THE DEVELOPMENT OF A HIGH-EXPLOSIVE DRIVEN CROWBAR SWITCH

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Summary

A compact explosively-driven, metal-to-metal contact, solid dielectric switch has been developed for use as a low-resistance, < 10-μΩ, low-inductance, < 10-nH, crowbar switch. A 100 milligram high-explosive charge is used to extrude a 0.090-in. plate through 0.040-in. polyethylene and achieve a hard current contact with a 0.625-in.-diameter die plate. The closure time, from the signal, which initiates the charge, to beginning of current rise in the switch, is 11.0 μsec ± 0.3 μsec. In crowbar application the switch has carried 180-330 kA which decays with a 1/e time of ≈ 1.2 msec.

Design Development

One of the experimental machines in LASL fusion research, known as the "Toroidal Z-Pinch" device, required the use of a fast-acting, metal-to-metal type switch for use in a low-inductance crowbar application. The space available in the machine geometry where these switches were to be installed was extremely minimal; consequently, these switches had to be designed as small self-contained units, quite unsimilar to a previously-used exploding foil switch.[1] The foil switches, while being desirable for some applications, require, among other features, large and elaborate clamping mechanisms, complex individual capacitance discharge systems, and general environmental necessities such that their use in our application seemed impractical. Our attention was therefore directed toward alternate energy sources to perform the switching action, i.e. to the use of high explosives. It was observed that while the exploding foil switch does not use a powder charge per se, it nonetheless makes use of expanding gases, not too unlike a powder discharge, to perform its function. In this sense only the two switching actions may be considered similar. It was also observed that the use of high explosives would not only provide us environmental flexibility, but would also offer a much wider range of explosive characteristics from which to choose. For example, the weight and type of powder charge could be varied and selected for the desired speed of burning and energy potential. Shaped charges could be used depending upon whether more penetration of the discharge was considered necessary (a la "Monroe Jet" principal). These were a few of the factors that led to the development and ultimate use of the detonator switch about to be discussed.

The basic action required in switches of this type, whether foil or detonator, involves the deformation of metal. This deformation, however, must be done in an extremely sophisticated manner and the one best versed in this field is the explosive metal-forming industry. Considerable literature is available on the subject of explosive metal forming and we found that the techniques applied here could be almost directly applied to our own requirements. Further study in this field also revealed that of all the energy sources for high-velocity forming, the use of high explosives is perhaps the most versatile.[2] In the light of the explosive-forming business then, we have what is called a typical explosive working system. In order for such a system to operate successfully it must embody the following features: (1) an explosive charge; (2) an energy transmittal medium; (3) a die plate; and (4) a work piece.

Within our frame of reference (see Fig. 1) plosive charge is a Type RP-2 detonator manufact Reynolds Industries of California. It is of the miniature variety, 0.200-in. diameter and approx 0.450-in. long. There are two explosive charges tained in this unit weighing approximately 64 m first charge is low-density PETN located adjacen the gold bridge wire initiator. This type charg extremely fast burning, which in turn ignites a high-density charge of tetryl which acts as a hi energy booster. The manufacturer of these deton provides a rigidly controlled crystallization pr of the explosive and loading operation. Charge is controlled through consistency of crystalline ture and precision weighing. The result is a de with a transmission time simultaniety of ± 25 ns "energy transfer medium" is a material used not transmit a fast uniform shock wave, but also act efficient coupling agent. The most efficient ma for such purposes would be some incompressible l such as water or oil. Both these materials, thou ideal, would be difficult to contain in our part geometry without fairly elaborate sealing method Hence, our second choice material, paraffin, is agent currently in use. The paraffin is premold fit the conical void between the detonator and t piece, or driven plate as we call it (Fig. 1). "die plate" in our system is in the shape of a w made of 6061-T6 aluminum alloy, and although thi is replaced after each shot, its use performs an tant dual function. It not only "shapes" the de tion of the driven plate, but it also acts as a current joint edge. The "work piece" in our sys a piece of 1100-0 aluminum and is deformed by th panding gases in such a manner that the "die pla "driven plate" are intimately forced together. 2 shows the before and after explosion condition explanation of the explosive action is as follow detonator is assembled in the breech block with open end extending within the conical taper sect The pre-molded paraffin plug which acts as the t fer medium is then pressed into the taper sectio is extremely important that the front end of the nator is actually imbedded within the paraffin s the coupling effect between the explosion and th fin is thus more fully assured. The rear of the tor is closed off with a steel backup slug (see This slug is appropriately slotted to provide pa for the bridge wire leads, but it also prevents cessive loss of explosive pressure out the back. the detonator is fired, the incident shock wave in a spherical manner through the transfer-mediu rial. A uniform pressure front then exerts itse the area of driven plate as limited by the base the conical taper section. It is important here a thin film of grease between the transmitting m and driven plate to more effectively couple tha front and drives the plate. The O-ring, immediat outside this area, serves to contain the explosi and prevent any lateral pressure loss. As the u pressure wave hits the surface of the driven pla bending and extruding action takes place forcing plate material first against the anvil piece, wh current contact is initially made, then into the plate where it becomes imbedded in the annulus b the die-plate washer and the anvil. This action the polyethyleme insulator in the process and ac causes it to flow out-of-the-way and ahead of the

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advancing metal of the driven plate. The anvil, made of hardened steel and opened with a through-hole, not only provides for the essential venting of the die area, but also acts as a bumper which stops the driven-plate material in the restrictive fashion as shown, after initial current contact. The metal-to-metal contact thus made is extremely tight, comparable perhaps to a "press-fit" condition found between various machine elements. This contact completes the swithcing action between the positive and negative potentials as shown in Fig. 2.

When experimentation was originally started on the development of this detonator switch, some of the initial tests conducted were influenced to some degree by prior design criteria which had been used on the exploding foil switches.^{3} It soon became apparent that this influence, though not without merit, was just not applicable to detonator use. Consequently a new set of parameters had to be established and new lore developed.

Where the most efficient die geometry used in the foil switch was a slot, it was not so with the detonator. The slot configuration did appear somewhat faster in closing time, but the end effect, or the part at the end of the slot, did not fully close and presented a very marginal current contact and was found to cause arcing when the current was switched. This and other limitations of the slot geometry led to the adoption of the circle as a more ideal die-plate geometry where the circle's circumference became the effective length of current-carrying surface. Since the detonator shock wave expands in a spherical manner, the constraint of the circular hole geometry thus became ideal for assuring a uniform current contact on thin surface.

Additional lore was established after several shots were fired with the detonator in direct contact with the driven plate. This procedure, though effective with foil switches, was disastrous for the detonator switch. We simply blew a hole clear through the iriven plate and disintegrated the very material we ieeded to perform the switching action. After further study of explosive-forming references, we concluded that "contact operations" would not achieve our ends but rather the application of "stand-off" techniques would be more effective.

The terms "contact" and "stand-off" operations are simply the two main divisions used by the explosive metal-forming industry. "Contact" operations are those where the explosive charge is located directly, and in contact with, the work piece. The "stand-off" operations are those where the charge is placed some distance away from the work piece and the optimum distance away is some junction of the diameter of explosive harge. The most desirable condition in our case is ith the front end of the detonator at 0.100 in. from he driven plate, together with a 45° angle in the reech. This combination results in the most suitable eformation of the switch plate.

First Design

Due to space limitation as mentioned previously, ur first design was to incorporate this switch with a hrough bolt being used to hold the transmission lines ogether. Such an arrangement is shown in Fig. 3 where he switch was designed in a coaxial manner and as can e seen, it includes the necessary plate constraints as ll as the required switching characteristics. While he design was found to be workable, subsequent measurents showed its inductance as too excessive to warrant ts further development.

The calculated inductance, assuming the switch to made up of small "infinite" (Fig. 4) sections, was 5.7 nH. The inductance measured was ≈ 37 nH.

With the test circuit (Fig. 5) the switch carried to ≈ 125 kA with a 1/e decay of 600 μsec with negligible arcing. The closure time is defined as the time from the beginning of current to the detonator bridge wire to the beginning of current in the switch, and was 12 μsec ± 0.5 μsec. Figure 6 shows a current trace of the crowbar current. The peak current in the crowbar was 277 kA and the current being switched in the load was 170 kA with an 1/e decay time of 600 μsec.

