $(\frac{1}{2}|\mathbf{R}| =$ $|\mathbf{V}|$) shown in Figure 13, the two initial conditions result, except in the "tail" region, in identical solutions. The quantities $|\mathbf{a}|^2 + |\mathbf{b}|^2$ and $|\mathbf{a}|^2$ are plotted in each case.

Figures 16-18 show the transmission of deuterium metastable atoms for the same cases and conditions.

Several observations about the general nature of the solutions may be made from the graphs:

- 1. For fixed |R|, both the height and width of the lines which correspond to a a(0) = l increase with increasing |V|. (For fixed |V|, the height and width of the peaks which correspond to b(0) = l increase with increasing |R|, although this is not shown here.) The heights, of course, vary in the manner stated previously, and depend only on |R|/|V|. For the case ½|R| = |V|, the a(0) = l and b(0) = l solutions become nearly identical. This result is apparent from the symmetry of the equations.
- From Figures 9-11, one can see that the width of the resonance lines must decrease monotonically as the interaction time in-



Fig. 16. The yield of deuterium metastable atoms $(|a|^2 + |b|^2 \text{ and } |a|^2)$ vs magnetic field for 1610 MHz; |R| = 250 MHz, and |V| = 125 MHz. For this case, curves corresponding to initial condition a(0) = 1 and to b(0) = 1 are identical.



Fig. 17. The yield of deuterium metastable atoms $(|a|^2 + |b|^2 \text{ and } |a|^2)$ vs magnetic field for 1610 MHz; |R| = 250 MHz, and |V| = 250 MHz. The solid curves correspond to initial condition a(0) = 1 and the dashed curves to b(0) = 1.

creases. The curves shown in Figures 13-18 are for t = 0.4 µsec, which corresponds to a cavity length of 12 cm for a beam with the velocity of interest (30 cm/µsec).

3. The separation of metastable hydrogen or



Fig. 18. The yield of deuterium metastable atoms $(|a|^2 + |b|^2 \text{ and } |a|^2)$ vs magnetic field for 1610 MHz; |R| = 250 MHz, and |V| = 375 MHz. The solid curves correspond to initial condition a(0) = 1 and the dashed curves to b(0) = 1.

tritium atoms with different nuclear spin orientations appears to be very easy in the sense that the parameters may vary over a wide range. However, for metastable deuterium atoms, if one uses too large a field strength, the width of the lines will be too large. Thus, the minimum cavity length appears to be ~ 6 cm for deuterium atoms, but could be shorter for hydrogen or tritium atoms. (This is because $|\mathbf{R}|/|\mathbf{V}|$ must be held constant to achieve a given transmission at resonance. Since $|V| < |V|_{max}$ is required, $|R| < |R|_{max}$ is also required. But the decay constants corresponding to the unwanted nuclear spin states are approximately proportional to |R|; this implies $\ell > \ell_{\min}$ where ℓ is the cavity length.)

For an incident unpolarized beam of metastables (i.e., 1/2 of beam in the α state, 1/2 in the β state) the transmission at resonance of the "spin filter" is exactly 50%, as may be verified from Figures 9 and 12 and from Figures 13-18. This follows from the expressions already derived which are repeated here in a matrix form:

$$\begin{pmatrix} \mathbf{a}(\mathbf{t} + \mathbf{\omega}) \\ \\ \\ \mathbf{b}(\mathbf{t} + \mathbf{\omega}) \end{pmatrix} = \frac{1}{\mathbf{p}^2} \begin{pmatrix} \mathbf{V}^*\mathbf{V} & -\frac{\mathbf{R}^*\mathbf{V}}{2} \\ -\frac{\mathbf{R}\mathbf{V}^*}{2} & \frac{\mathbf{R}^*\mathbf{R}}{4} \end{pmatrix} \begin{pmatrix} \mathbf{a}(0) \\ \\ \mathbf{b}(0) \end{pmatrix} .$$

The initial beam may be regarded as an incoherent mixture of α and β states although the final beam is a coherent mixture. If we average over initial and sum over final states, we find

$$|a(t + \infty)|^{2} + |b(t + \infty)^{2} = \frac{1}{2}|a(0)|^{2} + \frac{1}{2}|b(0)|^{2};$$

i.e., 50% of an (electron) unpolarized beam is quenched.

We next consider the physical nature of the states which are transmitted through the spin filter.

As a first step we eliminate the explicit time dependence by defining the new variables

$$A = ae^{-i(\omega_{\alpha} - \omega)t}$$

$$A = ae^{-i\omega_{\beta}t}$$

$$B = be^{-i\omega_{\beta}t}$$

$$C = ce^{-i\omega_{\beta}t}$$

The equations for these new variables are found to be

$$\begin{split} \mathbf{i}\mathbf{A} &= (\omega_{\alpha} - \omega)\mathbf{A} + \frac{1}{2}\mathbf{R}^{*}\mathbf{C} \\ \mathbf{i}\mathbf{B} &= \omega_{\beta}\mathbf{B} + \mathbf{V}^{*}\mathbf{C} \\ \mathbf{i}\mathbf{C} &= \frac{1}{2}\mathbf{R}\mathbf{A} + \mathbf{V}\mathbf{B} + (\omega_{e} - \frac{1}{2}\mathbf{i}\gamma)\mathbf{C} \quad . \end{split}$$

We choose $\omega_{\beta} = 0$ (which we may do since the energy scale is arbitrary) and define as usual $\delta = \omega_{\alpha\beta} - \omega$. The equations and definitions are then

$$i\dot{A} = \delta A + \frac{1}{2}R*C$$

$$i\dot{B} = V*C$$

$$i\dot{C} = \frac{1}{2}RA + VB - (\omega_{\beta e} + \frac{1}{2}i\gamma)C$$

$$A = ae^{-i\delta t}$$

$$B = b$$

$$C = ce^{+i\omega_{\beta}e^{t}}$$

Let us define the spinors r and s, with amplitudes p and q, as follows:

$$\mathbf{r} = \frac{1}{P} \left(\frac{1}{2} \mathbf{R}^* \alpha' + \mathbf{V}^* \beta \right)$$
$$\mathbf{s} = \frac{1}{P} \left(\mathbf{V} \alpha' - \frac{1}{2} \mathbf{R} \beta \right)$$

where the spinor $\alpha' = \alpha e^{\pm i \delta t}$. The total wave function, neglecting the e state (i.e., for $t \neq \infty$) is then of the form $\psi = a\alpha + b\beta \equiv (ae^{-i\delta t})\alpha e^{i\delta t} + b\beta \equiv A(\alpha e^{i\delta t}) + B\beta \equiv A\alpha' + B\beta$. Notice that r and s are orthonormal. We can invert the definitions of r and s to find:

,

$$\alpha^{i} = \frac{1}{P} \left(\frac{1}{2}Rr + V *_{B} \right)$$
$$\beta = \frac{1}{P} \left(Vr - \frac{1}{2}R *_{S} \right) .$$

Substituting these expressions into the definition of ψ :

$$\psi = pr + qs \equiv A\alpha' + B\beta$$

we obtain:

$$p = \frac{1}{P} (J_{2}RA + VB) \qquad A = \frac{1}{P} (J_{2}R^{*}p + Vq)$$

$$q = \frac{1}{P} (V^{*}A - J_{2}R^{*}B) \qquad B = \frac{1}{P} (V^{*}p - J_{2}Rq)$$

We now derive the differential equations for p and q:

$$i \dot{p} = PC + \frac{R\delta A}{2P}$$

$$i \dot{q} = \frac{V * \delta A}{P}$$

$$i \dot{C} = Pp - (\omega_{\beta e} + \frac{1}{2} i \gamma)C .$$

If we specialize to resonance ($\delta = 0$) these equations become

$$i\dot{p} = PC$$

 $i\dot{q} = 0$
 $i\dot{C} = Pp - (\omega_{\beta e} + \frac{1}{2}i\gamma)C$.

The variables may be further separated as follows:

$$-\ddot{p} = P(i\ddot{C}) = P(Pp - i(\omega_{\beta e} + \frac{1}{2}i\gamma)C)$$
$$= P^{2}p + (\frac{1}{2}\gamma - i\omega_{\beta e})\dot{p}$$

$$-\ddot{C} = P(i\dot{p}) - i(\omega_{\beta e} + \frac{1}{2}i\gamma)\dot{C} = P^2C + (\frac{1}{2}\gamma - i\omega_{\beta e})\dot{C}$$

Thus our three equations are

$$\ddot{\mathbf{p}} + (\mathbf{k}_{\mathbf{2}\mathbf{Y}} - \mathbf{i}\omega_{\beta \mathbf{e}})\dot{\mathbf{p}} + \mathbf{P}^{2}\mathbf{p} = 0$$
$$\dot{\mathbf{q}} = 0$$
$$\ddot{\mathbf{c}} + (\mathbf{k}_{\mathbf{2}\mathbf{Y}} - \mathbf{i}\omega_{\beta \mathbf{e}})\dot{\mathbf{c}} + \mathbf{P}^{2}\mathbf{C} = 0$$

These equations have the solutions

$$p = p_1 e^{-\mu_1 t} + p_2 e^{-\mu_2 t}$$
$$q = q_1$$
$$c = c_1 e^{-\mu_1 t} + c_2 e^{-\mu_2 t}$$

where $\mu_{1,2} = (\gamma/4 - i\omega_{\beta e}/2) \pm \sqrt{(\gamma/4 - i\omega_{\beta e})^2 - P^2}$; i.e., μ_1 and μ_2 are the two large decay constants defined earlier. For times of interest to us, therefore:

$$p \neq 0$$
$$q = q_1$$
$$c \neq 0$$

Thus the amplitude of the spinor s is conserved while the amplitude of r decays exactly as does the amplitude of e.

Let us momentarily allow an arbitrary initial phase; i.e., we put, once again, $R = R_0$. In spinor notation, for $\delta = 0$, r and s may be written

$$\mathbf{r} = \frac{R_{20}\psi_{00}}{P} \begin{pmatrix} \lambda_{\mathbf{s}R_{0}^{*}e} e^{-i\omega_{\alpha}t} \\ -i\omega_{\beta}t \end{pmatrix}$$
$$\mathbf{s} = \frac{R_{20}\psi_{00}}{P} \begin{pmatrix} v e^{-i\omega_{\alpha}t} \\ -\lambda_{2}R_{0}e^{-i\omega_{\beta}t} \end{pmatrix}$$

The expectation values of the Pauli operators for these states are tabulated below:

	r	8
<"x>	$\varepsilon_{\downarrow} \cos(\omega_{\alpha\beta} t + \Delta)$	$-\varepsilon_{\perp}\cos(\omega_{\alpha\beta}t + \Delta)$
<°y>	$\varepsilon_{\perp} \sin(\omega_{\alpha\beta} t + \Delta)$	$-\epsilon_{\perp}\sin(\omega_{\alpha\beta}t + \Delta)$
<"z>	ε _{ll}	-ε _μ

In the above table, $e^{i\Delta} = R_0 V^* / |R_0 V^*|$, $\epsilon_{\perp} = |R_0 V^*| / P^2$, and $\epsilon_{\parallel} = (\frac{1}{4}R_0^*R_0 - V^*V)/P^2$. Thus the spinors r and s point opposite directions at all times, make an angle of $\theta = \tan^{-1} \frac{\epsilon_{\perp}}{\epsilon_{\parallel}}$ with respect to the z axis, and rotate with the Larmor frequency $\omega_{\alpha\beta}/2\pi$. The phase of the rotation is such that the direction of r is parallel and s antiparallel to the direction of the transverse field at the time the longitudinal rf field has its maximum positive value. (This can be most easily seen by considering the static transverse field to define the x axis, so that R_0 and V are both real.)

