conf. 790175--4



Form No. 8.00 St. No. 2629 1/75



WASTER UNITED STATES ENERGY RESEARCH AND EVELOPMENT ADMINISTRATION CONTRACT W-7405-ENG. 36

LARGE CERAMICS TOR FUSION APPLICATIONS

۰.

.

WILLARD E. HAUTH and STEPHEN D. STODDARD

Los Alamos Scientific Laboratory, Los Alamos, New Mexico 87545, USA

Prominent ceramic raw materials and products manufacturers were surveyed to determine the state of the art for alumina ceramic fabrication. This survey emphasized current capabilities and limitations for fabrication of large, high-density, high-purity, complex shapes. Some directions are suggested for future needs and development.

Ceramic-to-ceramic availing has applications for several technologies that require large and/or complex vacuum-tight ceramic anapes. Information is provided concerning the assembly of complex monolithic ceramic shapes by bonding of subassemblies at temperatures ranging from 450 to 1500°C. Future applications and fabrication techniques for various materials are presented.

LARGE CERAMICS FOR FUSION APPLICATIONS

WILLARD E. HAUTH and STEPHEN D. STODDARD

Los Alamos Scientific Laboratory, Los Alamoa, New Mexico 87545, USA

Promiment ceramic raw materials and products manufacturers were surveyed to determine the state of the art for elumina ceramic fabrication. This survey emphasized current capabilities and limitations for fabrication of large, high-density, high-purity, complex shapes. Some directions are suggested for future needa and development.

Ceramic-to-ceramic sealing has applications for several technologies that require large and/or complex vacuum-tight ceramic shapes. Information is provided concerning the assembly of complex monolithic ceramic shapes by bonding of subassemblies at temperatures ranging from 450 to 1500°C. Future applications and fabrication techniques for various materials are presented.

1. INTRODUCTION

Large, vacuum-tight ceramic components are needed by the fusion community for a number of applications including Tokamak current breaks, neutral beam injector insulators, auperconducting magnet insulation, and several first wall requirements. The entire plasma containment vessels for Reverse Field Pinch Machines are ceramic.

The electrical insulation properties of ceramic matarials coupled with high purity, chemical stability, strength, and resistance to heat and radiation damage make them attractive, in fact necessary, for many fusion applications. Most high purity caramics are commercially available only in relatively small aizes, while very large ceramic ahapes are often required for fusion. The use of ceramic ahapes having dimensions in the range of one to three meters has been proposed for some applications.

In the first aection of this report we deacribad the results of a survey of the major American tachnical caramic manufacturers to datermine the aize limitations for commercially available caramics. In the aecond report section methods of joining ceramics components to form large, complex ceramics shapes are reported.

2. INDUSTRIAL CAPABILITY FOR LARGE CERAMIC SHAPE FABRICATION

In order to define industrial capabilities for fabrication of large, high purity caramic products in commercial quantities a survey of the major technical caramic manufacturars was undertaken. Although there are technologies for fabricating large, high density, high purity parts from savaral caramic materials, alumina is the predominant commercial material. Accordingly, the aurvey was conducted to determine the state of the art for alumina ceramics fabrication.[1]

The five primary concerns for which this survey sought industrial input are presented in Table I.

Table I

Examples of Information Requested

- Variety of chemistry in commerical bodies including alumina content and major impurities.
- Maximum sizes of regular and irregular shapes within fabrication capabilities.
- Types of forming, firing, and finishing facilitias.
- Areas of current technology that show potential for large shapes.
- 5. Vital factors in future capability devalopment.

This aurvay also was designed to obtain information about the relationship between raw data points. For axample, it is useful to know if fabrication of large plates is kimited more by composition than by fabrication or firing system size.

The largest size capability reported for rectangular plates was 560-mm long by 500-mm wide by 40-mm thick. The largest right circular cylinder was 510-mm o.d. by 460-mm long with a 40-mm-thick wall. These sizes are genarally independent of composition with the axception of bodies containing more than 99.5% alumine. Limiting sizes were also smaller for rlip cast parts than for those made by dry or isostatic pressing. When these sizes were limited by aquipment capacity it was a result of a size limitation imposed by the caramic manufacturer or because of a lack of consumer interast in larger sizes. The fired densities reported for these parts range from 3.40 to 3.94 Mg/m^2 (i.e. 90 to 97% theoretical density).