In the ideal case where the crowbar is assumed to have no inductance and resistive effects are neglected the peak crowbar current is exactly double the current in the load. In the actual situation an accurate description of the switch capability includes two currents (1) the current in the load at the time of crowbar switch closure, and (2) the peak current the crowbar switch carries. Furthermore, the decay time of the current in the load is also an important parameter called the 1/e decay time or L/R time where L and R are the inductance and resistance respectively of the crowbar switch and load-cirucuit loop. Still referring to Fig. 6, notice that at about 300 μsec there is a discontinuity. This is presumably the point at which the switch began to burn. The 170 kA was much less than the expected 300 kA we were hoping to achieve. Although this was discouraging, it did provide very valuable information as to the maximum energy density we could hope to achieve with this switch when working in the range of 1/e decay times of 1 msec. Further, it provided the needed information to extrapolate the switch design and meet the switch requirements.

For the time of interest, i.e., up to the point the switch starts to burn, 300 μsec, the current is of the form

$$I = I_o e^{-R/L\ t} - I_o \cos \omega t\ e^{-r/\ell\ t} \quad .$$

Where, Fig. 5,

$$L/R = \frac{L_p + L_{cb}}{R_2} \quad ,$$

ω = ringing frequency of capacitor bank through L_p,

$$\ell/r = \frac{L_1 + L_{Ts} + L_p}{R_1} \quad ,$$

and

I_o = maximum average crowbar current.

Before the equation could be plotted, a determination of the four parameters, I_o, ω, L/R, ℓ/r, had to be made. By careful examination of the oscillogram, ω was measured . Between about 200 μsec and 300 μsec, the second term is absent from the equation due to ignition cut-off. By taking careful measurements of relative current amplitude and time at two different times, L/R could be found by the following equation:

$$L/R = \frac{t_2 - t_1}{\ln (I_2/I_1)} \quad .$$

This equation assumes R, the resistance, in the crowbar loop to be constant. This is not true because of the skin effect, however, it is a reasonable approximation and for the purpose of this calculation will be assumed. Since the current was measured with a calibrated Rogowski loop, I_o could be determined. The constant ℓ/r was determined by fitting the equation to th data. We can now calculate the total energy dissipate in the switch up to the time it started to burn. Usin

$$I_o = 158.5\ \text{kA} \quad ,$$

$$\omega = 1.84 \times 10^5 \quad ,$$

$$R/L = 1.67 \times 10^3 \quad ,$$

and

$$r/\ell = 1.72 \times 10^5 \quad ,$$

e have:

$$= \int_0^t I^2 R_s \, dt \quad ,$$

$$= \int_0^{300\ \mu\mathrm{sec}} \left(I_o e^{-R/L\ t} - I_o \cos \omega t\ e^{-r/\ell\ t}\right)^2 r_s \, dt \quad ,$$

$$= \int_0^{300\ \mu\mathrm{sec}} \left(I_o^2\ e^{-2\ R/L\ t} - 2\ I_o^2 \cos \omega t\ e^{-(R/L - r/\ell)\ t} + I_o^2 \cos^2 \omega t\ e^{-2\ r/\ell\ t}\right) R_s \, dt \quad .$$

ote: When the energy is actually calculated, one finds hat the last two terms actually contribute less than .5% to the total energy, when $t = \infty$.

$$E = 50 \text{ joules, assumes } R_s = 10\ \mu\Omega \ ,$$

$$\text{Energy density} = 12.5 \text{ joules/cm} \quad .$$

Second Design

The foregoing calculations served as a basis for second and much improved design. This concept, known s the transmission-plate design and the one currently n use, is shown in Fig. 7. As will be noted, this rrangement is without the through-bolt constraint eature, and though the bolt omission allows some plate eflection in this area, due to magnetic field pressure, t was not considered great enough to cause concern. By mitting the bolt, we were able to build the switch irectly into the transmission lines as shown. Several dditional features were also introduced at this time. y changing the thickness of the driven plate from .062 in. to 0.090 in., its penetration into the die late was greatly improved, thus doubling the energy issipation of this joint. The diameter of the hole n the die plate was enlarged by 20%, thus increasing ts current carrying capability. Additional venting of he anvil and die-plate areas further shortened the ffective closure time by eliminating excessive back ressure. Difficulties with the breech design led to ts further refinement through the study and use of rious materials. Cold rolled steel was first used t errosion and compaction of this material, due to he detonator explosion, increased the hole size or learance around the detonator to such an extent that ucceeding shots resulted in faulty reproducibility. ngsten alloy and tool steel were tried, but severe racking and continued errosion was observed. The material presently in use is AISI 4340 steel, heat treatd to approximately 250,000 psi. It appears to be rong enough and yet not too brittle to contain the plosive pressure without cracking. The errosion probm was eliminated by using a small steel sleeve fitted ound the detonator body. When the detonator fired, he errosion occurred on the inside of the sleeve only. using a new sleeve on each shot the breech material mains essentially uneffected.

Further refinements that were incorporated include st-acting constrainer yokes for both breech block de and anvil side, thus allowing rapid replacement d reassembly of parts. Suitable dies were designed economically form the driven-plate pieces as well dies for casting the conical paraffin slug. Elecical contacts to the detonator lead wires were simified, requiring only "banana plug" type connections the breech assemblies.

Tests were performed on this design and the following conditions were observed. A current of 280 kA in the load was crowbarred with subsequent $L/R \approx 1.2$ msec with no burning of the contact points, Fig. 8.

Switch Inductance. Referring to Fig. 5, careful measurement of the period of the circuit ringing with L_1 only and $L_1 + L_{Ts} + L_p$ only, with a calculation of L_{TS}, L_p was determined to be

$$L_p = 48 \text{ nH} \quad .$$

L_{CB} could be determined from the ripple on the crowbar current signal. Using the following equation and Fig. 9,

$$\frac{1/2\ B}{A} = \frac{L_{CB}}{L_p} \quad .$$

The inductance of the crowbar and transmission lines was determined to be 7.2 nH. Since much of the inductance is in the transmission lines, the inductance of the crowbar must be on the order of

$$L_{CB} \approx 2 - 3 \text{ nH} \quad .$$

Switch Resistrnce. A high resistance was connected directly across the transmission plates and the voltage was measured with a Pearson current transformer. The bottom trace, Fig. 10, shows the voltage across the switch. Notice that at about 200 μsec, $V = 0$ at this time, and;

$$L\dot{I} = IR$$

from the crowbar current trace about $\dot{I}$ was estimated to be 1.9×10^8 A/sec. At this time $I = 1.7 \times 10^5$ A. Using these figures and 2.5×10^{-9} H for the inductance,

$$R_S = 2.8\ \mu\Omega \quad .$$

High-Voltage Hold Off. The in-plate transmission-line switch was assembled on a test stand and connected to a 50-kV capacitor. The capacitor was charged to various voltages, the assembly was pulsed to a maximum of 42 kV and the switch fired. Each pulse the closure time was measured to determine the effect of the voltage on closing time of the switch. Figure 11, top trace, shows the high-voltage pulse being switched some 9 μsec after it comes on. The bottom trace shows the current in the detonator bridge wire. On the low-voltage, high-current tests the average closure time was $\tau c = 11$ μsec ± 0.3 μsec. With 42 kV on the switch, the closure time is affected and the closure time is shortened 2.0 μsec, Fig. 12.

Conclusions

A compact metal-contact crowbar switch that is activated by a small explosive charge (~ 100 mg HE) has been developed. The switch has a closure time of 11.0 μsec ± 0.3 μsec, with 0.040 in. polyethylene insulation. Both the resistance and inductance are very low, $R < 3\ \mu\Omega$, and $L < 3$ nH. The switch will crowbar a load current of 330 kA with a 1/e decay time of 1.2 msec. Due to the current doubling effect of crowbarring, the switch carries ≈ 600 kA on a short-time scale, several tens of μsec. Although the switch-closure time is slightly affected when it has high voltage on it, in crowbar use the voltage is small at switch closure. In the case of ZT-1,[3] a magnetic energy-storage system imposes a fast, high-voltage spike (60–80 kV; few tenths of a μsec long) on a load followed by a fast-rising current (rise time of 0.1 μsec) which rings with a sort of cosine wave (the period is 40–60 μsec). The crowbar switch was ideal in this case because it enabled crowbar of the load current 3.0 μsec after the high-voltage spike, still within 95% of peak current.

This switch has been developed using but a single detonator. It is not inconceivable, however, that considerably higher currents could be switched simply by using two or more similar detonators in the same systems and firing them in parallel. It is also possible to use other detonators having higher and faster powder charges, thus larger current contact areas could be effectively used.