From this formulation we can again conclude that 50% of an (electron) unpolarized beam will survive the spin filter, since in that case a given particle has a 50% probability of being in either of any two orthonormal spin states, including the r and s states defined above.

We note that our resulting metastable beam has both 100% electron polarization (rotating) and 100% nuclear polarization, and that the relative direction of the electron spin can be varied. Further, the phase of the electron spin rotation is related to the cavity rf phase.

8. THE FOUR-LEVEL PROBLEM

We now consider the effect of the f-level on the solutions previously discussed. Qualitatively, it is clear that the transverse electric field will induce quenching through the α - f transition and the longitudinal rf electric field will induce quenching through the β - f transition.

The four-level equations were stated in Section 5. The frequency dependent quantities which enter into these equations are

$$e^{i\omega_{\alpha}e^{t}} \cos \omega t = \frac{i(2\omega_{\alpha}\beta + \omega_{\beta}f - \delta)t}{2e}$$
$$i(\omega_{\beta}e^{t} + \delta)t$$
$$+ \frac{i(\omega_{\beta}e^{t} + \delta)t}{2e}$$

and

$$e^{i\omega_{\beta}f}\cos\omega t = \frac{i(\omega_{\alpha}f - \delta)t}{2e} + \frac{i(\omega_{\beta}f - \omega_{\alpha\beta} + \delta)t}{2e}$$

where $\delta = \omega_{\alpha\beta} - \omega$ as before. The first of these expressions, as noted in the discussion of the three-level system, may be approximated (near $\delta =$ 0) by the second term alone. For the second of these expressions, on the other hand, the two terms are of roughly equal importance. Thus the simplest equations which reasonably describe the four level system are:

$$i \overset{i(\omega_{\beta e} + \delta)t}{=} \overset{i\omega_{\alpha f}t}{+} V \overset{i\omega_{\alpha f}t}{=} V \overset{i\omega_{\beta e}t}{=} - \overset{i\omega_{\beta f}}{=} cos(\omega_{\alpha \beta} - \delta)t$$

$$i \overset{i}{=} \overset{-i(\omega_{\beta e} + \delta)t}{=} + V \overset{-i\omega_{\beta e}t}{=} \overset{-i\omega_{\beta f}t}{=} cos(\omega_{\alpha \beta} - \delta)t ,$$

$$i \overset{i}{=} V \overset{*}{=} \overset{-i\omega_{\alpha f}t}{=} - \overset{i\omega_{\beta f}t}{=} cos(\omega_{\alpha \beta} - \delta)t ,$$

where we have put $\mathbb{R}^{\prime} = -\mathbb{R}^{*}$ and $\mathbb{V}^{\prime} = \mathbb{V}^{*}$ in accordance with Table X and the discussion in Section 6. Note that these relations hold only in the zero field limit; i.e., if ε_{1} , ε_{2} , ε_{3} , and $\varepsilon_{4} \neq 1$. All fourlevel calculations presented here are based on this assumption. Note also that an arbitrary initial phase cannot be included in the four-level case by putting $\mathbb{R} = \mathbb{R}_{0}$ as was done in Section 7. The initial phase is, however, of no importance.

We first consider the quenching of α states by a transverse electric field with no rf longitudinal field present (i.e., R = 0). The equations above then separate into two independent pairs of which the α - f pair is

$$i\dot{a} = Vde^{-i\omega_{\alpha}f^{t}}$$
$$i\dot{d} = V^{*}ac^{-i\omega_{\alpha}f^{t}} - \frac{1}{2}i\gamma d$$

These equations are easily solved if one assumes

$$a = A_{1}e^{-\mu_{1}t} - \frac{\mu_{2}t}{A_{2}e}$$

$$d = (D_{1}e^{-\mu_{1}t} + D_{2}e^{-i\omega_{\alpha}t})e^{-i\omega_{\alpha}t}$$

One finds that μ_1 and μ_2 are the roots of

$$\mu^{2} + 2\xi\mu + |V|^{2} = 0$$

where

$$\xi = \gamma/4 - i\omega_{\alpha}r/2$$

Thus we may write $\mu_{1,2} = \xi \pm \eta$ where $\eta = \sqrt{\xi^2 - |V|^2}$. For the initial condition a(0) = 1, d(0) = 0, the general solution for a is found to be

$$\mathbf{a} = \frac{1}{2}(1 - \frac{\xi}{\eta})e^{-(\xi + \eta)t} + \frac{1}{2}(1 + \frac{\xi}{\eta})e^{-(\xi - \eta)t}$$

If
$$|\xi|^2 \gg |V|^2$$
, we may approximate n by
 $\eta = \xi - \frac{|V|^2}{2\xi}$.

The expression for a becomes

$$a \approx \frac{|v|^2}{4\xi^2} e^{-2\xi t} + e^{-(\frac{|v|^2}{2\xi})t}$$
.

The first term has a small coefficient and rapid decay constant; for times of interest, we may write

$$|a|^2 \approx e^{-(\gamma^{\alpha f})t}$$
, $\gamma^{\alpha f} = \frac{\gamma |V|^2}{\omega_{\alpha f}^2 + (\gamma/2)^2}$

which is the Stark quenching formula given by Lamb and Retherford.⁵ Similar results are obtained for the β - e quenching:

$$|\mathbf{b}|^2 \approx e^{-(\gamma^{\beta e})t}$$
, $\gamma^{\beta e} = \frac{\gamma |v|^2}{\omega_{\beta e}^2 + (\gamma/2)^2}$

and for the α - e quenching:

$$|a|^2 \approx e^{-(\gamma^{\alpha e})t}$$
, $\gamma^{\alpha e} = \frac{\gamma |R|^2/4}{(\omega_{\alpha e} - \omega)^2 + (\gamma/2)^2}$

This result is not applicable to the β - f quenching, however. It should also be noted that for the field strength of present interest, the expansion of n used above will not be valid for the β - e case if $\omega_{\beta e}$ is small or zero.

Thus, for a atoms in the presence of both rf and static electric fields, we would expect an effective decay constant of the order of, but greater than, $\gamma^{\alpha f}$. The situation is complicated, however, since the various contributions to the decay are coherent.

An analytic solution at $\delta = 0$ is possible if $i\omega_{\alpha}f^{t}$ $i\omega_{\alpha}f^{t}$ $i\omega_{\alpha}f^{t}$. As already noted, this is not a good approximation; however, it at least partially takes into account the $\beta - f$ interaction and is included here primarily for the physical insight that it may afford. To obtain this solution, we first eliminate the oscillating time dependence with the substitution

$$A = ae^{-i\delta t}$$

$$B = b$$

$$C = ce^{i\omega}\beta e^{t}$$

$$D = de^{i(\omega_{\alpha f} - \delta)t}$$

The equations for these variables are

$$\begin{bmatrix} i\dot{A} \\ i\dot{B} \\ = \begin{bmatrix} \delta & 0 & \frac{1}{2}R^{*} & \gamma \\ 0 & 0 & V^{*} & -\frac{1}{2}R \\ \vdots \\ i\dot{C} \\ i\dot{D} \end{bmatrix} \begin{bmatrix} \delta & 0 & \frac{1}{2}R^{*} & \gamma \\ 0 & V^{*} & -\frac{1}{2}R \\ V^{*} & -\frac{1}{2}R & 0 \\ V^{*} & -\frac{1}{2}R^{*} & 0 & -(\omega_{\alpha f} - \delta + \frac{1}{2}i\gamma) \end{bmatrix} \begin{bmatrix} A \\ B \\ C \\ D \end{bmatrix}.$$

In terms of the previously defined amplitudes p and q, we can derive

$$\begin{split} \mathbf{\dot{p}} &= \mathbf{R}\delta A/2\mathbf{P} + \mathbf{PC} \\ \mathbf{\dot{q}} &= \mathbf{V} * \delta A/\mathbf{P} + \mathbf{PD} \\ \mathbf{\dot{c}} &= \mathbf{Pp} - (\omega_{\beta \mathbf{e}} + \frac{1}{2}\mathbf{i}\gamma)\mathbf{C} \\ \mathbf{\dot{D}} &= \mathbf{Pq} - (\omega_{\alpha \mathbf{f}} - \delta + \frac{1}{2}\mathbf{i}\gamma)\mathbf{D} \end{split} \right\} P^{2} &= \frac{1}{2}\mathbf{R} * \mathbf{R} + \mathbf{V} * \mathbf{V} \quad . \end{split}$$

At resonance ($\delta = 0$) the equations reduce to the two coupled pairs

> ip = PC $i\tilde{C} = Pp - (\omega_{\beta e} + \frac{1}{2}i\gamma)C$,

and

$$i\dot{D} = Pq - (\omega_{\alpha f} + \frac{1}{2}i\gamma)C$$

from which it follows that

ig = PD

$$\begin{vmatrix} \ddot{p} + 2\xi_{\beta e}\dot{p} + p^{2}p = 0 \\ \ddot{c} + 2\xi_{\beta e}\dot{c} + p^{2}c = 0 \end{vmatrix}$$

$$\xi_{\beta e} = \gamma/4 - i\omega_{\beta e}/2$$

and

$$\left\{ \begin{array}{c} \mathbf{\hat{q}} + 2\xi_{\alpha \mathbf{f}} \mathbf{\hat{q}} + \mathbf{P}^2 \mathbf{q} = 0 \\ \mathbf{\hat{b}} + 2\xi_{\alpha \mathbf{f}} \mathbf{\hat{b}} + \mathbf{P}^2 \mathbf{D} = 0 \end{array} \right\} \qquad \xi_{\alpha \mathbf{f}} = \gamma/4 - i\omega_{\alpha \mathbf{f}}/2$$

 $-\mathbf{u}_{-}\mathbf{t}_{-}$

Thus

w

$$p = p_1 e^{-1} + p_2 e^{-2}$$
where $\mu_{1,2} = \xi_{\beta e} \pm \sqrt{\xi_{\beta e}^2 - p^2}$
and

-u t

$$q = q_1 e^{-\mu_1^{\dagger}t} + q_2 e^{-\mu_2^{\dagger}t}$$

where $\mu_{1,2}^{\dagger} = \xi_{\alpha f} \pm \sqrt{\xi_{\alpha f}^2 - P^2}$

The quantities μ_1 and μ_2 are recognized as the two larger decay constants discussed in the three-level case; thus, for times of interest, $p \rightarrow 0$. However, $\xi_{\alpha f} >> P^2$ for the present region of interest, so we may expand the square root (as before) to obtain

$$\mu_{1}' \approx 2\xi = \gamma/2 - i\omega_{\alpha f}$$
$$\mu_{2}' \approx P^{2}/2\xi = P^{2}/(\gamma/2 - i\omega_{\alpha f})$$

The μ_1^{\prime} term decays rapidly, so for times of interest

$$q \approx q_2 e^{-(p^2/2\xi)t}$$
.