Responses to quastions concerning large, complex shape fabrication indicate a general lack of experience in this area. Most frequently these parts are formed by isopressing a billet and machining to the required shape. The current limiting size for finished parts is about 130 by 130 by 120 mm.

It is apparent that the primary factor limiting fabricated part size capability has been the lack of commercial interest in large, high purity parts. The consensus among survey respondents is that dimensions of one-half to one meter would involve very little extension of existing technology, particularly for relatively aimple shapes. This opinion presupposes significant interest and financial support for the purchase of larger capacity forming and firing equipment. Significant incrasses shows shout a one meter dimension and/ or an increase in complexity will require a well-designed davalopment program as well as the procurement of large capacity forming and firing equipment, ample raw material, and sufficiant anergy supplies.

The commercial alumina compositions of primary interest for use as containment systema contain at least 99.0% alumina. This requirement has been based on the need to minimize materials additions that would reduce the chamical and/or physical atability of the containment system in fusion anvironmants. This aquirament has not been corroborated by axperiments' avidence. The information presented is limited to industrial fabrication of bodies with greater than 95% alumins. It should be noted that aignificant increases in current part size capabilities could be applied to some of the proposed ceramic requirements if a concession could be made in favor of lower alumina content of the ceramic bodies (e.g. electrical porcalain, etc.).

Several materials and fabrication techniques have shown promise for extension of existing technologies to the fabrication of large and/or complex shapes. These promising areas include improvements of forming and firing systems, use of materials with increased reactivity, improving energy afficiency, and the use of component joining techniques.

- 3. FABRICATION OF LARGE SHAPES BY COMPONENT JOINING TECHNIQUES
- 3.1 Bonding with no chamical variation

Savaral projects requiring fabrication of

large, high purity, vacuum-tight caramic shapes have been pursued successfully at the Los Alemos Scientific Laboratory (LASL) by means of caramic-t>-ceramic sealing of fired and ground aubaraemblias. Fabrication of large and/or complex, monolithic ceramic shapes in this manmer has not been an astablished commercial capability for high purity ceramic materials.

One approach that has been developed at LASL for ceramic-to-ceramic sealing involves bonding of ceramic components to provide an assembly that is monolithic with regard to both chemistry and refractoriness. This approach consists of sealing two or more ceramic parts using a slip or paste of the same composition as the parts being acaled. An example of a complex, highpurity alumina ahape fabricated using this acaling technique is that of a pump-out port (Fig. 1) that was used in a ceramic thermonuclear fusion containment system for the Syllac machine.



Fig. 1. Syllac Pump-Out Port

Because of the complexity of the port, it cannot be fabricated by conventional ceramic forming techniques. The bonds of the port are formed by applying the joining sealant onto the joint area between two unfired praformed shapes. High temperature firing provides a fully aintered port that is monolithic with regard to both atrength, chemical composition, and vacuum integrity. This technique also has been applied auccassfully to othar high purity oxide systems including magnesis, zirconis, and thoris. This technology, although developed for relatively amall, complex parts, could be axtended to larger shapes given adequate capacity forming and firing aquipment.

3.2 Glass seelent joining

Joining of aubaaaamblias using glass acalants provides a vary useful method for fabricating asaemblica when chemistry and/or rafractoriness are not major considerations.

The basic materials requirements of acalants for large ceramic-to-ceramic acals are: (1) compatible CTE between the components and the acalant; (2) good acaling action when fired at relatively alow heating rates to minimize thermal atresses in the bonded components; and (3) mealants that form a acal and mature chemically at temperatures significantly below the softening or alumping point of the components being scaled. In addition, it is highly desirable to have several scalant materials with maturing conditions covering a wide temperature range.