While designed primarily as a crowbar switch, the detonator-switching action has also been used in other switch functions where low resistance and low inductance is a requirement.

References

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2. "High Velocity Forming of Metals," A.S.T.M., (1964).

3. J. A. Phillips, "Proposal for a Shock-Heated Toroidal Z-Pinch Experiment," Los Alamos Scientific Laboratory report LA-4352, (1969).

Captions

Fig. 1 Schematic of main switch features.

Fig. 2 Switch conditions before and after detonation.

Fig. 3 Throughbolt assembly.

Fig. 4 Inductance calculation schematic.

Fig. 5 Current test circuit.

Fig. 6 Crowbar current trace, throughbolt design.

Fig. 7 Transmission plate design.

Fig. 8 Crowbar current transmission plate design.

Fig. 9 Effect of source inductance on crowbar current ripple.

Fig. 10 Measurements for calculation of transmission plate inductance.

Fig. 11 Switching a high-voltage pulse.

Fig. 12 Closure time v.s. switch voltage.

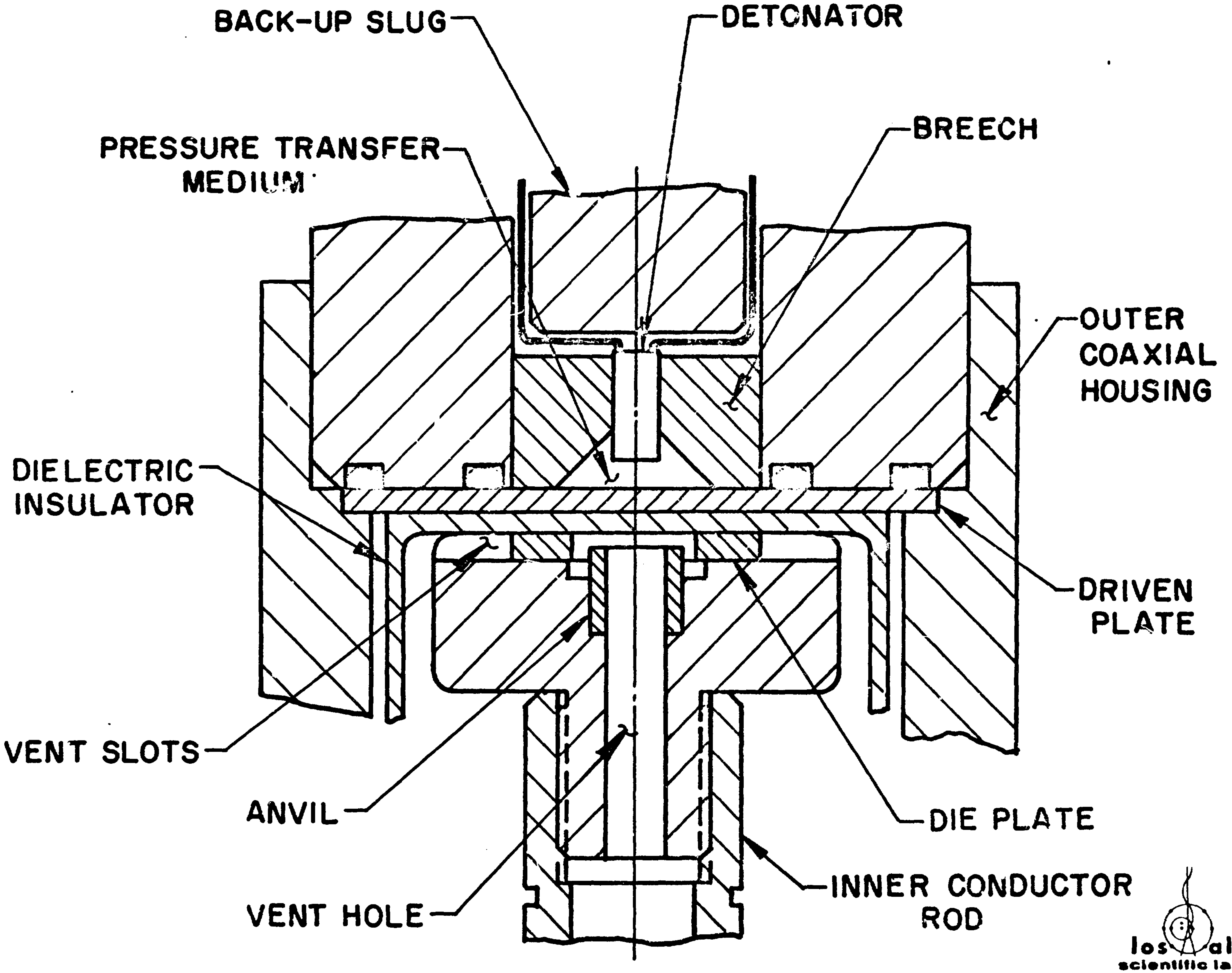

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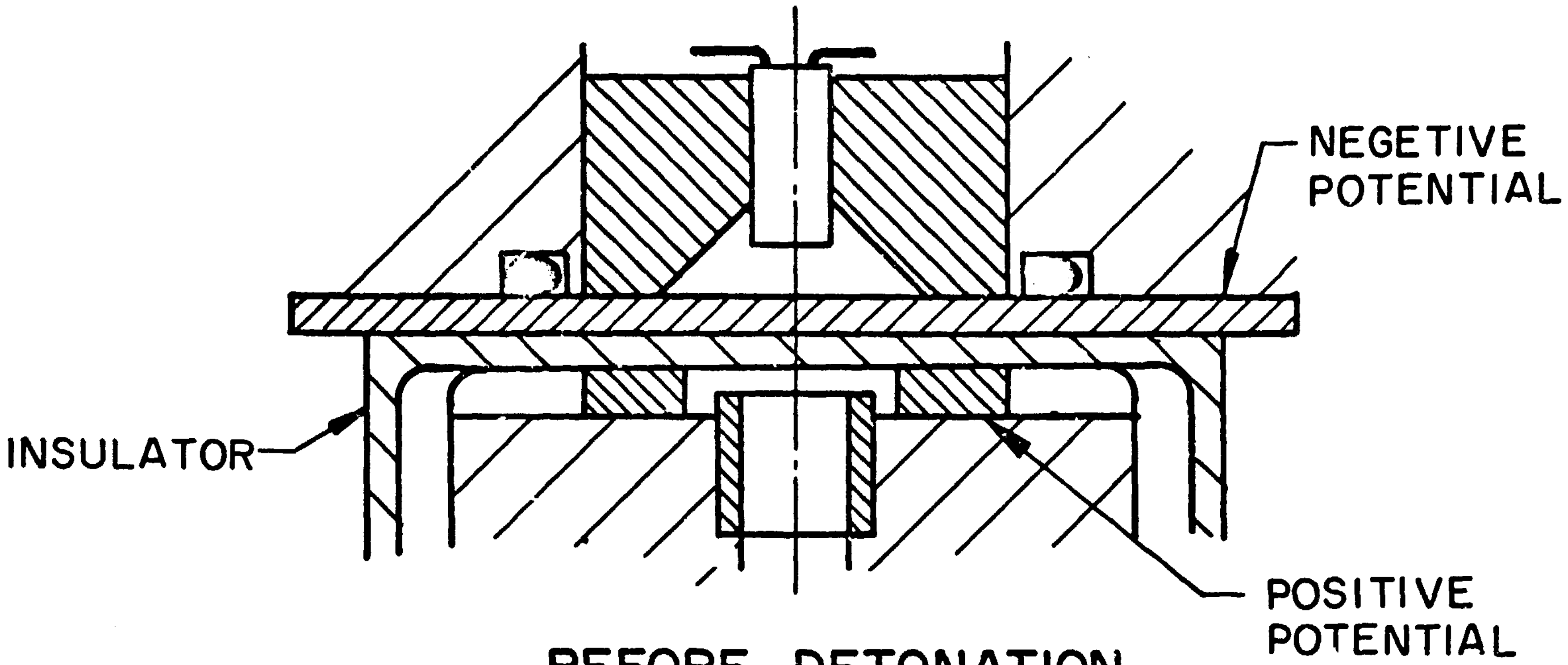
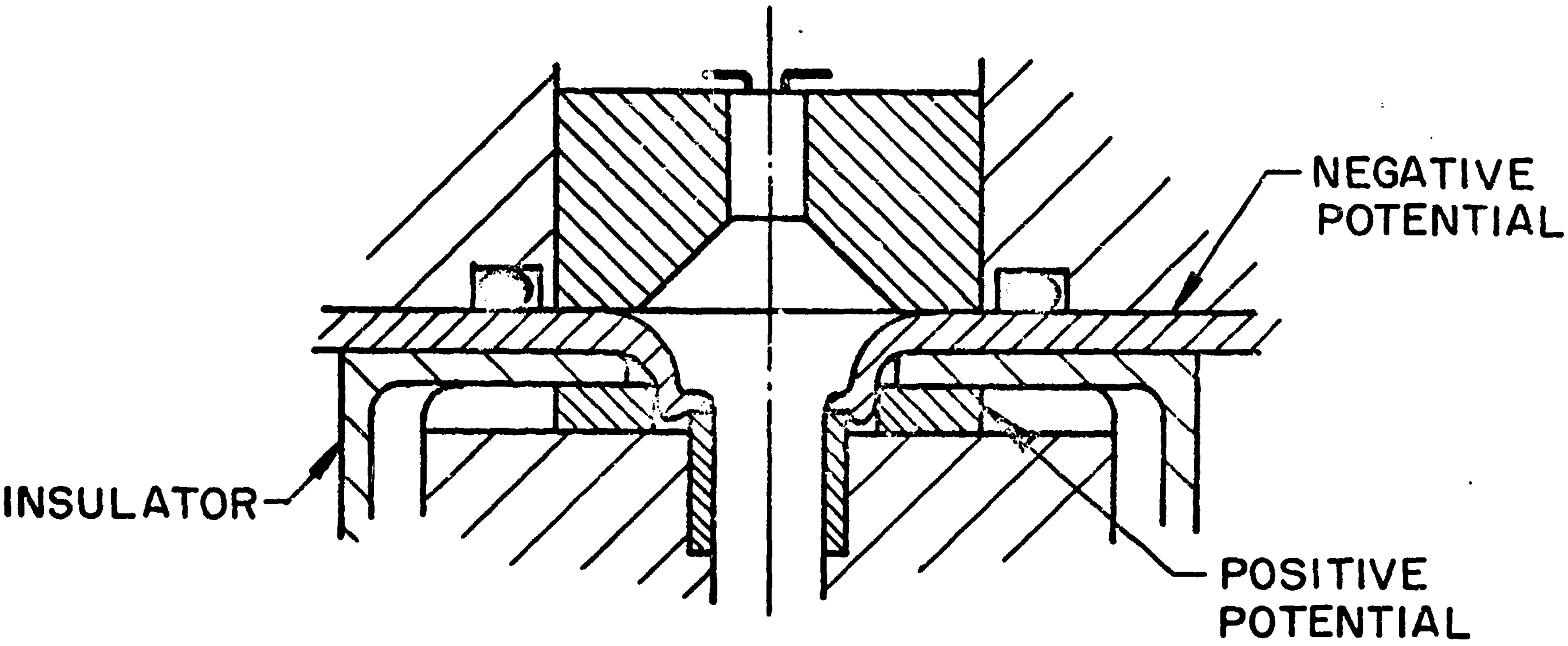
Fig. 1