Our initial conditions are A(0) = 1, B(0) = C(0) =D(0) = 0. Now

$$q(0) = \frac{1}{P} (V^*A(0) - \frac{1}{2}R^*B(0)) = \frac{V^*}{P}$$

and

$$\dot{q}(0) = \frac{1}{P} (V^* \dot{A}(0) - \frac{1}{2} R^* \dot{B}(0)) = 0$$
,

where the latter condition follows from the differential equations. These conditions yield

$$q_2 = \frac{\xi + \eta}{2\eta} \frac{V^*}{P} \approx \frac{V^*}{P} .$$

Thus, for large times,

$$p \neq 0; q \neq \frac{V^*}{P} e^{-(P^2/2\xi)t}$$



Fig. 19. The line shape as calculated with various approximations. The upper curves correspond to $|a|^2$ and the lower curves to $|b|^2$. The curves marked 1 correspond to the three-level theory. The curves marked 2 show the effect of inclusion of both terms of cos wt in the three-level theory. The curves marked 3 correspond to the approximate four-level theory in which $e^{\beta r}$ cos wt is

 $i(\omega_{\alpha f} - \delta)t$ $i\omega_{\alpha e}t$ $i(\omega_{\beta e} + \delta)t$ replaced by e and e cos $\omega t \rightarrow e$. The curves marked 4 correspond to the exact solutions of the four-level problem.

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Inserting these into the definition of A and B, we obtain

$$A = \frac{1}{P} (\frac{1}{2}R^*p + Vq) + \frac{|V|^2}{P^2} e^{-(P^2/2\xi)t}$$
$$B = \frac{1}{P} (V^*p - \frac{1}{2}Rq) + \frac{-RV^*}{2P} e^{-(P^2/2\xi)t}$$

In the three-level case, for large time, we obtained

$$A + \frac{|v|^2}{p^2} \qquad B + \frac{-Rv^*}{2P}$$

Thus, both $|A|^2$ and $|B|^2$ are altered only by a multiplicative factor $e^{-\gamma^{\alpha f_t}}$ where

$$\gamma^{\alpha f} = \frac{\gamma P^2}{\omega_{\alpha f}^2 + (\gamma/2)^2}, \quad P^2 = \frac{1}{2} |R|^2 + |V|^2$$

A point worth noticing with respect to these solutions is that only the state with amplitude q (the s state) is coupled directly to the f state. That is, if the e level were not present, the α -f- β interaction, in this approximation, would select the r state and quench the s state. This is exactly the opposite to the situation for the α -e- β interactions; thus this contribution from the f level is destructive.

In Figure 19 the line shape obtained by numerical integration, with various approximations, is shown. The calculation is for the case of $m_{I} = 0$ deuterium atoms at the (nearly) optimum frequency of 1611.99 MHz (which corresponds to $B_{o} = 575$ G). The parameters are |R| = |V| = 250 MHz. We note that, as expected, the curve which corresponds to the ($\delta = 0$) analytic solution given above gives a result about midway between the three-level and the four-level results.

In Figure 20 the exact four-level results for the loss (at resonance) of $|a|^2$ are shown for various parameters and for the same frequency and magnetic field as above. These curves represent the ratio of $|a|^2$ (at 0.25 µsec) to the three-level equilibrium value $(|a_0|^2)$ which would obtain in the absence of the f level. The dashed curve represents the prediction of the approximate four-level analytic solution given above. Note that this predicted value depends only on $k_1 |\mathbf{R}|^2 + |\mathbf{V}|^2$. The



Fig. 20. The ratio of $|a|^2$ to $|a_0|^2$, where $|a_0|^2$ is the three-level equilibrium value of $|a|^2$, for $B_0 = 575$ G. The points are calculated from the exact four-level theory; the curves are visual fits to the points. The dashed curve represents the prediction obtained from the (approximate) four-level analytic solutions.

ratios vary approximately linearly with the interaction time t. The ratio of $|b|^2$ to $|b_0|^2$ is, for this case, indistinguishable from the ratio of $|a|^2$ to $|a_0|^2$.

Figure 21 shows the time dependence of the solutions, at $\delta = 0$, for the conditions used in Figure 19. Note that the inclusion of the antiresonant term in the three-level theory (the Bloch-Siegert correction term) results in a decay from the threelevel equilibrium solution of about 2%/µsec.

Figure 22 shows the line shape for a frequency of 1508.326 MHz. Again the calculation is for $m_I = 0$ deuterons (for which this particular frequency corresponds to $B_0 = 538$ G) and for |R| = |V| = 250 MHz. Note the shift of the peaks from the resonant field.

Figure 23 shows the loss through the f state, for a frequency 1508.326 MHz and field 538 G (m_I = 0 deuterium atoms), for a variety of parameters $|\mathbf{R}|$ and $|\mathbf{V}|$. In this case, unlike that shown in Figure 20, the ratios $|\mathbf{a}|^2/|\mathbf{a}_0|^2$ and $|\mathbf{b}|^2/|\mathbf{b}_0|^2$ are not identical. Further, the loss through the f level appears to be somewhat greater. However, as may be seen by comparing Figures 19 and 22, the peak positions are shifted in the latter case, and therefore $\delta = 0$ does not, in general, correspond to maximum transmission. If both $|\mathbf{a}|^2$ and $|\mathbf{b}|^2$ transmission



Fig. 21. The time dependence of the amplitudes $|\mathbf{a}|^2$ and $|\mathbf{b}|^2$, at $\delta = 0$, for various approximations. The curves are labeled as in Fig. 19.

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Fig. 22. The line shape as calculated with various approximations. The curves are labeled as in Fig. 19. Note the shift of the peaks from the resonant field (see arrows).



Fig. 23. The lower graph shows the ratio of $|a|^2$ to $|a_0|^2$, where $|a_0|^2$ is the three-level equilibrium value of $|a|^2$, for $B_0 = 538$ G. The upper graph shows the ratio of $|b|^2$ to $|b_0|^2$ for these conditions.

are of interest (see Section 9) the value of δ which results in maximum transmission of $|a|^2 + |b|^2$ will depend on the parameters. (This is true since the $|a|^2$ and $|b|^2$ curves are shifted in opposite directions for $\omega_{\beta e} \neq 0$, and the relative contribution of $|a|^2$ and $|b|^2$ to the total transmitted beam depends on $|\mathbf{R}|/|\mathbf{V}|$.) Thus the curves given in Figure 23 predict greater loss, in general, than would be obtained by choosing an optimum value of δ .

Finally, calculations show that the three-level and four-level results agree to within $\sim 10\%$, for a wide range of parameters, in the tail region. Thus, the transmission of the unselected substates is adequately described by the results given in Table XI. The transmission of the selected substate can, however, be improved by the field shaping technique to be described in Section 9. 9. ADIABATIC VARIATION OF THE ELECTRIC FIELDS In the preceding discussion, we have assumed that the various applied fields are constant throughout the spin filter. If this condition is not met, we must resort to numerical techniques to solve even the three-level equations, although some general features of the solutions may be deduced from the form of the equations.

For application to a practical polarized ion source, the optimum transmission of the desired nuclear spin substate can be achieved if (a) the static electric field is constant, and (b) the rf field increases slowly from zero at the entrance of the spin filter to a maximum near the center and then decreases to zero at the exit.

It was shown in Section 7 that, in three-level approximation, exactly 50% of an (electron) unpolarized H^{2S} beam with the desired m_{I} value could be transmitted through a combination of static transverse and longitudinal rf electric fields. In a practical ion source, however, the β component of the atomic beam will almost certainly be quenched by the required "sweep" fields long before it reaches the spin filter. In addition, any β component which emerges from the filter will probably be quenched before reaching the argon exchange cell. For the parameters $|\mathbf{R}| = |\mathbf{V}| = 250$ MHz, for example, only 64% of an initially pure α beam would emerge from the spin filter in an α state, so that only about 1/3 of the initially produced unpolarized beam would be available at the argon exchange cell. (Note that we are referring always to the beam component with the desired m_{I} value; thus, in terms of the total atomic beam the 1/3 given above becomes 1/6 for hydrogen or tritium beams and 1/9 for deuterium beams.)

If the fields are shaped as indicated above, it is possible, in the three-level approximation, to achieve 100% transmission for a pure a beam. A spin filter with such field shaping will have 0% transmission for a β beam and thus will still have 50% transmission for an (electron) unpolarized beam. This is indicated in Figure 24 for a space variation of the rf field strength of the form $\sin(\frac{\pi z}{z_0})$ where z is the distance from the entrance to the rf region and z₀ is the total length of the rf region. For this example |V| is assumed to have the constant



Fig. 24. The quantities $|a|^2 + |b|^2$ and $|a|^2$ vs time as a metastable beam (a(0) = 1) traverses a cavity whose rf strength varies as $\sin(\pi z/z_0)$, where $z_0(= 30 \text{ cm})$ is the total length of the cavity. These curves correspond to $\delta/2\pi = 0$, $|\mathbf{R}|_{max} = 250$ MHz, and to a constant static electric field such that |V| = 250 MHz.

value 250 MHz and $|\mathbf{R}|_{max} = 250$ MHz. The results of both three-level and four-level theory are shown. (The deviation from 100% of the transmission which corresponds to three-level theory arises solely from the inclusion of both frequency terms in the expansion of $\cos(\omega t)$, while the discussion above is based on the assumption $\cos \omega t \cong \frac{1}{2}e^{i\omega t}$. All results presented in Figures 24 and 25 are based on calculations which include both terms of $\cos \omega t$.)

These results can be understood as follows. For simplicity, consider the special case of resonance $(\delta = 0)$ and crossing $(\omega_{\beta e} = 0)$. The three-level equations are then, as noted in Section 7:

 $ia^{*} = \frac{1}{2}R*c$ $ib^{*} = V*c$

 $ic = \frac{1}{2}Ra + Vb - \frac{1}{2}(i\gamma c)$.

Also as noted in Section 7, it is evident that one possible solution of these equations is

$$a = a_{0}, b = b_{0}, c = 0$$



Fig. 25. The quantities $|a|^2 + |b|^2$ and $|a|^2$ vs time for various rates of increase and decrease of of the rf field strength. The rising and falling portions of the rf field have the shape $\sin^2(t\pi/2\tau)$. The curves numbered 1-7 correspond to $\tau = 0.2$, 0.1, 0.05, 0.025, 0.00125, 0.000625, and 0.0 µsec, respectively. For all curves $\delta/2\pi = 0$ and |R| = |V|= 250 MHz. Note the decrease in the overall decay rate when the rf field is turned off.

where the constants a and b are related by

$$\frac{1}{2}Ra + Vb = 0$$

or, equivalently

$$a_0/b_0 = -2V/R$$
.

(These are, in fact, the equilibrium solutions previously discussed.) If $|\mathbf{R}| \neq 0$, the equilibrium solution will correspond to a pure a state. If $|\mathbf{R}| \rightarrow 0$ all nuclear substates are equivalent and no selection would occur. However, if |R| is increased sufficiently gradually, so that the condition ¹₂Ra + Vb = 0 can be followed adiabatically, the nuclear spin selection can be made without loss. At this point, the amplitude which describes a particle in the beam will be a coherent mixture of a and β states. If |R| is then slowly decreased to zero, the α and β mixture will be transformed back into a pure a state. Thus there are two important aspects to the field shaping: (a) a slow rise of |R| prevents loss from occuring through the excitation of "transients" as the beam enters the cavity,

and (b) a slow fall of |R| transforms the mixed α and β state back into the more stable pure α state. If no quenching between the rf region and the argon exchange region were likely to occur, the second part of the field shaping would be unnecessary. It is evident that the important parameter in these arguments is |R|/|V|, so that an exactly constant |V| is not required.