Seven glass and glass-ceramic materials have been developed or modified at LASL [2] for use in joining of subassemblies. These sealants cover the maturing temperature range from 450° to 1500°C. The general approach used to develop these scalant materials started with a review of materials that form glasses and glazes [3,4], phase equilibria [5] of the systems containing these materials, and estimation of CTE for matured glasses and glazes.[6] Each candidate sealant resulting from the evaluation of these data was tested for its ability to exhibit flow, limited reactivity and compatibility of CTE when matured in contact with highpurity alumina shapes. Sealants that proved successful in these evaluations were then tested for bulk tensile strength using a bonded step joint. All of the sealants described proved to be as strong or stronger than the alumina shapes being bonded in this particular atep joint design.

The group of sealants that have been developed have a wide variation in chemistry as a result of the need to maintain a glassy phase with a compatible CTE to alumina while allowing refractoriness over a large temperature range. The materials systems used to develop these sealants include PbO-B₂O₃-SiO₂, BaO-B₂O₃-Al₂O₃, and K₂O-Al₂O₃-SiO₂.

Figures 2 and 3 show assemblies fabricated using the glass sealant approach. Figure 2 ahows a 30-cm-diam cylinder of 99.5% alumina which includee seven sapphire windows hermetically asaled in the wall using sealants of six different compositions. Figure 3 ahows an asaembly of eight 20-cm-diam 96% alumina cylinders that has been sealed using four different sealants. During fab.icstion of these sealed assemblias, some of the seals were rafired aeveral times, in some cases using their original maturing conditions, with no apparant affact on the seal integrity.



Fig. 2. Multiple Window Seal Segment



Fig. 3. Multiple Segment Seals

Each of the sealants described above has been used to repair unmatisfactory seals formed by other glass sealants with equal or higher maturing temperature. This capability enhances the versatility of this group of sealants. For example, given the requirement for fabrication of a complex alumina assembly, seals and/or coatings may be applied to the developing assembly in at least six different atages. Each stage, avolving at a lower maturing temperature, would provide the capability to repair any defective aeals appearing during prior processing.

4. SUMMARY

Industrial sizes of high purity ceramic parts are currently limited to relatively simple shapes with maximum dimensions in the range of one-half meter. The availability in acaling systems, such as those described, greatly expands current commercial fabrication capabilities for large and/or complex alumina shapes. The capability has been demonstrated to form multiple, vacuum-tight seals up to 5.0-m long between alumina and/or sapphire parts during one or more firing operations using the compositions described. These sealants also were used to repair and/or modify previously formed seals. It is felt that there is a potential for application of these technologies to other ceramic systems.

REFERENCES

- W. E. Hauth and S. D. Stoddard, "State-ofthe-Art--Alumina Ceramics For Energy Applications," Bull. Am. Ceram. Soc. <u>57</u> (2), 1978.
- Willard E. Hauth, "Ceramic-to-Ceramic Sealing of Large Shapes," submitted for publication to the American Ceramic Society, Inc., 1978.
- 3. H. Rawson, <u>Inorganic Glass Forming Systems</u> (Academic Press, New York, 1967).
- 4. George W. Morey, <u>The Properties of Glass</u> (Van Nostrand Reinhold Co., New York, 1954).
- Ernest M. Levin and Howard F. McMurdie, <u>Phase Diagrams for Ceramists</u> (American Ceramic Society, Inc., Columbus, Ohio, 1975).
- Cullen W. Parmelee, <u>Ceramic Glazes</u> (Cahners Publishing Co., Inc., Boston, Massachusetts, 1973).

t

PRESCHEDULED AUTOSTART program which zeros the common area status words and CONNECTS the RMI interrupts. If errors are detected during this initialization the operator is notified that all or part of the communication system is not operational.

Common Block Structure

Each of the four common areas is structured as in the following diagram:



Status Word (RRXSTA)

The common status word has the following bit definitions:

EQU Bit Meaning

1

- RPXESY 0 Set if the common area is busy.
- REMONE 1 On-line test bit. The requesting computer can set this

bit and interrupt the other computer to see if the other computer is on-line. The other computer should reset this bit to indicate that it is on-line. At the present time the on-line test bit is not used. If an attempt is made to request a service from an off-line computer the symbiont will relinquish forever while waiting for the "operation completed" bit to be set.