BEFORE DETONATION



AFTER DETONATION

Fig 2

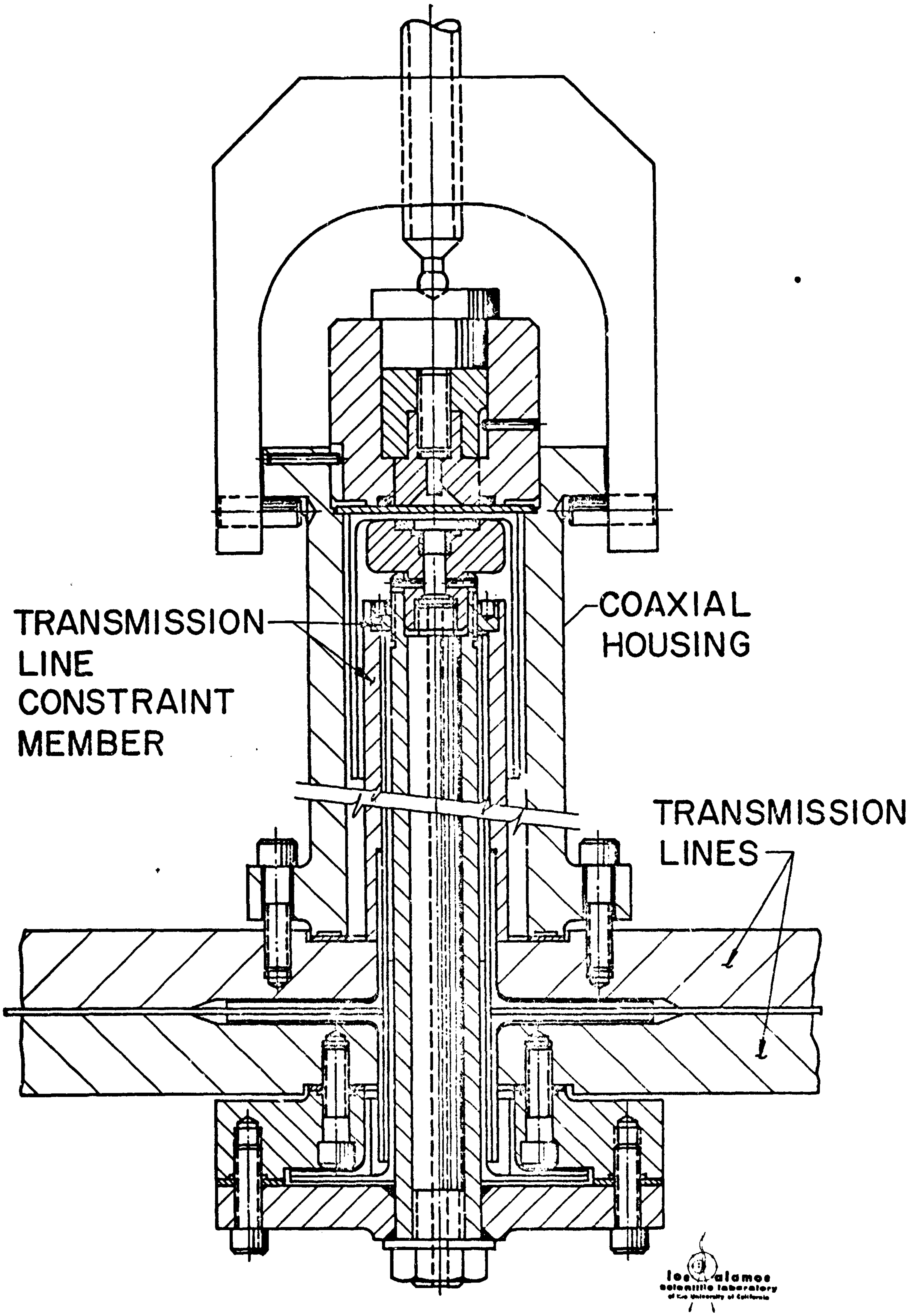
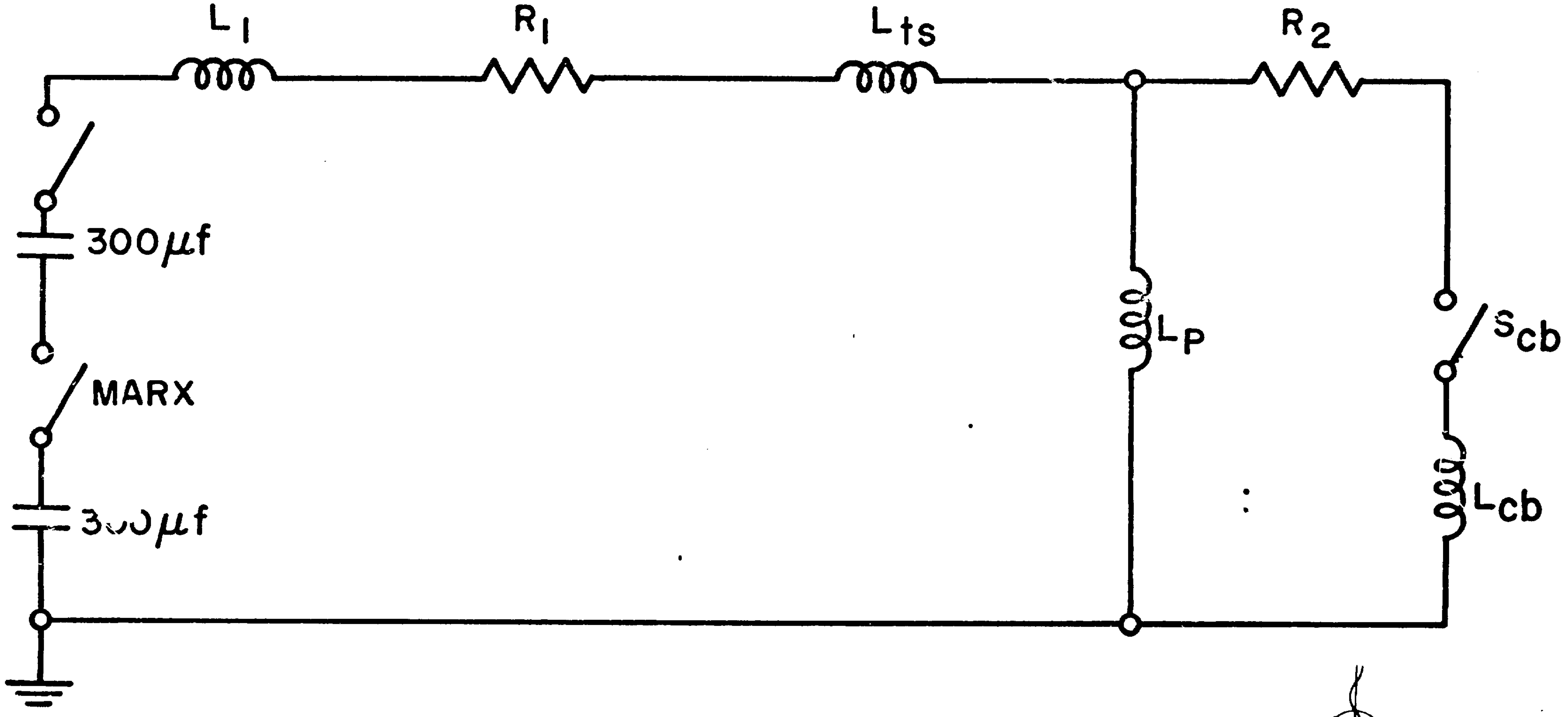