The above can also be expressed in terms of the r and s spinors defined in Section 7. We recall that

$$\mathbf{s} = \frac{1}{P} \left(\mathbf{V} \boldsymbol{\alpha} - \frac{1}{2} \mathbf{R} \boldsymbol{\beta} \right)$$

and has the constant amplitude q_1 . In terms of a and b, for $\delta = 0$,

$$q = q_1 = \frac{1}{P} (V^* a - \frac{1}{2} Rb)$$

Thus, if $|\mathbf{R}| \neq 0$, s $\neq \alpha$ and $q(t) = q_0 = a(0) = 1$. If $|\mathbf{R}|$ is increased sufficiently gradually, the state s will be conserved and therefore a particular $\alpha + \beta$ mixture will be formed. If $|\mathbf{R}|$ is then decreased sufficiently gradually, it will again be conserved and the mixture state will be transformed back into a pure α state.

It remains to determine what is meant by "sufficiently gradually." In Figure 25 the results for various assumed rise times for the rf field are presented. The exact four-level theory was used for these calculations. We assume a 30 cm overall path (velocity = 30 $cm/\mu sec$) and that only the static electric field acts over the last 15 cm. The rising and falling portions of the rf field is assumed to have the shape $\sin^2(t\pi/2\tau)$. The rf field is fully turned off at t = 0 and at t = 0.5 usec. The various curves are labeled with the parameter τ and in each case the upper curve represents $|a|^2 + |b|^2$, and the lower curve $|a|^2$. It is seen that no loss occurs for the case $\tau = 0.2$ µsec. At the steepest part of the $\sin^2(t\pi/2\tau)$ curve, the fractional rate of change in $|\mathbf{R}|$ is π/τ . For $\tau = 0.2$ µsec, $\pi/\tau \cong$

15.7 x 10^6 sec^{-1} . Since the Larmor frequency is around 1600 x 10^6 sec^{-1} , $|\mathbf{R}|$ changes about 1% in a Larmor cycle. Thus, we have demonstrated that a satisfactory criterion for adiabaticity is that the strength of the rf field may change no more than about 1% per cycle. This is about the value that one would expect.

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REFERENCES

- G. G. Ohlsen and J. L. McKibben, Bull. Am. Phys. Soc. <u>12</u>, 463 (1967).
- J. L. McKibben, G. G. Ohlsen, and R. R. Stevens, Bull. Am. Phys. Soc. <u>12</u>, 463 (1967).
- B. L. Donnally, T. Clapp, W. Sawyer, and M. Schulz, Phys. Rev. Letters <u>12</u>, 502 (1964).
- 4. B. L. Donnally and W. Sawyer, Phys. Rev. Letters <u>15</u>, 439 (1965).
- Willis E. Lamb, Jr., and Robert C. Retherford, Phys. Rev. <u>81</u>, 222 (1951).
- R. T. Robiscoe and B. L. Cosens, Phys. Rev. Letters <u>17</u>, 69 (1966).
- R. T. Robiscoe and B. L. Cosens, Bull. Am. Phys. Soc. <u>11</u>, 62 (1966).
- 8. Willis E. Lamb, Jr., Phys. Rev. 85, 259 (1952).
- C. W. Drake and R. Krotkov, Phys. Rev. Letters <u>16</u>, 848 (1966).
- 10. M. Leventhal, Physics Letters 20, 625 (1966).
- 11. B. Donnally, Bull. Am. Phys. Soc. <u>12</u>, 509 (1967).
- F. Bloch and A. Siegert, Phys. Rev. <u>57</u>, 522 (1940).
- H. A. Bethe and E. E. Salpeter, <u>Handbuch der</u> <u>Physik</u>, Vol. 35, p. 88 (Springer-Verlag, Berlin, 1957).
- 14. E. U. Condon and G. H. Shortley, <u>The Theory of Atomic Spectra</u> (Cambridge University Press, London, 1953).

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APPENDIX A. A COMPUTER PROGRAM FOR EVALUATING THE ANALYTIC SOLUTION OF THE THREE-LEVEL EQUATIONS

A FORTRAN IV program which evaluates the solutions developed in Section 7 is given in this appendix. The version given computes the squared amplitudes $|a|^2$, $|b|^2$, $|c|^2$, and $|a|^2 + |b|^2$ as a function of time for a set of fixed driving frequencies and for fixed magnetic field. The modulus and phase of a, b, and c are also given. Other versions of the program exist in which time is held constant while the variation of the above quantities with magnetic field at fixed frequency, or with frequency at fixed magnetic field, is studied.

The input for the program is as follows:

Card 1 (FORMAT 6 F12.6)

- XSPIN spin of nucleus (i.e., ½ or 1)
- GJ g_{T} value for the 2S_k states (\geq 2)
- XMU magnetic moment of the nucleus (in nuclear magnetons)
- DELW zero magnetic field hyperfine splitting for the $2S_{\frac{1}{2}}$ state (MHz)
- GJP g_J value for the $2P_{\lambda_2}$ states ($\equiv 2/3$) DELWP zero magnetic field hyperfine splitting for the $2P_{\lambda_2}$ states (MHz)

(The radiative correction to the g_J value is supplied by the subroutine BREIT and should not be included in GJ and GJP.)

Card 2 (FORMAT 6 F12.6)

FREQMN	minimum applied frequency (MHz)
FREQDL	increment in applied frequency (MHz)
FREQMX	maximum applied frequency (MHz)
TF	maximum time at which solutions are to
	be evaluated (µsec)

DELT increment in time at which solutions are to be evaluated (TF/DELT should not exceed 500)

```
BGAUSS magnetic field (G)
```

Card 3	(FORMAT 6 F12.6)	
XMM	M in MHz (angular frequency	r)

				-	
RR	R	in	MHz	(angular	frequency)

VV V in MHz (angular frequency)

where these quantities are complex and therefore appear as three pairs of numbers on the card. The real part of each quantity appears first. The relations between these units and practical units are given in the program listing.

Card 4	(FORMAT 6 I4)
IMODE	If IMODE = 1, program returns to start.
	If IMODE = 2, program returns to read
	in new Card 3 and proceeds.
ICSMN	minimum case to be calculated
ICSMX	maximum case to be calculated

where $m_{I} = 1$, 0, -1 correspond to cases 1, 2, and 3 for deuterium atoms and $m_{I} = \frac{1}{2}$, $-\frac{1}{2}$, correspond to cases 1 and 2 for hydrogen and for tritium atoms.

The program consists of a main program together with several subroutines. The function of the various subroutines is as follows:

a) SUBROUTINE CUBIC (P, Q, R, RT1, RT2, RT3) This subroutine evaluates the solutions of a cubic equation with complex coefficients of the form x^3 + Px^2 + Qx + R = 0. It uses double-precision arithmetic in order to obtain the required accuracy. The three complex roots, RT1, RT2, and RT3 are in order of decreasing real parts.

b) SUBROUTINE DPROD (XR, XI, YR, YI, ZR, ZI) This subroutine multiplies the complex numbers X and Y together to give complex Z. Double-precision arithmetic is used; thus the real and imaginary parts are carried separately.

c) SUBROUTINE DARCTAN (Y. X, Z)

This subroutine finds $Z = \arctan(Y/X)$ in the correct quadrant. Double-precision arithmetic is used.

 d) SUBROUTINE BREIT (XI, FFF, XM, GJ, GI, DELW BGAUSS, W, XGAUSS, EPS1)

This subroutine evaluates the energy of a given state according to the Breit-Rabi formula (see Section 2). The input variables are

	XT	spin of nucleus
	FFF	F quantum number
	XM	m _r quantum number
	GĴ	g _J value (atomic g factor) excluding
		radiative corrections
	GI	g _I value (nuclear g factor)
	DELW	zero magnetic field hyperfine splitting
		in MHz
	BGAUSS	magnetic field in G
'h	e output	variables are
	W	energy of state in MHz
	XGAUSS	value of the parameter X(defined in
		Section 2)

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EPS1 nuclear moment correction term ϵ_1 (in MHz; already included in W)

The output from the program is fully labeled, and includes the values of the coefficients A_k , B_k , and C_k , the decay constants μ_k , and the relevant frequencies in MHz. In addition, the three quantities F1, F2, and F3, which are the values of $\mu_k^3 + P\mu_k^2$.

+ $Q\mu_k$ + R for k = 1, 2, 3, are given. The deviation of these quantities from zero gives some idea of the accuracy with which the roots have been determined.

Tape 10 is defined as input and Tape 9 as output for the particular system for which this program was written.