- RRXASS 2 Set if the requested file is not assigned in the task of the remote computer.
- RRXHOL 3 I/O hold condition. Set if the remote device is not ready and action by the operator is required. This indicates that the symbiont is in a "stall" condition.
 - 4 Spare
 - 5 Spare
- 6,7,8,9 Bits 6,7,8,9 are reserved for future services other than REX I/O requests. For example, other types of REX services or simple core-to-core data transfers.
- RRXREQ 10 Set if a REX I/O request is the service requested.
- RRXCOM 11 Operation complete. Set if the remote operation has been completed.
 - CC Bits 12,13,14,15 are used to transmit back to the requesting cpu the condition codes as returned by the remote REX I/O service. At the present time the symbiont does not use this information.

Other EQU Locations

- RRXLNT 192 Length of an individual common area.
- MYCPU #BF Actual memory location of the cpu number (0,1,2). This location is actually reserved by the system for the 63rd party line interrupt vector.

Some Comments on the Tasks Which Pespond to the PMI Interrupts PHP, RVR, RTP

These tasks are actually two source codes because the DMP's of the satellite computers cannot access the common memory which resides in the host. That is, RVR and RTR are identical and RHR must transfer the I/O buffer from its private memory to the common area for a write operation using the DMP and from common to private with a read operation using the EMP.

The tasks are designed to be general programs which can perform remote functions other than REK I/O services.

Resources of the Tasks

Fig. 5 and Fig 6 are sample listings of the resources of the tasks as they might be cataloged.

Notice also that practically all of the disc files on the Host are accessible by the satellites, but only two files (BSL and the random access file RAD) on the satellites are accessible by the Host. Like the magnetic tapes and the card reader these disc files also have <u>logical file</u> names which are the same as the device names. The exceptions to this are those disc files and devices which exist on all machines.

Fig. 6 is a list of the resources of the symbionts RT, RH AND RV. The source codes and resources for these symbionts are identical.

Error Conditions

Various error conditions can arise during operation of the symbiont. These are outlined below:

ErrorActionFile not assigned at the
remote opuThe symbiont types "FILE xx NOT ASSIGNED AT
PEMOTE CPU" and aborts the calling program.
Here xx is the name of the file after all file-
to-file assignments have been resolved.
Note that files may be "protected" by not

SOURCE OF RESOURCES FOR RTR

-

SOURCE OF RESOURCES FOR RVR

DEFAULT FILL SM #C8 #C8 TASK RTR STACKS #0064 #000C IUPERATIONS #02 PAGESHARING #01 SYSPAGES #02 DEALLUCATE ALL BIAS #0000 OPTION NO6 UPTIUN 6 LUGFILE MC SSL.SSL. LUGFILE MT1 MT1.MT1. LUGFILE MT2 MT2, MT2, LUGFILE CR CR, CR, LOGFILE PSL PSL, PSL, LOGFILE FSL FSL, FSL, LUGFILE SSL SSL, SSL. LOGFILE AS7 AS7.AS7. LOGFILE DNO DNO, DNO, LUGFILE DNA DNA.DNA. LOGFILE DNB DNB+DNB+ LUGFILE DNC DNC. DNC. LUGFILE SND DND. DND. LOGFILE AS1 AS1, AS1, LUGFILE AS2 AS2. AS2. LC"FILE AS3 AS3.453. LUSFILE AS4 AS4.AS4. LUGFILE AS5 AS5.AS5. LUGFILE AS6 AS6.AS6. LUGFILES #04 LUGFILE OPH OPM. OPM. LOGFILE LP LP2+LP2+ LUGFILE ULH BSL BSL LUGFILL TYH IY. TY. LUGHILE RAH RAD.RAU. LUGFILE MAR MAR.MAR. 10 3 5 70 PECULIAR PRIVLEGED SPACE #0000 #0000