TRANSMISSION LINE CONSTRAINT MEMBER
COAXIAL HOUSING
TRANSMISSION LINES

Fig 3



L_1	SOURCE INDUCTANCE
L_{+s}	TRANSMISSION LINE INDUCTANCE
L_P	ALUMINUM PINCH INDUCTANCE
L_{cb}	CROWBAR INDUCTANCE
R_1	SOURCE RESISTANCE
R_2	PINCH AND CROWBAR RESISTANCE

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Fig 4

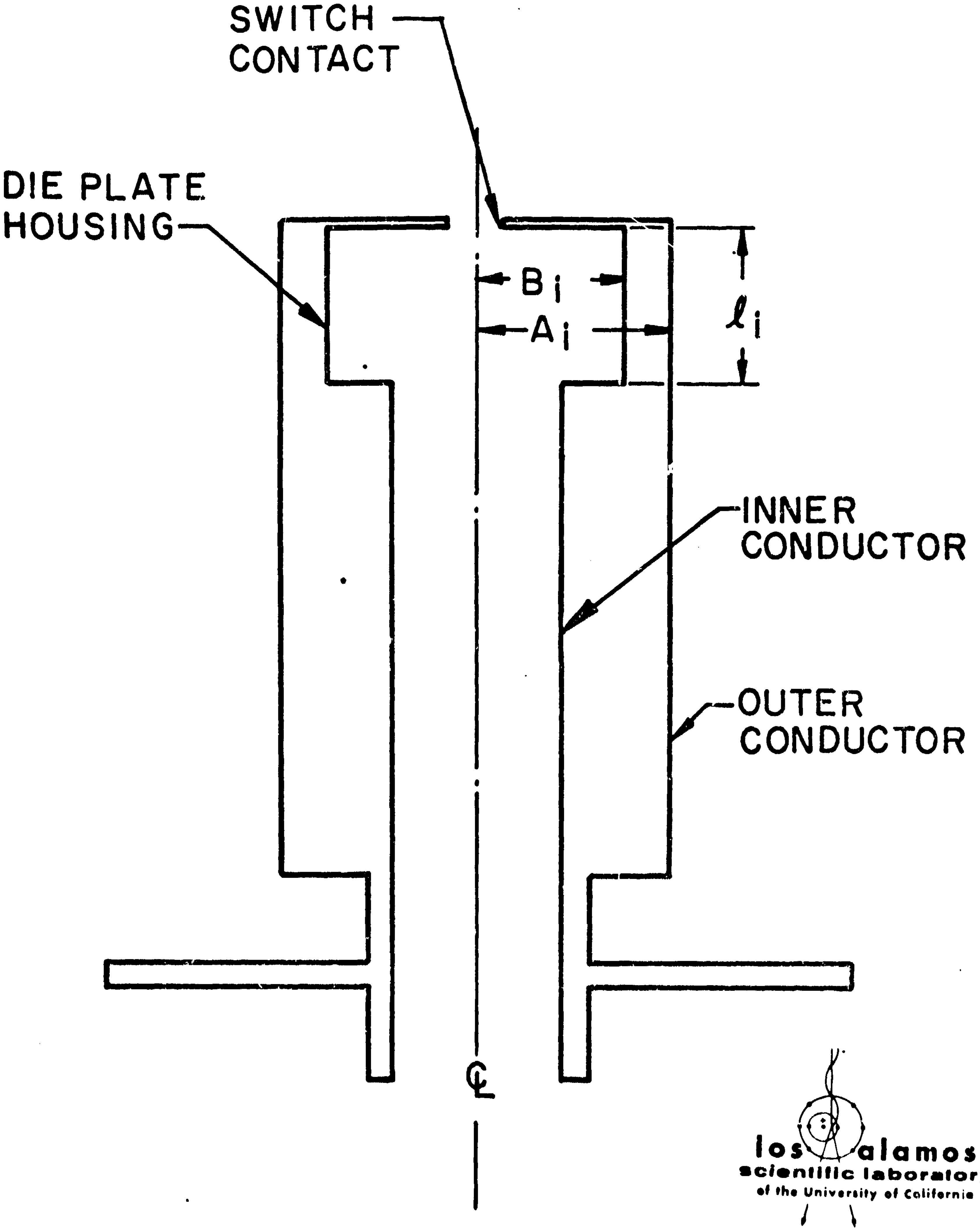
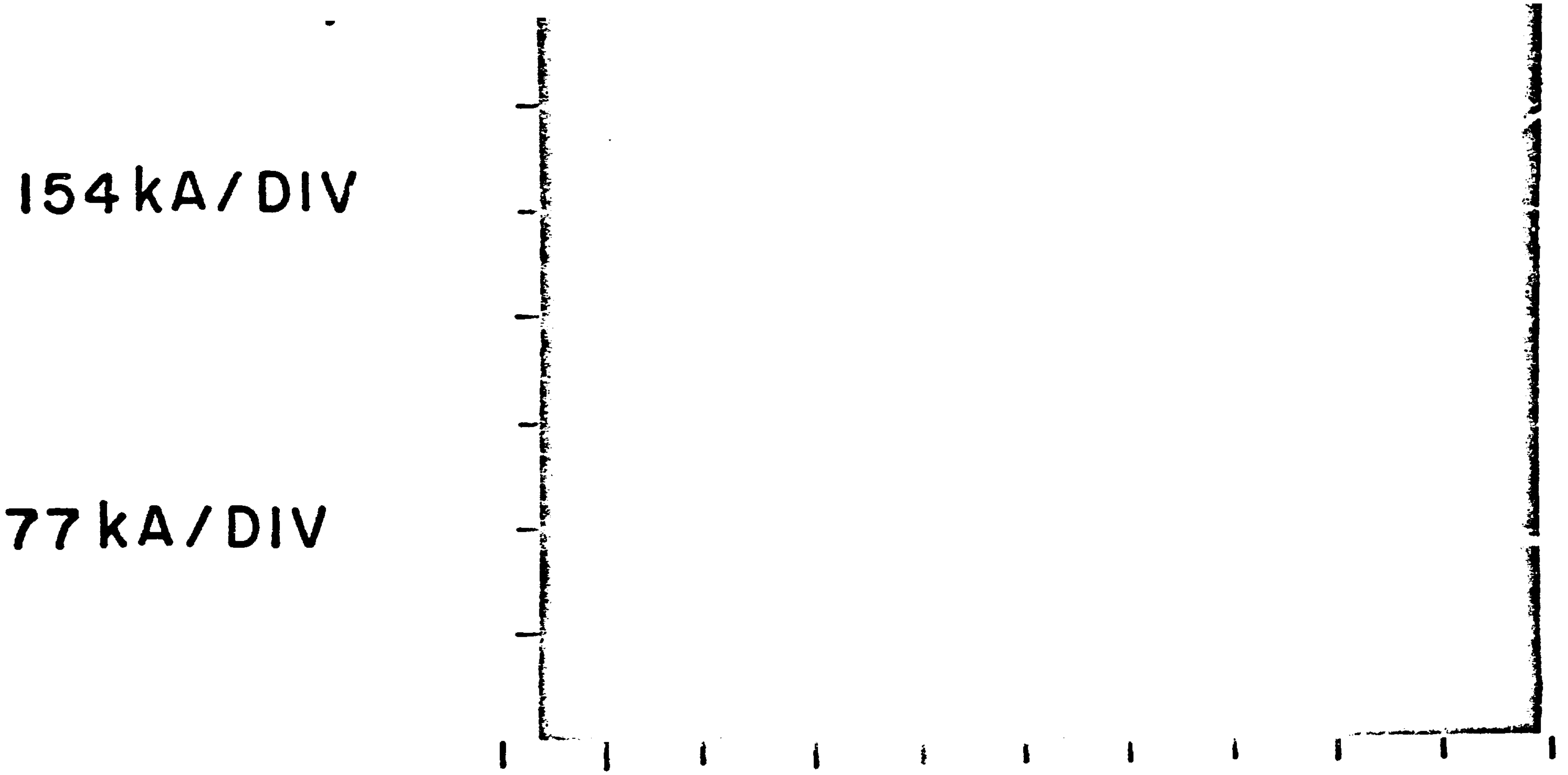