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```
IIME PLOT VERSION
C
  DIVIDE R AND V BY 13.94 TO OBTAIN VOLTS/CM PEAK TO ZERO
С
 DIVIDE M BY 8.80 TO OBTAIN GAUSS PEAK TO ZERO
С
  IHAT IS, ENTER R,V, AND M IN MHZ ANGULAR FREQUENCY
С
      DIMENSION FFA(6), FFB(6). XMFA(6), XMFB(6)
      DIMENSION FARS(3), FACS(3), FBCS(3)
      DIMENSION ASQ(500), BSQ(500), CSQ(500), ABSQ(500), TIME(500)
      COMPLEX XMM, RR, VV, DELAC.P, Q, R, XMMSTR, RRSTAR, VVSTAR, XI.RT1, RT2, RT3,
     1XIMU(3), D, EPS(3), DEL(3), A(3), B(3), C(3), SUM
      COMPLEX X, F1, F2, F3, AA, BB, CC, PHASAB, PHASAC
      DOUBLE PRECISION PI
      COMMON PI
    1 FORMAT(6F12.6)
    2 FORMAT(6H A(K)= 6F9.4,7H MU(1)= 2F9.4,4H F1= 2F9.4)
3 FORMAT(6H B(K)= 6F9.4,7H MU(2)= 2F9.4,4H F2= 2F9.4)
    4 FORMAT(6H C(K)= 619.4,7H MU(3)= 2F9.4,4H F3= 2F9.4)
    5 FORMAT(6H0FREQ= F10.3,5X,3HK=1.15X,3HK=2,15X,3HK=3 )
                                                     B**2
                                                                            A++2
    6 FORMAT(122H0
                           TIME
                                        A * * 2
                                                                    C++2
                          PHASE A
                                        Mun B
                                                 rhase b
                                                              MOD C PHASE C
                 MOD A
     1+8**2
     2
                            )
    7 FORMAT(F12.3.4F12.6,6F10.3)
    8 FORMAT(1H1)
    9 FORMAT(4H MM= 2F12.6,4H RR= 2+12.6,4H VV= 2F12.6)
   10 FORMAT(6H FREU= F12.3,7H GAMMA= F12.3,5H FAB= F12.3, 5H FAC= F12.
     13,5H FBC= F12.3 )
   12 FORMAT(40H DOUBLE PRECISION CUBIC SOLUTION METHOD
                                                                 )
   13 FORMAT(614)
   14 FORMAT(7H SPIN= 12.6,4H GJ= F12.6,5H MU= F12.6,6H DELW= F12.6,
   15H GJP= F12.6.7H DELWP= F12.6)
15 FORMAT(14H STATE NUMBER 14,
                                    6H GAUSS )
  160 FORMAT(48H INITIAL CONDITIONS A=1, B=0, C=0
161 FORMAT(48H INITIAL CONDITIONS A=0, B=1, C=0
                                                                                )
                                                                                )
      PI = 4.0 + DATAN(1.0D+0)
      GAMMA=200.+3.1415927
      XI=CMPLX(0.0,1.0)
       WRITE(9,8)
   19 RFAD(10.1)XSPIN, GJ, XMU, DELW, GJP. DELWP
      READ(10,1)FREUMN, FREQDL.FREQMX.FF.DELT.BGAUSS
       GI=XMU/XSPIN
       ISPIN=XSPIN+1.0
      GO TU (100.101). ISPIN
  1°0 NCASE=2
      FFA(1)=1.0
      XMFA(1)=1.0
      FFB(1)=0.0
      XMFB(1) = 0.0
      FFA(2)=1.0
      XMFA(2)=0.0
       FFB(2)=1.0
      XMFB(2)=-1.0
      GO TO 20
  101 NCASE=3
      FFA(1)=1.5
       XMFA(1)=1.5
       FFB(1)=0.5
```

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xMFB(1)=0.5
      FFA(2)=1.5
      XMFA(2)=0.5
      FFB(2)=0.5
      XMFB(2)=-0.5
      FFA(3)=1.5
      XMFA(3)=-0.5
      FFB(3)=1.5
      XMFB(3) =-1.5
   20 READ(10,1)XMM, RR, VV
      READ(10,13)IMODE, ICSMN, ICSMX
  IMODE 1 GO TO 19 2 GO TO 20
C
      WRITE(9,8)
      NFREQ=(FREQMX-FREQMN)/FREQDL
      NFREQ=NFREQ+1
      NTIME=TF/DELT
      NTIME=NTIME+1
      D0 132 INIT=1,2
      DO 110 ICASE=ICSMN, ICSMX
      CALL BREIT(XSPIN, FFA(ICASE), XMFA(ICASE), GJ, GI, DELW, BGAUSS, FA, XGAUS
     15, FPS1)
      CALL BREIT(XSPIN, FFB(ICASE), XMF8(ICASE), GJ, GI, DELW, BGAUSS, FB, XGAUS
     1S, EPS1)
      CALL BREIT(XSPIN, FFA(ICASE), XMFA(ICASE), GJP, G1, DELWP, HGAUSS, FC, BGA
     1USS, EPS1)
      FC=FC-1058.070
      FAR=FA-FB
      FAC=FA-FC
      FABS(ICASE)=FAB
      FACS(ICASE)=FAC
      FBCS(ICASE) = FB-FC
      D0 110 I=1,NFREQ
      FI=I-1
      FREQ=FREQMN+FI*FREQDL
      DELAB=(FREQ-FAB) +2.0+3.1415927
      PHASAB=CMPLX(0.0,DELAB)
      ARL=(FREQ-FAC)*2.0*3.1415927
      PHASAC=CMPLX(0.0.ARL)
      AIM=-0.5+GAMMA
      DELAC=CMPLX(ARL,AIM)
      XMMSTR=CONJG(XMM)
      RRSTAR=CONJG(RR)
      VVSTAR=CONJG(VV)
      P=DELAB+DELAC
      Q=DELAB*DELAC-VV*VVSTAR=0.25+(RR*RRSTAR+XMM*XMMSTR)
      R=0.5+REAL(XMM+VV+RRSTAR)+0.25+(RR+RRSTAR+DELAB+XMM+XMMSTR+DELAC)
      P=-XI*P
      Q ∓ - Q
      R=XI*R
      CALL CUBIC(P.Q,R,RT1,RT2,RT3)
      X = RT1
      F1=X**3+P*X**2*Q*X+R
      X=RT2
       F2=X**3+P*X**2+0*X+R
      X=RT3
       F3=X**3+P*X**2+Q*X+R
       XIMU(1)=RT1+XI
       XIMU(2)=RT2+XI
       XIMU(3) = RT3 * XI
       DO 22 K=1,3
       D=(DELAC+XIMU(K))+(DELAB+XIMU(K))-VV+VVSTAR
       EPS(K)=-0.5+(XMM+(DELAC+X1MU(K))-RR+VVSTAR)/D
    22 DEL(K) =- 0.5+(RR+(DELAB+XIMU(K))-XMM+VV)/D
       A(1)=EPS(2)+DEL(3)-EPS(3)+DEL(2)
       A(2)=EPS(3)*DEL(1)-EPS(1)*DEL(3)
       A(3)=FPS(1)+DEL(2)-EPS(2)+DEL(1)
       SUM = A(1) + A(2) + A(3)
       GO TO (130,131), INIT
  131 A(1)=DEL(2)-DEL(3)
       A(2)=DEL(3)-DEL(1)
       A(3) = DFL(1) - DEL(2)
   130 DO 23 K=1,3
```

```
A(K) = A(K) / SUM
     B(K) = EPS(K) + A(K)
  23 C(K) = DFL(K) + A(K)
      WRITE(9,8)
      WRITE(9.14)XSPIN, GJ, XMU, DELW, GJP, DELWP
      WRITE(9,5)FRED
     WRITE(9,2)(A(K),K=1,3),RT1.F1
      WRITE(9,3)(B(K),K=1,3),RT2,F2
      WRITE(9.4)(C(K),K=1,3),RT3,F3
      GO TO (150,151), IHIT
 150 WRITE(9.160)
      GO TO 152
 151 WRITE(9.161)
 152 WRITE(9,9)XMM, RR, VV
      WRITE(9,10)FREQ, GAMMA, FABS(ICASE), FACS(ICASE), FBCS(ICASE)
      WRITE(9,15)ICASE, HGAUSS
      WRITE(9,6)
      DO 114 ITIME=1,NT!ME
      FITIME=ITIME
      T=(FITIME-1.0) +DELT
      TIMF(ITIME)=T
      X = RT1 + T
      F1=CEXP(X)
      X=RT2+T
      F2=CEXP(X)
      X=RT3+T
      F3=CEXP(X)
      AA=A(1)/F1+A(2)/F2+A(3)/F3
      BB=B(1)/F1+B(2)/F2+B(3)/F3
      BB=BH+CEXP(PHASAB+T)
      CC=C(1)/F1+C(2)/F2+C(3)/F3
      CC=CC+CEXP(PHASAC+T)
      ASQ(ITIME)=(CABS(AA))*+2
      BSQ(ITIME)=(CABS(8B))++2
      CSQ(ITIME)=(CABS(UC))**2
      ABSQ(ITIME) = ASQ(ITIME) + BSQ(ITIME)
      XMODAA=CABS(AA)
      XMODBB=CABS(BB)
      XMODCC=CABS(CC)
      PHASAA=ATAN2(AIMAG(AA),REAL(AA))
      PHASAA=180.0*PHASAA/3.1415927
      PHASEB=ATAN2(AIMAG(BB).REAL(BB))
      PHASBB=180.0*PHASBB/3.1415927
      PHASCC=ATAN2(AIMAG(CC), REAL(CC))
      PHASCC=180.0+PHASCC/3.1415927
  114 WRITE(9,7)TIME(ITIME),ASO(ITIME).BSO(ITIME),CSO(ITIME),ABSO(ITIME)
     1, XMODAA, PHASAA, XMODBB, PHASBB, XMUDCC, PHASCC
  1<sup>1</sup>0 CONTINUE
  132 CONTINUE
      GO TO (19,20), MODE
      END
      SUBROUTINE CUBIC(P,Q,R,RT1,RT2,RT3)
      DOUBLE PRECISION VERSION
C
  SOLVES CUBIC EQUATIONS OF THE FORM X**3+P*X**2+Q*X+R*0.0 WITH P, G,
C
  AND R COMPLEX. THE THREE ROOTS RT1, RT2, AND RT3 ARE IN ORDER CF
C
  DECREASING REAL PART.
С
      COMPLEX P, Q, R, RT1, RT2, RT3, RT(3) . A, B, U, W120
      DOUBLE PRECISION PR, PI, QR, QI, RR, RI, P2R, P2I, AR, A1, P3R, P3I, PQR, PGI,
     1BR, BI. B2R, B2I, A2R, A2I, A3R, A3I, RI2R, RT21, RTABS, RTARG, RTR, RTI, AAR,
     ZAAI, DARG
      w120=CMPLX(-0,5,0.8660254)
      PR=REAL(P)
      QR=REA( (Q)
      RR=REAL(R)
      PI = AIMAG(P)
      QI = AIMAG(Q)
      RI=AIMAG(R)
      CALL DPROD(PR, PI, PR, PI, P2R, P21)
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AR=QR/3.0-P2R/9.0
   A1=Q1/3.0-P21/9.0
   ASNGLR=AR+3.0
   ASNGLI=A1+3.0
   A=CMPLX(ASNGLR+ASNGL1)
   CALL DPROD(P2R,P21,PR,P1,P3R,P31)
CALL DPROD(PR,P1,UR,Q1,PQR,PQ1)
   BR=P3R/27.0-PGR/6.0+RR/2.0
   BI=P31/27.0-PQ1/6.0+R1/2.0
   CALL DPROD(88,81,88,81,828,821)
   CALL DPROD(AR, AI, AR, AI, A2R, A21)
   CALL DPROD(AR, AI, A2R, A2I, A3R, A31)
   RT2R=B2R+A3R
   RT21=B21+A31
   RTABS=(RT2R++2+RT21++2)++0,25
   CALL DARCTN(RI21,RT2R,RTARG)
   RTARG=RTARG/2.0
   RTR=RTABS+DCOS(RTARG)
   RTI=RTABS+DSIN(RTARG)
   ABSAA=DSQRT((RTR=BR)++2+(RT1+B1)++2)
   ABS8B=DSQRT((RTR+BR)++2+(RT1+H1)++2)
   IF (ABSAA.GE.ABSBB) GD TO 2
   SGN=-1.0
   GO TO 3
 2 SGN=1.0
 3 AAR=-BR+SGN+RTH
   AAI=-BI+SGN+RTI
   ABS=(AAR++2+AAI++2)++(1.0/6.0)
   CALL DARCTN(AAI, AAR, DARG)
   ARG=DARG/3.0
   UR=ABS+COS(ARG)
   UI=ABS+SIN(ARG)
   U=CMPLX(UR,U1)
   DO 1 J=1,3
   RT(J)=U-(P+A/U)/3.0
 1 U=U+W120
   R1=REAL(RT(1))
   R2=REAL(RT(2))
   R3=REAL(RT(3))
   1F(R1.GE.R2)G0 T0 10
   IF(R3.GE.R2)G0 T0 11
   1F(R3.GE.R1)60 TO 12
   J1=2
   .)2=1
   J3=3
   GO TO 15
12 J1=2
   J2=3
   13=1
   GO TU 15
11 J1=3
   12=2
   J3=1
   GO TO 15
10 IFTR3.GE.R1)G0 TO 13
   1F (R3.GE, R2) GO TO 14
   J1≖1
   J2=2
   13=3
   GO TH 15
14 11=1
   12=3
   13=2
   GO TO 15
13 .1=3
   J2=1
   13=2
15 CONTINUE
   RT1=HI(J1)
   RT2=HT(J2)
   RT3=RT(J3)
   RETURN
   END.
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SUBROUTINE DPROD(xR,xI,yR,yI,ZR,ZI) DOUBLE PRECISION XR, XI, YR, YI. ZR, ZI ZR=XR+yR-XI+YI ZI=XI+yR+XR+YI RETURN END