DEFRULT FILE SM #C8 #C8 TASK HVR STACKS #0064 #000C IUPERATIONS #02 PAGESHARING #01 SYSPAGES #02 DEALLOCATE ALL BIAS #000U UPTION NUG UPTION 6 LOGFILE MC SSL.SSL. LOGFILE MT1 MT1.MT1. LUGFILE MT2 MT2.MT2. LOGFILE CR CR. CR. LUGFILE PSL PSL PSL LUGFILE FSL FSL.FSL. LOGFILE SSL SSL, SSL, LOGFILE AS7 AS7, AS7, LUGFILE DNU DNU, DNO, LUGFILES #04 LUGFILE ONA DNA.DNA. LUGFILE DIVE DIVE. DIVE. LUGFILE DIVC DIVC . DIVC . LOGFILE DND DND. DND. LUGFILE AS1 AS1.AS1. LUGFILE AS2 AS2.AS2. LUGFILE AS3 AS3+AS3+ LOGFILE AS4 AS4.AS4. LUGFILE AS5 AS5+AS5+ LUGFILE AS6 AS6. AS6. LUGFILE UPM OPHIOPMI LUGFILE LP LP1+LP1+ LUGFILE MAE MAE MAF. LUGFILE ULH BSL+BSL+ LOGFILE TYH TY. IY. LUGFILE RAH KAD+KAD+ 10 3 5 76 PECULIAR PRIVLEGED SPACE #0000 #0000

SOURCE OF RESCURCES FOR RHR

DEFAULT FILE SM TASK RHR #FF #FF STACKS #0064 #000C LOPERATIONS #02 PAGESHARING #01 SYSPAGES #02 DEALLOCATE ALL BIAS #0000 LUGFILES #04 LUGFILE ULV BSL+BSL+ LUGITLE ULT BSL+BSL+ LUGFILE TYV 11. 11. LUGFILE TYT TY, TY, LOGFILE RAV RAU, RAD, LUGFILE RAT RAD.RAU. IU 3575 PECULIAR PRIVLEGED SPACE #0000 #0000

SOURCE OF RESOURCES FOR RH

ULFAULT FILE SM TASK RH #FF HU6 STACKS #0064 #0008 IUPERATIONS #110 PAGESHAR1NG #01 SYSPAGES #02 DEALLUCATE ALL BIAS #0000 10 3 5 76 PECULIAR PRIVLEGED PECULIAR SYMBIONT SPACE #0000 #0000

.

assigning them in the task of the target cpu or by not placing them in the SYSGEN of the sending cpu.

Remote device is off line Types "REMOTE DEVICE xx IS OFFLINE" and sets the symbiont device off-line. Here xx is the actual device name.

Remote card reader/punch, paper tape reader/punch or printer is not ready The symbiont types "!xx ? (bell)" and goes into a "stall" condition until the operator either fixes the device or aborts the calling program. When the remote device is made ready the I/O will resume.

The program aborts during a remote I/O operation and leaves the "common busy" bit set.

At the moment the common status word must be zeroed using the operator command "//MAC" -modify actual memory. A better way might be to put this into an operator command (OC) to initialize the communications symbiont and common areas. In the six months we have been using the system, however, this error has yet to occur.

SYSGEN Statements

The following SYSGEN statements were added to the Host SYSGEN source:

MYCPU BORG	#BF,2	HOST IS CPU 2	
GLOBAL	GXFER,3,,,252,XCPU	COMMON FOR COMMUNICATIONS	
SYMCONTROL	LER RV	SYMBIONT FOP VERTICAL	<i>i</i> .
SYMCONTROL	LER RT	SYMBIONT FOR TANDEM	
DEVICE	<pre>ILV.RV,200,1,,,0,0,0</pre>	0,0,0,0,0 USER LIB ON VERTICAL	
D'EVIC E		,0,0,0,0 USER LIE ON TANDEM	
DEVICE	PAV,RV,200,1,.,0,0,0	0,0,0,0,0 RAND. ACCESS VERTICAL	
DEVICE	RAT,RV,200,1,,,0,0,0	,0,0,0,0 RAND. ACCESS TANDEM	
DEVICE	TYV,RV,80	TYPEWRITER ON VERTICAL	I
DEVICE	TYT,RT,80	TYPEWRITER ON TANDEM	:
PRESCHEDUL	E RV,,SM	SYMETONT TO VERTICAL	
PRESCHEDUL	E RT,,SM	SYMBIONT TO TANDEM	
PRESCHEDUL	E RVR, SM	PESPOND TO VERTICAL	
PRESCHEDUL	E RTR.,SM	RESPOND TO TANDEM	