SWITCH CONTACT
DIE PLATE HOUSING
B_i
A_i
ℓ_i
INNER CONDUCTOR
OUTER CONDUCTOR
℄

Fig 5



CROWBAR CURRENT
TOP TRACE 10 μSEC/DIV
BOTTOM TRACE 100 μSEC/DIV

fig. 6

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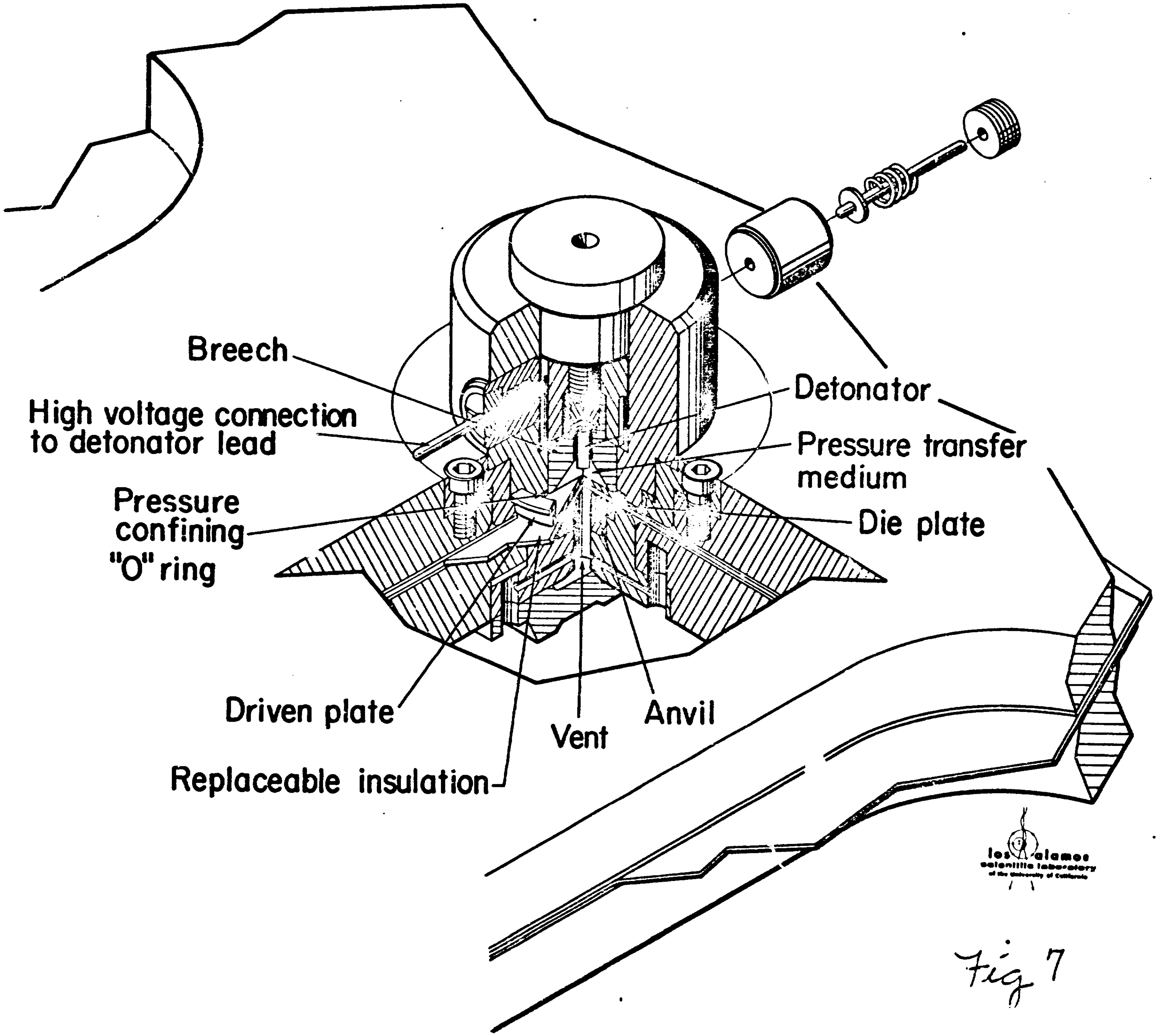