```
SUBROUTINE DARCTN(Y,X,Z)
C FINDS DOUBLE PRECISION ARCTANGENT IN RADIANS IN CORRECT QUADRANT.
 DEFINES ZERO/ZERO=ZERO, USES RANGE PI TO - PI
C
      DOUBLE PRECISION X, Y, Z, PI, YX
      COMMON PT
      YX=Y/X
      IF(X)300,301,302
  300 IF(Y)303,304,304
  303 7=DATAN(YX)-P1
      GO TO 308
  304 Z=DATAN(YX)+PI
                                       .
      GO TO 308
  301 IF(Y)305,306,307
  305 7=-P1/2.0
      GO TO 308
  306 Z=0.0
      GO TO 308
  307 Z=P1/2.0
      GO TO 308
  302 Z=DATAN(YX)
  308 RETURN
      END
```

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SUBROUTINE BREIT(XI,FFF,XM,GJ,GI.DELW,BGAUSS,W,XGAUSS,EPS1)
 ISGN=FFF
 F=ISGN
 SGN=(F+2.0-1.0)+(DELW/2.0)
  GJ_1 = GJ + 0.00229 * (GJ - 1.0)
  EPS=1.0/(GJ1+1836.1/GI-1.0)
 XGAUSS=GJ1*9.2732*BGAUSS/(6.625*DELW*(1.0+EPS))
5 EPS1=EPS+DELW+XGAUSS
6 W=-DELW/(4.0*XI+2.0)+EPS1*XM
 B=2.0+XM/(X1+0.5)
  IF(B+1.0)1,1,2
1 IF(XGAUSS-1.0)2,3,3
3 SGN=-SGN
2 W=W+SGN+SQRT(1+0+B+XGAUSS+XGAUSS+XGAUSS)
  IF(GJ.GE.1.0) RETURN
 DELTA=ABS(W) +4.0+BGAUSS/(9.0+5214.0)
  W=W-DELTA
 RETURN
 END
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APPENDIX B. A COMPUTER PROGRAM FOR THE NUMERICAL INTEGRATION OF THE FOUR-LEVEL EQUATIONS A FORTRAN IV program which numerically integrates the four-level equations is given in this appendix. The version given finds $|a|^2$, $|b|^2$, $|c|^2$, $|d|^2$, and $|a|^2 + |b|^2$ as a function of time for a set of fixed driving frequencies and fixed magnetic field. The real and imaginary parts of a, b, c, and d are also given. Other versions of the program exist in which time is held constant while the variation of the above quantities with magnetic field at fixed frequency, or with frequency at fixed magnetic field, is studied.

On a CDC 6600, the program requires (for the accuracy used here) about 1 minute of central processor time per microsecond of integration time. More precisely, the computation times and number of times the subroutine DERIV is called are as follows: Card 3 (FORMAT F12.6)

FREQ2 driving transverse frequency in MHz (normally zero)

Card 4 (FORMAT 6 F12.6)

Identical to Card 3 for program described in Appendix A.

Card 5 (FORMAT 6 F12.6)

XMMP	M۱	in MHz	(angular	frequency)
RRP	R'	in MHz	(angular	frequency)
VVP	٧١	in MHz	(angular	frequency)

where these quantities are complex and again require two numbers each for their specification.

Cards 6, 7 (FORMAT 6 F12.6)

XO(1)	initial	real part	of a		
XO(2)	initial	imaginary	part	of	a

Case	DERIV Calls per µsec	Computation Time per µsec	Approximation
1	5,000	35 sec	3 level, e ^{iwt}
2	80,000	66 sec	3 level, cos wt
3	40,000	42 sec	4 level, $e^{i\omega t}$, $e^{-i\omega t}$
24	80,000	81 sec	4 level, cos wt

where the case number is as given in Figure 20. The program is believed to maintain better than 1% accuracy for integration times at least up to 1 microsecond. The accuracy can be adjusted with the parameters RELTST and ABSTST in subroutine INTEG. Accuracy testing is done in subroutine ACCRY.

The program is set up to allow the transverse electric field to oscillate also. This case could be of interest if the metastable beam was mixed with a plasma, since rf fields could penetrate the plasma, under appropriate conditions, while static electric fields cannot.

The input for the program is as follows:

Card 1 (FORMAT F12.6)

Identical to Card 1 for program described in Appendix A.

Card 2 (FORMAT F12.6)

Identical to Card 2 for program described in Appendix A.

XO(3)	initial real part of b
xo(4)	initial imaginary part of b
XO(5)	initial real part of c
xo(6)	initial imaginary part of c
XO(7)	initial real part of d

XO(8) initial imaginary part of d

Card 8 (FORMAT 6 14)

Identical to Card 4 of program described in Appendix A.

The program consists of a main program together with several subroutines. The function of the various subroutines is as follows:

 a) SUBROUTINE INTEG (NN, TI, TTF, HH, HHP, MM, VVM, IP, XO, TT, XXP)

This subroutine integrates an arbitrary system of real inear differential equations. The arguments of this subroutine are defined by comments in the main program listing. The monitoring feature (a periodic test of a specified variable against some limit) is not used. INTEG calls a number of subroutines of which only those which are specific to the problem under discussion will be further described.

b) SUBROUTIN DERIV (T, V, FD)

This subroutine computes the value of the first derivatives FD(I) (for I = 1 to 8) given the value of the functions V(I) (for I = 1 to 8) and the time T. I = 1 and 2 correspond to the real and imaginary parts of a, 3 and 4 to the real and imaginary parts of b, and so on. (The four complex first-order differential equations have been rewritten as eight real first-order differential equations.)

c) SUBROUTINE PRINT (T, V)

This subroutine sets up the common variable arrays at the specified print-step intervals for later printout.

d) SUBROUTINE BREIT (XI, FFF, XM, GJ, GI, DELW,

BGAUSS, W, XGAUSS, EPS1)

This subroutine was described in Appendix A.

The output from the program is fully labeled. Tape 10 is defined as input and Tape 9 as output for the system for which this program was written.

The inclusion of fields whose strength varies as time (or displacement in a cavity) can be easily incorporated in the subroutine DERIV. It is required to give RR, RRP, MM, MMP. VV. and VVP the required time dependence, as indicated on comment cards.

It is important to simplify DERIV as much as possible, from the point of view of computation time, since it is in the innermost loop. The form listed here is more general than required for many problems, and, if computer time is important, it should be simplified in those cases.

PROGRAM LAMBV(INPUT, TAPE 10=INPUT, OUTPUT, TAPE 9= OUTPUT, FILM, TAPE 1 12=FILM) AMPLITUDES AS FUNCTION OF TIME VERSION. LONGITUDINAL AND TRANSVERSE C DRIVING FREQUENCIES ALLOWED (TRANSVERSE FREQUENCY NORMALLY ZERO). DIMENSIONS ALLOW UP TO 5 FREQUENCY POINTS, 100 TIME POINTS С (RESULTS STORED AS DIMENSIONED VARIABLES TO FACILITATE PLOTTING) C DIVIDE R AND V BY 13.94 TO UBTAIN VOLTS/CM PEAK TO ZERO DIVIDE M BY 8.80 TO OBTAIN GAUSS PEAK TO ZERO С THAT IS, ENTER P,V, AND M IN MHZ (ANGULAR FREQUENCY) COMPLEX XMM, XMMP, RR. RRP, VV, VVP COMMON ARL(3+100,5), BRL(3,100+5), CRL(3+100+5), DRL(3+100+5), 1AIM(3,100,5),BIM(3,100,5),CIM(3,100,5),DIM(3,100,5),ICASE,IFREQ, 2ITIME, TIME(100) COMMON/RLK3/XMM+XMMP+RR+RRP+VV+VVP+GAMMA2+WAB+WAE+WAF+WBF+WBF+WEF+ 1WFREW1.WFREQ2 CUMMON/RLK7/IDERIV DIMENSION ASU(100) + BSQ(100) + CSO(100) + DSQ(100) + ABSQ(100) DIMENSION FFA(3) . XMFA(3) . FFB(3) . XMFB(3) DIMENSION X0(30) . XXP(30) . FREQ(5) . FSP(3.6) 1 FORMAT (6F12.6) 6 FORMAT (132H 5##A TIME H##2 C##2 D##2 A##2 CIM ORL 1+8++2 ARL ΛIM BRL BIM CRL DIM 2 1 7 FURMAT(F10.3.5F10.6.8F7.3) S FORMAT(1H1) 9 FORMAT 44 MM= 2F14.6.44 HR= 2F14.6. 44 VV= 2F14.6) 10 FORMAT (9H HGAUSSE F12.3+ 8H GAMMAE F12.3+8H FREQIE F12.3+ 184 FRE42= F12.3) 11 FURMAT(SH MMP= F13.6+F14.6+ SH RRP= F13.6+F14.6+ SH VVP= F13.6+ 1=14.6) 13 FORMAT(614) 14 COPMAT (74 SPIN= F12.6.4H GJ= F12.6.5H MU= F12.6.6H DELW= F12.6. 15H GJP= F12.6,7H DELWP= F12.6) 15 FORMAT (14H STATE NUMBER 14) 16 FORMAT(16H INITIAL VECTOR 4(F10+3+F7+3)) 17 FORMAT (5H FAB= F10.3+5H FAE= F10.3+5H FAF= F10.3+5H FBE= F10.3+ 15H FRF= F10.3,5H FEF= F10.3) GAMMA#100+0#2+0#3+1415927 GAMMA2=0.5+GAMMA WRITE(9,8)