The satellite computers have the same SYSGEN sources except for the

cpu numbers -- the Vertical cpu is cpu 0 and the Tandem is cpu 1:

MYCPU			0 FOR VERT., 1 FOR TANDEM COMMON FOR COMMUNICATIONS SYMBIONT FOR HOST	
	SYMCONTROLL			
	DEVICE		TYPEWRITER ON HOST	
	DEVICE		CARD READER ON HOST	
	DEVICE	LP,RH,134	LINE PRINTER ON HOST	
	DEVICE	MT1,RH,256	MAG TAPE 1 ON HOST	
	DEVICE	MT2,RH,256	MAG TAPE 2 ON HOST	
	DEVICE		,0,0,0,0 FHD PARTITION	
	All partitions on the host's fixed head disc			
			,0,0,0,0 FHD PARTITION	
	DEVICE	DNA,RH,200,1,,,0,0,0	,0,0,0,0 M1 MHD PARTITION	
		one on the bestle may	ing hand disp (M1)	
	All partitions on the host's moving head disc (M1)			
	DEVICE		,0,0,0,0 M1 MHD PARTITION	
	DEVICE			
			,0,0,0,0 RAND. ACCESS	
	DEVICE	ULH,RH,200,1,,,0,0,0		
	PRESCHEDULE		SYMBIONT TO HOST	
	PRESCHEDULE	RHP,,SM	RESPOND TO HOST	

The BORG macro is a MODCOMP SYSGEN macro which "back-origins" to the address given as the first argument and puts in the value of the second argument. The 7 extra words at the end of the DEVICE statements allow the MAX IV system to put in the information about these "disc files" without destroying the next DEVICE statement. That is, the seven extra words make the code generated by the DEVICE statements the same length as the code generated by the DISCDEVICE statements.

.

Program Sizes

The sizes of the programs are as follows, omitting the 768 words of GLOBAL COMMON:

RT,RV,RH (the symbionts)	#414 (1044 ₁₀)
RVR,RTR (respond to interrupt)	#5C (92 ₁₀)
RHR (respond to interrupt)	#100 (256 ₁₀)
Cold Start Initialization	#85 (235 ₁₀)

-10-

Limitations

The symbiont system of communication does not, at the present time, support system I/O which uses the DMP chaining. This would include such operations as loading a program (quick load module) from a remote disc. We have also found that using the "LIST" command in the Task/Overlay Catalogen (TOC) when the disc partition is remote is also not possible. It is possible, however, to GET, PUT, SAVE and RESTORE remotely using TOC. Basically the system described here is designed to allow the use of remote peripherals.

Speed

The speed of the system is slower than a comparable I/O operation locally because of the additional overhead of a second call to BIOS in the remote computer and the time required for the taskmaster to schedule the tasks which are connected to the RMI interrupts. However, This time is usually small compared to disc arm motiom. In fact, we routinely use a scratch partition of the M1 disc of the host to compress satellite disc files because the lack of arm contention makes the operation proceed almost twice as fast than if the same local disc is used.

As an example of the difference in speed, the following test was made:

A FORTRAN program on disc M1 of the host was compiled by a satellite computer and the output was sent back to the host for printing. The binary output was placed on the satellite's local disc. The same operation was done on the host with M0 being used for the binary output. In both cases the line printer spooling was done to the host's fixed head disc. This way the disc arm contention should be about the same.

Using the satellite the time required was one minute and fifty-two seconds and, using the host, with all local devices, the time required was one minute and forty-eight seconds -- a difference of four seconds or less than 4%.