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Fig 7

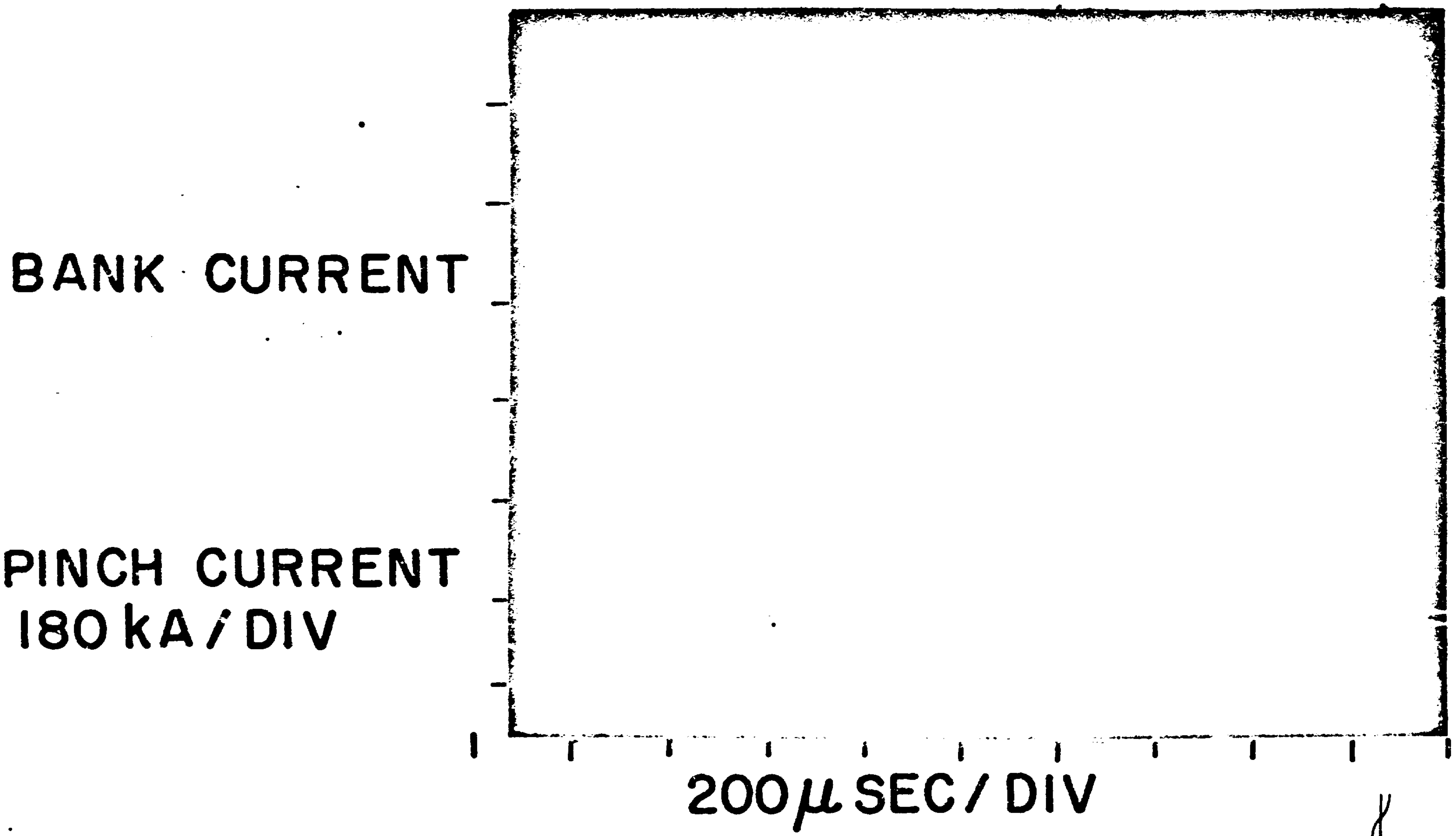

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Fig. 5

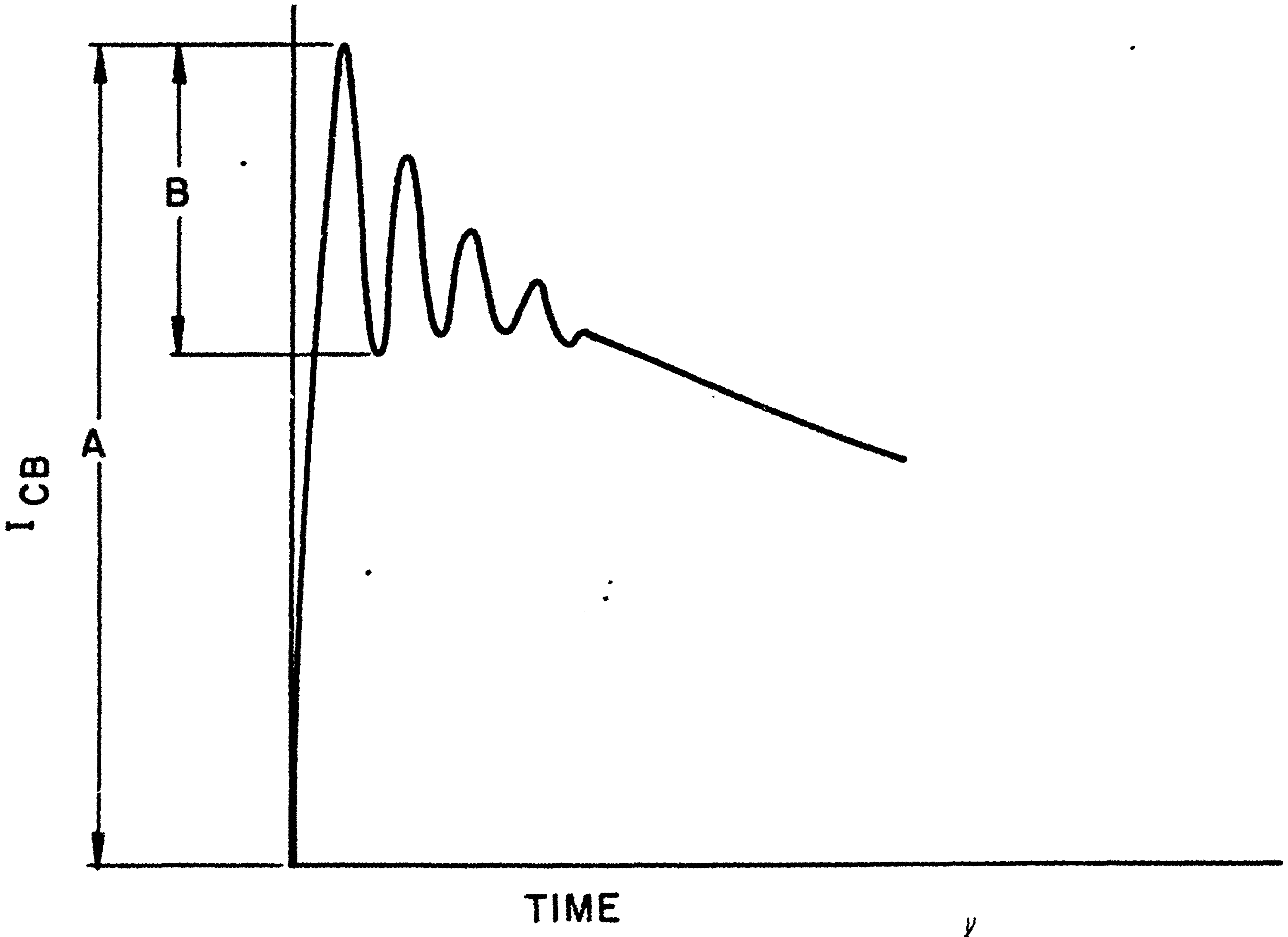

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Fig 9