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19 READ(10,1)XSPIN+GJ+XMU+DELW+GJP+DELWP
    READ(10,1)FREQMN, FREQDL, FREQMX, TTF, HHP, BGAUSS
    READ(10,1)FREQ2
    GI=XMU/XSPIN
    ISPIN=XSPIN+1.0
    GO TO (100,101) . ISPIN
100 NCASE=2
    FFA(1)=1.0
    XMFA(1)=1.0
    FFB(1)=0.0
    XMFB(1) \equiv 0 = 0
    FFA(2)=1.0
    XMFA(2)=0.0
    FFB(2)=1.0
    XMFH(2)=-1.0
    GO TO 20
101 NCASE=3
    FFA(1)=1.5
    XMFA(1)=1.5
    FF8(1)=0.5
    XMFB(1)=0.5
    FFA(2)=1.5
    XMFA(2)=0.5
    FFB(2)=0.5
    XMF8(2)=-0.5
    FFA(3)=1.5
    XMFA(3)=-0.5
    FFB(3)=1+5
    XMFB(3)=1.5
 20 READ(10.1)XMM, RR, VV
    READ(10.1) XMMP.RRP.VVP
    REAU(10,1)(X0(1),1=1+8)
    READ (10,13) IMODE. ICSMN, ICSMX
    NFREQ# (FREQMX-FREQMN) /FREQUL
    NFREG#NFREQ+1
    DO 110 ICASE=ICSMN+ICSMX
    IDERIV=0
    ITIME≢0
    CALL BRFIT (XSPIN.FFA (ICASE), XMFA (ICASE), GJ, GI, DELW, BGAUSS, FA,
   1XGAUSS, EPS1)
    CALL BREIT (XSPIN.FFB (ICASE) .XMFB (ICASE) .GJ,GI,DELW,BGAUSS,FB,
   1XGAUSS.FPS1)
    CALL BREIT (XSPIN, FFA (ICASE) , XMFA (ICASE) , GJP, GI, DELWP, BGAUSS, FE,
   1XGAUSS,EPS1)
    CALL BREIT(XSPIN, FFB(ICASE), XMFB(ICASE), GJP, GI, DELWP, BGAUSS, FF,
   1XGAUSS, EPS1)
    FE=FE-1058.070
    FF=FF-1058.070
    FAB=FA-FB
    FAE=FA=FE
    FAF=FA-FF
    FBE=FB-FE
    FBF=FB-FF
    FEF=FE-FF
    WAB=FA8+6.2831854
    WAE=FAE+6.2831854
    WAF=FAF+6.2831854
    wBE=FBE+6.2831854
    wBF=FRF#6.2831854
    wEF=FEF#6.2831854
    FSP(ICASE+1)=FAB
    FSP(ICASE+2)=FAE
    FSP(ICASE+3) #FAF
    FSP(ICASE,4)=FBE
    FSP(ICASE+5)=FBF
    FSP(ICASE+6)=FEF
    DO 112 IFREQ=1.NFREQ
    FIFREQ=IFREQ
    FREQ(IFREQ) = (FIFREQ-1.0) *FREQDL+ FREQMN
    FREQ1=FREQ(IFREQ)
    WFREQ1=6.2831854*FREQ1
    WFREQ2=6.2831854*FREW2
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WRITE(9,8)
      NN=8
      TI=0.0
      HH=0.0001
      MM=0
      VVM=0.0
      TP=0
      CALL INTEG (NN,TI,TTF,HH,HHP,MM,VVM,IP,XO,TT,XXP)
   NN
        NUMBER OF FIRST ORDER DIFFERENTIAL EQUATIONS
        INITIAL VALUE OF INDEPENDENT VARIABLE
С
   TΙ
   TTF
        FINAL VALUE OF INDEPENDENT VARIABLE
С
        GUESS AT STEP SIZE
PRINT STEP SIZE
С
   HH
   HHP
С
        VARIABLE TO BE MONITORED (0=NO, 1 TO NN YES )
C
   ММ
С
   VVM
        VALUE TO MONITOR FOR
   IP
        NUMBER OF PARAMETERS
С
С
   XO
        VECTOR OF STARTING VALUES
        VALUE OF TIME RETURNED AT END OF INTEGRATION
C
  TT
        VARIABLE VALUES RETURNED AT END OF INTEGRATION
  XXP
С
  112 CONTINUE
  110 CONTINUE
      NTIME=ITIME
      DO 26 IFREQ=1,NFREQ
      DO 25 ICASE=ICSMN+ICSMX
      WRITE (9,8)
      WRITE(9,14)XSPIN,GJ,XMU,DELW,GJP,DELWP
      WRITE(9,9)XMM,RR,VV
      WRITE (9,11) XMMP + RRP, VVP
      WRITE(9,10)BGAUSS+GAMMA+FREQ(IFREQ)+FREQ2
      WRITE (9,15) ICASE
      WRITE( 9+16)(XO(I)+I=1+B)
      WRITE( 9,17) (FSP (ICASE, IFS), IFS=1,6)
      wRITE(9,6)
      DU 24 ITIME=1.NTIME
      ASQ(ITIME)=AKL(ICASE,ITIME,IFREQ)**2+AIM(ICASE,ITIME,IFREQ)**2
      BSQ(ITIMF)=BRL(ICASF+ITIME+IFREQ)++2+BIM(ICASE+ITIME+IFREQ)++2
      CSQ(ITIME) = CRL (ICASE + ITIME + IFREQ) **2+CIM (ICASE + ITIME + IFREQ) **2
      DSQ(ITIME)=DRL(ICASE+ITIME+IFREQ)*+2+DIM(ICASE+ITIME+IFREQ)*+2
      AUSQ(ITIME) #ASQ(ITIME) +BSQ(ITIME)
   24 WRITE(9,7)TIME(ITIME),ASQ(ITIME),BSQ(ITIME),CSQ(ITIME),DSQ(ITIME),
     1ABSQ(ITIME),
     2ARL(ICASE, ITIME, IFREW), AIM(ICASE, ITIME, IFREW),
     3BRL(ICASE, ITIME, IFREQ), BIM(ICASE, ITIME, IFREQ),
     4CRL(ICASE + ITIME + IFREQ) + CIM(ICASE + ITIME + IFREQ) +
     5DRL(ICASE, ITIME, IFREQ), DIM(ICASE, ITIME, IFREQ)
   25 CONTINUE
   26 CONTINUE
      GO TO (19+20)+IMODE
      END
      SUBROUTINE INTEG (NN+TI+TTF+HH+HHP+MM+VVM+P+X0+TT,XXP)
   INTEG() SOLVES A SYSTEM OF N FIRST ORDER DIFF EQNS BY A 4TH
   ORDER ADAMS P-C METHOD WITH AUTOMATIC ERROR CONTROL. STARTING
С
   IS BY RUNGA-KUTTA.
С
C
      INTEGER P.U
      REAL LB
      LUGICAL ACC
      CUMMON/RLK1/N+T+TF+H+H0+HP+M+VM+J+ACC+LB+RELTST+ABSTST+FACTOR+
     1BND+X(3n,5),F(30,5),E(30),XP(30)
      COMMON/BLK5/IDOUBL,NDOUBL
      DIMENSION X0(30),XXP(30)
   SET UP INITIAL VALUES
С
      N=NN
      TF#TTF
      H#HH
      HPaHHp
      м≖мМ
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VM=VVM
       00 10 I=1+N
   10 x(I+1)=x0(I)
IF (P.EQ.0) GO TO 21
       L=N+1
       Ū≡N+P
       n0 20 I=L+U
       XP(I)=Xn(I)
       DO 20 J=1,5
   20 x(I+J)=x0(I)
21 T=TI
       BND=TI+HP
       HO=H
       ABS8=1.0E=4
       RELBEABSB
       ABSTST=ABSB#14.2
       RELTST=RELB+14.2
       FACTOR=RELB/ABSB
       LB=0.005#RELTST
       IDUARF=0
       NDOUBL=3
       H=5+0#H
30 CALL START(IRETRN)
GU TO (100,99),IRETRN
C SHOULD ANY OF THE STARTING VALUES BE PRINTED OUT
  100 T=T-3.0*H
       00 35 J=2+4
       T≖T+H
       CALL TEST (IRETRN)
       60 TO (35,60), IRETRN
   35 CONTINUE
C BEGIN ÁDAMS METHOD
   40 CALL ADAMS
       CALL ACCRY
IF (ACC) GO TO 50
       00 45 I=1+N
   45 X(I+1)=X(I+4)
       GU TO 30
   50 CALL TEST(IRETRN)
GO TO (101+60)+IRETRN
  101 CALL DOUBLE(IRETRN)
GU TO (40+30)+IRETRN
   60 IF (J.EQ.5) GO TO 65
   DU 64 Iml+N
64 XP(I)=X(I+J)
   65 CALL PRINT(T+XP)
       TTET
       DO 70 I=1+N
   70 XXP(I)=XP(I)
99 RETURN
       END
       SUBROUTINE START (IRETRN)
C RUNGA-KUTTA STARTING METHOD
       LUGICAL ACC
      CUMMON/BLK1/N+T+TF+H+H0+HP+M+VM+J+ACC+LB+RELTST+ABSTST+FACTOR+1BND+X(30+5)+F(30+5)+E(30)+XP(30)
       CUMMON/BLK2/G(30,4)
       Ĵ=2
       CALL RNGA
   10 DU 15 I=1+N
   15 XP(I)=X(I+2)
C XP(I)=DBL INTERVAL RESULT FOR ERHOR ANALYSIS
       T=T=H
       H=0.5+H
       IF ((T+H) .NE.T) GO TO 30
       WRITE (9,20)
   20 FURMAT (50H EUNS CANNOT BE SOLVED FURTHER WITHIN GIVEN ERROR )
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TPLUSH=T+H
       WRITE (9,21) TPLUSH ,T
   21 FORMAT (6H T+H# E15.10. 6H T#
                                               E15.10)
       IKETRN#2
       RETURN
   30 DO 40 J=2,3
   40 CALL RNGA
41 CALL ACCRY
       IF (.NOT.ACC) GO TO 10
       Ĵ≡4
       CALL RNGA
       IRE [RN=1
       RETURN
       END
       SUBROUTINE RNGA
C INTEGRATE N EQNS AHEAD ON THE JITH STEP OF LENGTH H.
       CUMMON/BLK1/N, T, TF, H, HO, HP, M, VM, J, ACC, LB, RELTST, ABSTST, FACTOR,
      1BND+X(30+5)+F(30+5)+E(30)+XP(30)
       COMMON/BLK2/G(30,4)
       CALL DERIV(T+X(1,J=1),F(1,J=1))
D0 10 I=1+N
       G(I+1) = H + F(I+J-1)
   10 X(I+J)=X(I+J-1)+0+5+G(I+1)
       TT=T+0.5#H
       CALL DERIV(TT,X(1,J)+F(1+J))
       n0 20 I=1,N
       G(I+2)=H+F(I+J)
   20 \chi(1 \cdot J) = \chi(I \cdot J - 1) + 0 \cdot 5 + G(I \cdot 2)
       CALL DERIV(TT+X(1+J)+F(1+J))
D0 30 I=1+N
       G(I+3) = H + F(I+J)
   30 \times (I + J) = \times (I + J - 1) + c_1 (I + 3)
       T=T+H
       CALL DERIV(T+X(1+J)+F(1+J))
       DO 40 I=1.N
       G(I+4)=H*F(I+J)
   40 \ \chi(I_{9}J) = \chi(I_{9}J-1) + (G(I_{9}1)+2_{9}0 + (G(I_{9}2)+G(I_{9}3))+G(I_{9}4))/6_{9}0
       RETURN
       END
       SUBROUTINE ACCRY
C TESTS ABS AND REL ERROR AND SETS ACC .FALSE. IF NEITHER SATISFIED
       LOGICAL ACC
       COMMON/BLK1/N+T+TF+H+H0+HP+M+VM+J+ACC+LB+RELTST+ABSTST+FACTOR+
      1BND+X(30+5)+F(30+5)+E(30)+XP(30)
       ACC# .TRUE .
       DO 50 I=1+N
       E(I) = ABS(XP(I) = X(I,J))
       IF (E(I).GE.ABS(x(I,J))*RELTST) GO TO 10
       E(I) = E(I) / ABS(X(I+J))
   GO TO 50
10 IF (2(1).GE.ABSTST) 30 TO 29
       E(I) =E(I) +FACTOR
       GO TO 50
   20 T=T-H
       H0=0.5+H
       ACC# .FALSE .
   75 FORMAT(1H + 16HSTEP SIZE CUT TO, F12.8, 6H AT T=, F12.8)