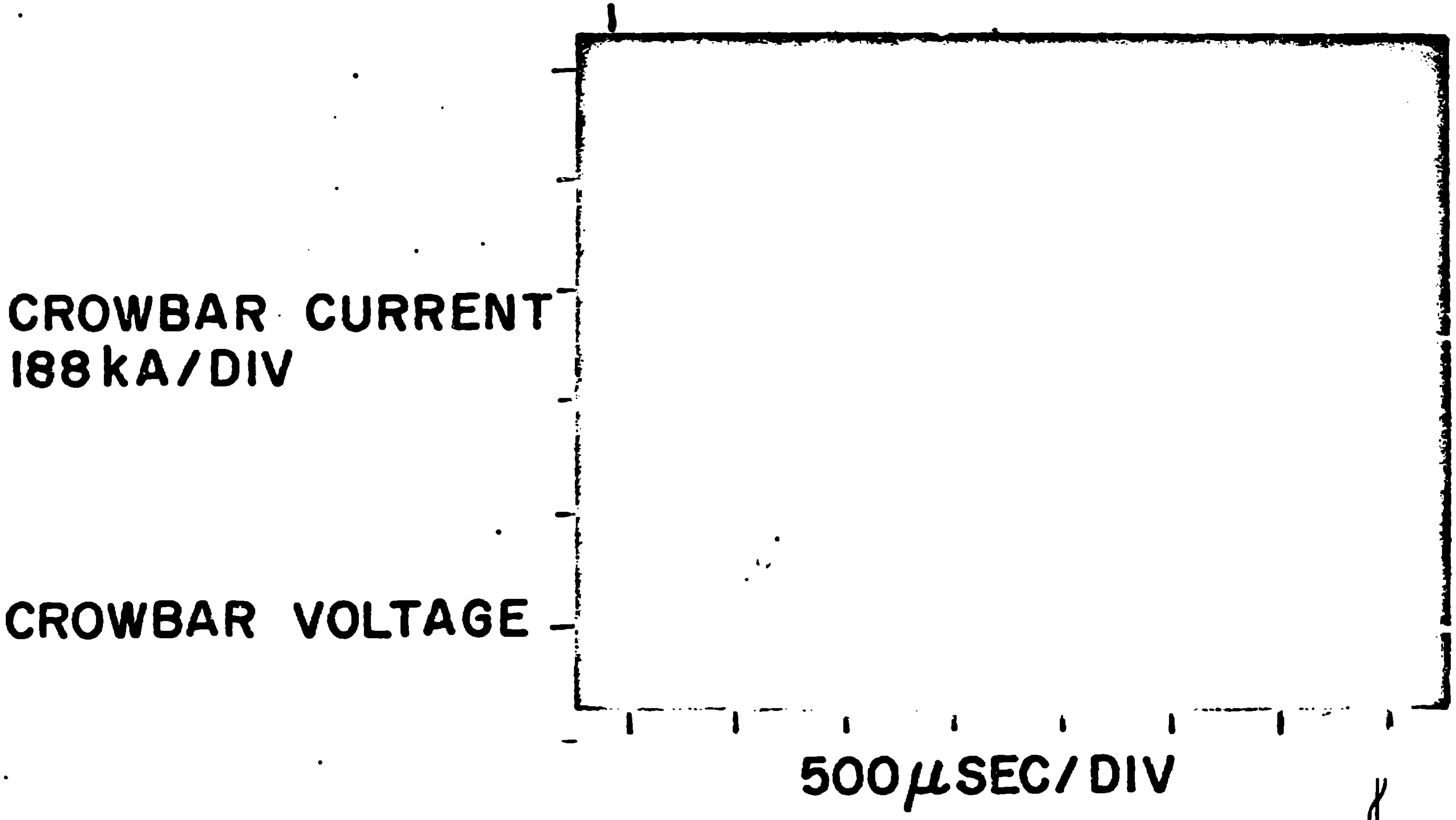

Fig 10

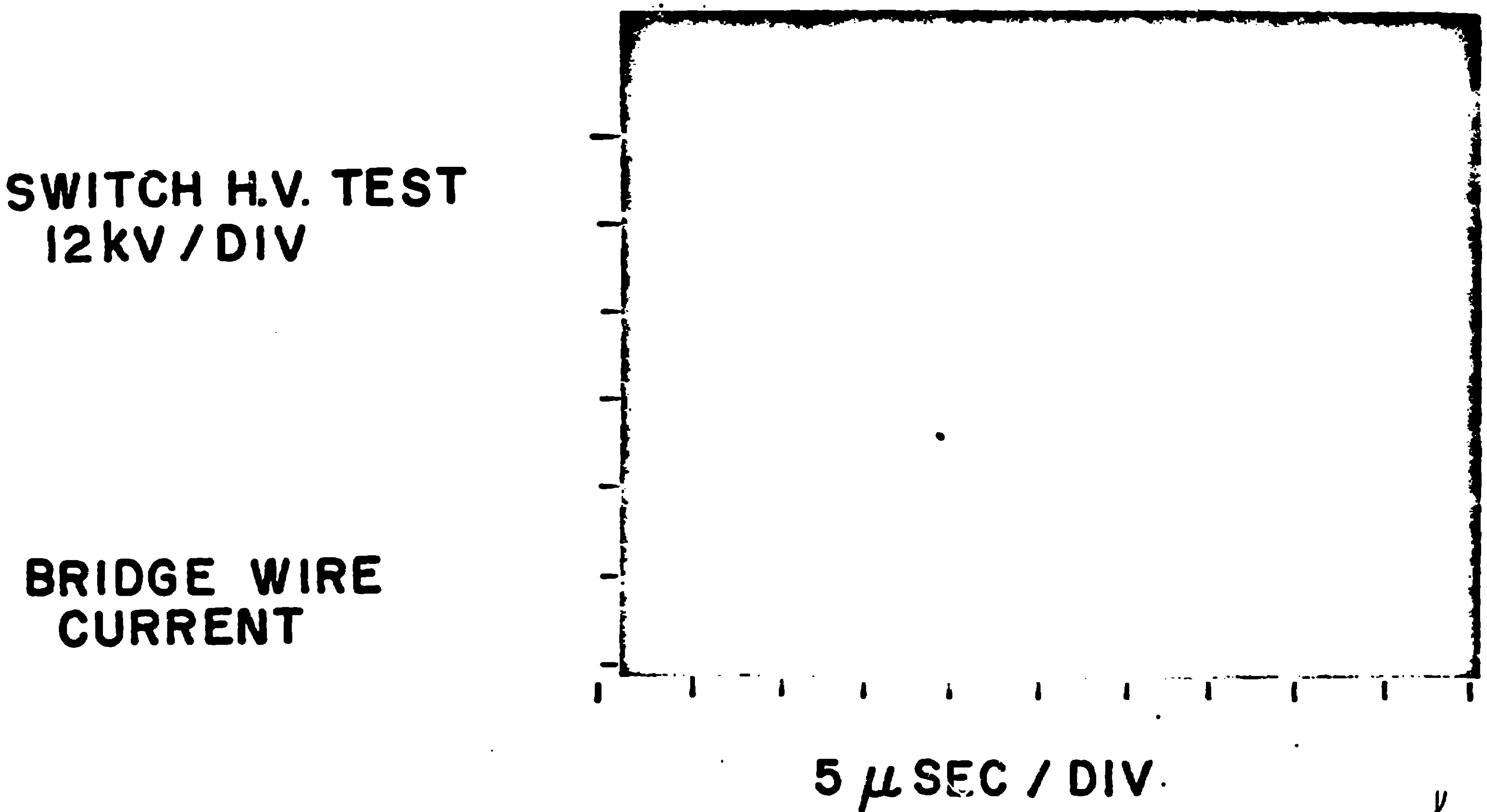

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Fig 11

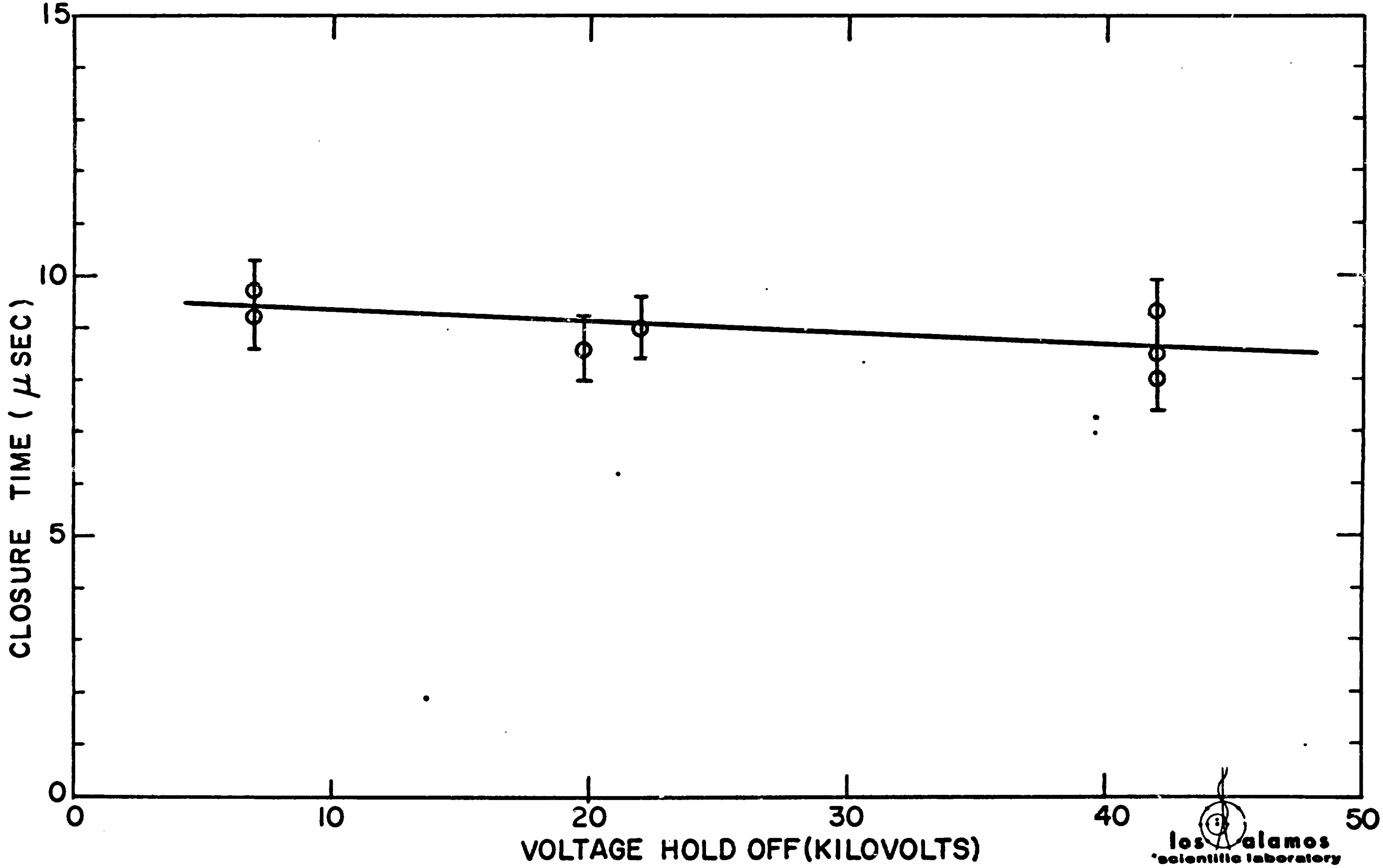

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Fig 12