WRITE(9,75) H0,T
       GO TO 99
   50 CONTINUE
   99 RETURN
       END
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SUBROUTINE TEST (IRETRN)
  MONIFORS FOR VM. END OF INTEGN ON PRINT RANGE.
C
      COMMON/RLK1/N+T+TF+H+H0+HP+M+VM+J+ACC+LB+RELTST+ARSTST+FACTOR+
      18N0+X (30,5) +F (30,5) +E (30) +XP (30)
      DIMENSION X1(30) + X2(30) + F1(30) + F2(30)
      IF (M.EQ.0) GO TO 20
IF ((X(M,J).LE.VM).AND.(X(M,J-1).GT.VM)) GO TO 10
       IF ((X(M,J).GT.VM).AND.(X(M,J=1).LE.VM)) GO TO 10
       GU TD 20
   10 CALL DIODE
      IF(T-TF)70.70,30
   70 IRETRN=2
      RETURN
   20 IF (ABS((T-TF)/TF1-1.0E-6) B0,81,81
   80 IRFTRN=2
      RETURN
   81 IF(T.LE.TF) GO TO 40
   30 H=TF-T
      D0 35 I=1+N
   35 X(I+1)=X(I+J)
       J=2
      CALL RNGA
      IRETRN=2
RETURN
   40 IF (T.LT.BND) GO TO 50
С
  SAVE ALL VARIABLES WHICH MAY BE MODIFIED IN PRINT PROCEDURE
      HSAVE=H
      TSAVE≖T
      JSAVE=J
      DO 45 I≡1+N
      X1(I) = X(I+1)
      x2(1)=x(1+2)
      F1(I) = F(I+1)
      F2(I) = F(I+2)
   45 x(I+1)=x(I+J)
      J≢2
      H=BND-T
      CALL RNGA
      CALL PRINT(T+X(1,J))
      BND=BND+HP
C RESTURE VARIABLES TO PROCEED
      J=JSAVE
      H=HSAVE
      T=TSAVE
      D0 46 I=1+N
      X(I+1) = XI(I)
      x(1+2)=x_{2}(1)
      F(I+1) = F1(I)
   46 F(I+2)=F2(I)
   50 IF (J.NF.5) GO TO 99
      10 60 I=1+N
      \chi(I+4) = \chi(I+5)
      NO 60 J=2+5
   60 F(I+J=1)=F(I+J)
   99 IRETRN=1
      RETURN
      END
      SUBROUTINE DIODE
C FIND VALUE OF T WHERE THE M/TH VARIABLE REACHES THE VALUE VM
      COMMON/BLK1/N,T+TF,H+H0,HP+M,VM+J,ACC+LB,RELTST,ABSTST,FACTOR,
     18ND+X(30+5)+F(30+5)+E(30)+XP(30)
      DIMENSION D(30)
      Y1=X(M,J)
      Y0=X(M,J-1)
      DELT=-ABS(H+Y1/(Y1-Y0))
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10 H=DELT
D0 20 I±1+N
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20 x(I+1)=x(I+J)
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J=2
      CALL RNGA
      CALL DERIV(T+X(1,J),U)
      DELT=(VM-X(M+J))/D(M)
      IF (ABS(DELT).GE.1.0E-4) GO TO 10
      NV=(L+M)X
      RETURN
      END
      SUBROUTINE ADAMS
  INTEGRATE ONE STEP BY THE ADAMS PREDICTOR-CORRECTOR METHOD
С
      CUMMON/HLK1/N,T,TF,H,H0,HP,M,VM,J,ACC,LB,RELTST,ABSTST,FACTOR,
     1BND+X(30+5)+F(30+5)+E(30)+XP(30)
      J≍5
      CALL DERIV(T+X(1,4),F(1+4))
      DO 10 I=1+N
   10 XP(I)=X(I+4)+0+041666667*H*(55+0*F(I+4)-59+0*F(I+3)
     1+37+0 (I+2)=9+0 (I+1))
      T=T+H
      CALL DERIV(T+XP+F(1+5))
      DO 20 I=1+N
   20 X(I+5)=X(I+4)+0+0416666667*H*(9+0*F(I+5)+19+0*F(I+4)
     1-5.0*F(I.3)+F(I.2)
      RETURN
      END
      SURROUTINE DOUBLE (IMETRN)
 CAN INTERVAL BE DOUBLED
С
      REAL LH
      COMMON/BLK1/N,T,TF,H,H0,HP,M,VM,J,ACC,LB,RELTST,ABSTST,FACTOR,
     1BND+X(30,5),F(30,5),E(30),XP(30)
      CUMMON/BLK5/IDOUBL, NDOUBL
      IDOUBL=IDOUBL+1
 IF (IDOURL .LT .NDOUBL) GO TO 99
ALLOWS DOURLE ATTEMPT ONLY EVERY NDOUBL/TH CALL
С
      IDOURT=0
      DO IO I=1+N
      IF (E(I).GT.LB) GO TO 99
   10 CONTINUE
      D1=HP/(2.0+H)
      IF (D1.LE.2.0) GO TO 99
      D2=(BND=T)/(2 \cdot 0 + H)
      IF (D2.LE.2.0) GO TO 99
      DO 20 I=1+N
   20 \times (I + 1) = \times (I + 4)
      HU=2.0*H
H=2.0*H0
   30 FORMAT(18H STEP INCREASED TO F12.8, 6H AT T= F12.8)
      WRITE(9,30)H0+T
      IRETRN=2
      RETURN
   99 IRFTRN=1
      RETURN
      END
      SUBROUTINE DERIV(T,V,FD)
      DIMENSION V(30),FD(30)
      COMPLEX UBA+UFE+UEA+UFB+UFA+UEB
      COMPLEX XMM+XMMP,RR,RRP+VV+VVP
      COMMON/BLK3/XMM+XMMP+RR+RRP+VV+VVP+GAMMA2+WAB+WAE+WAF+WBE+WBF+WEF+
     1WFREQ1 • WFREQ2
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CUMMON/BLK7/IDERIV
      IDERIV=IDERIV+1
      FOFT1=COS(WFREQ1+T)
  REPLACE FOFT1 BY FOFT1* (DESIRED SLOW FUNCTION OF TIME) TO MODULATE
C
  RR+RRP+MM+MMP
С
      FOFT2=COS (WFREQ2+T)
   IF FREQ2=0.0 IS ONLY CASE OF INTEREST SET FOFT2=1.0 TO SAVE COMPUTER
С
С
   TIME
  REPLACE FOFT2 BY FOFT2* (DESIRED SLOW FUNCTION OF TIME) TO MODULATE
С
  VV+VVP
С
      UR=-SIN(WAE+T)
      UI==COS(WAE*T)
      UEA=RR#FOFT1#CMPLX(UR+UI)
      UR=-SIN(WBE+T)
      UI=-COS(WBE*T)
      UER=VV*FOFT2*CMPLX(UR,UI)
      UEAR=REAL (UEA)
(IEBR=REAL (UEB)
      UEAI=AIMAG(UEA)
      UEBI=AIMAG(UEB)
      FD(1)=-UEAR*V(5)-UEA1*V(6)
      FU(2) = UEAI + V(5) = UEAR + V(6)
      FD(3) =-UEBR*V(5)-UE81*V(6)
      FU(4)=UEBI+V(5)=UEBR+V(6)
      FD(5)=UEAR+V(1)-UEAI+V(2)+UEBR+V(3)-UEBI+V(4)-GAMMA2+V(5)
      FD(6)=UEAI+V(1)+UEAR+V(2)+UEBI+V(3)+UEBR+V(4)-GAMMA2+V(6)
      FD(7) = -GAMMA2 + V(7)
      FU(8) == GAMMA2 +V (A)
       IF (CABS(RRP) .NE .0.0) GO TO 101
       IF (CABS (VVP) +NE + 0 + 0) GO TO 101
      GO TO 200
  101 UR=-SIN(WBF+T)
       UI==COS(WBF#T)
      UFB=RRP#FOFT1#CMPLX(UR,UI)
      UR=-SIN(WAF+T)
      UI==COS(WAF*T)
      UFA=VVP+FOFT2+CMPLX(UR,UI)
      UFBR=REAL(UFB)
       UFAR=REAL (UFA)
       UFBI=AIMAG(UFB)
       UFAI=AIMAG(UFA)
       FD(1)=FD(1)=UFAR+V(7)=UFAI+V(8)
      FD(2)=FD(2)+UFAI+V(7)-UFAR+V(8)
      FD (3) =FD (3) =UFBR+V (7) =UFBI+V(8)
      FU(4) = FD(4) + UFBI + V(7) = \langle IFBR + V(8) \rangle
       FD(7)=FD(7)+UFAR+V(1)=UFAI+V(2)+HFBR+V(3)=UFBI+V(4)
      FD(8)=FD(8)+UFAI+V(1)+UFAR+V(2)+UFBI+V(3)+UFBR+V(4)
  200 IF(CABS(XMM) .NE. 0.0) GO TO 201
       IF (CABS (XMMP) .NE.0.0) GO TO 201
       GO TO 300
  201 UH=-SIN(WAB+T)
       UI==COS(WAB#T)
       UHA=XMM+FOFT1+CMPLX(UR+UI)
       UR=-SIN(WEF#T)
       UI=-COS(WEF*T)
       UFE=XMMP+FOFT1+CMPLX(UR+UI)
       UBAR=REAL (UBA)
       UFER=REAL (UFE)
       UBAI=AIMAG(UBA)
       UFEI=AIMAG(UFE)
       FD(1)=FD(1)=UBAR+V(3)=UBAI+V(4)
       FD(2)=FD(2)+UBAI+V(3)=UBAR+V(4)
       FD(3) \pm FD(3) + UBAR + V(1) - UBAI + V(2)

FD(4) = FD(4) + UBAI + V(1) + UBAR + V(2)
       FD(5)=FD(5)=UFER+V(7)=UFEI*V(8)
       FD(6)=FD(6)+UFEI+V(7)-UFER+V(8)
       FD(7)=FD(7)+UFER+V(5)-UFEI+V(6)
       FD(8)=FD(8)+UFEI+V(5)+UFER*V(6)
  300 RETURN
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END

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SURROUTINE PRINT (T,V)
   DIMENSION V(30)
   COMMON ARL (3,100,5), BRL (3,100+5), CRL (3,100,5), DRL (3,100,5),
  1A1M(3+100+5)+BIM(3,100+5)+CIM(3+100+5)+DIM(3,100+5)+ICASE+IFREQ+
  2ITIME.TTME(100)
   CUMMON/BLK1/N,T,TF,H,H0,HP,M,VM,J,ACC,LB,RELTST,ABSTST,FACTOR,
  1BND+X (3n+5) +F (30+5) +E (30) +XP (30)
   COMMON/BLK7/IDERIV
   ITIME=ITIME+1
   FITIME=TTIME
   TIME(ITIME) = FITIME + HP
WRITE (9,10) ICASE, ITIME, IFREQ, IDERIV
10 FORMAT(6H ICASE 14,6H ITIME 14,6H IFREQ 14,13H DERIV CYCLES I10)
11 FORMAT (9F12.6)
   wRITE(9,11)T+(V(I)+I=1,8)
   ARL(ICASE + ITIME + IFREQ) = V(1)
   AIM(ICASE+ITIME+IFREQ)=V(2)
   BRL(ICASE + ITIME + IFREW) =V(3)
   BIM(ICASE, ITIME, IFREW) =V (4)
   CRL(ICASE+ITIME+IFREW)=V(5)
   CIM(ICASE+ITIME+IFREQ)=V(6)
   DRL(ICASE, ITIME, IFREQ) =V(7)
   DIM(ICASE, ITIME, IFREQ) =V(8)
   RETURN
   END
   SUBROUTINE BREIT (XI, FFF, XM, GJ, GI, DELW, BGAUSS, W, XGAUSS, EPS1)
   ISGN=FFF
   F=ISGN
   SGN= (F+2.0-1.0) + (DELW/2.0)
   GJ1=GJ+0.00229#(GJ=1.0)
   FPS=1.0/(GJ1*1836.1/GI=1.0)
   XGAUSS=GJ1*9.2732*BGAUSS/(6.625*nELW*(1.0*EPS))
 5 EPS1=EPS+DELW+XGAUSS
```

6 W=-DELW/(4.0*XI+2.0)+EPS1*XM

2 W=W+SGN+SQRT(1.0+B+XGAUSS+XGAUSS+XGAUSS+XGAUSS)

DELTA=ABS(W) #4.0+BGAUSS/(9.0+5214.0)

B=2+0*XM/(XI+0.5) IF(8+1.0)1+1+2 I IF(XGAUSS=1.0)2+3+3

IF (GJ.GE.1.0) RETURN

3 SGN=-SGN

W=W-DELTA RETURN END 4

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